

**U.S. DEPARTMENT OF ENERGY
OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT**

**PRESENTATION TO
THE NUCLEAR WASTE TECHNICAL REVIEW BOARD**

**SUBJECT: APPLICABILITY OF
LABORATORY EXPERIMENTS**

**PRESENTERS: DR. AREND MEIJER AND
DR. ROBERT S. RUNDBERG**

**PRESENTER'S TITLE
AND ORGANIZATION: GEOCHEMISTS,
LOS ALAMOS NATIONAL LABORATORY
LOS ALAMOS, NEW MEXICO**

**PRESENTER'S
TELEPHONE NUMBER: (505) 667-0675/(505) 667-4559**

DECEMBER 11-12, 1989

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APPLICABILITY OF LABORATORY EXPERIMENTS

OVERVIEW

- PHYSICAL AND CHEMICAL PROCESSES THAT DETERMINE RADIONUCLIDE (RN) MOBILITY
- MAIN FACTORS THAT CONTROL SORPTION BEHAVIOR FOR EACH RN
- EXPERIMENTAL R_d DETERMINATIONS
- EXPERIMENTAL DETERMINATION OF OTHER TRANSPORT PARAMETERS
- APPLICABILITY OF LABORATORY EXPERIMENTS TO UNSATURATED-ZONE MOBILITY OF RN AT YUCCA MOUNTAIN

PHYSICAL AND CHEMICAL PROCESSES THAT DETERMINE RN MOBILITY IN GROUND WATER SYSTEMS

- **GROUND-WATER FLOW PARAMETERS**
 - VELOCITY, DISPERSION, MATRIX VS. FRACTURE FLOW, MATRIC POTENTIAL, ETC.
- **RN SOLUBILITY, COLLOID FORMATION**
- **RN DIFFUSION RATE, OSMOTIC POTENTIAL (?)**
- **INTERACTION WITH HOST ROCKS AND FRACTURE LININGS**
 - ANION EXCLUSION, COLLOID FILTRATION
 - SORPTION REACTIONS, COPRECIPITATION

MAIN FACTORS THAT CONTROL SORPTION BEHAVIOR OF EACH RN

- **TYPES AND ADSORPTION CAPACITIES OF SOLID SURFACES IN ROCKS AND FRACTURES**
 - ION EXCHANGE IN ZEOLITES AND CLAYS
 - SURFACE ADSORPTION IN Fe–Mn PHASES, FELDSPARS, SILICA PHASES, GLASS, ETC.
- **GROUND-WATER COMPOSITION**
 - pH, Eh, m, I
- **IDENTITIES AND CONCENTRATIONS OF RN**
- **SORPTION KINETICS**
- **TEMPERATURE**

EXPERIMENTAL R_d DETERMINATIONS

- **BATCH CRUSHED ROCK, SOLID-ROCK WAFERS, CRUSHED-ROCK COLUMNS**
 - OBTAIN R_d 's FOR EACH RN UNDER RANGE OF ANTICIPATED CONDITIONS
 - INVESTIGATE SORPTION KINETICS FOR EACH RN
- **VALIDATION AND EXTRAPOLATION OF EXPERIMENTAL R_d DATA**
 - INVESTIGATE POTENTIAL EXPERIMENTAL ARTIFACTS
 - MECHANISTIC STUDIES OF SORPTION ON "KEY MINERALS"

EMPIRICAL (BATCH) APPROACH

- SELECT:**
- (1) ROCK (CRUSHED) SAMPLE**
 - (2) GROUND-WATER COMPOSITION**
 - (3) RADIONUCLIDE SPECIES AND CONCENTRATIONS**
 - SOLUBILITY CONSTRAINTS**
 - (4) ATMOSPHERE**
 - pH, Eh CONSTRAINTS**
 - (5) WATER/ROCK RATIO**
 - UNSATURATED-ZONE DATA**
 - EXPERIMENTAL CONSTRAINTS**
 - 6) EXPERIMENT DURATION – KINETICS**

EMPIRICAL (BATCH) APPROACH

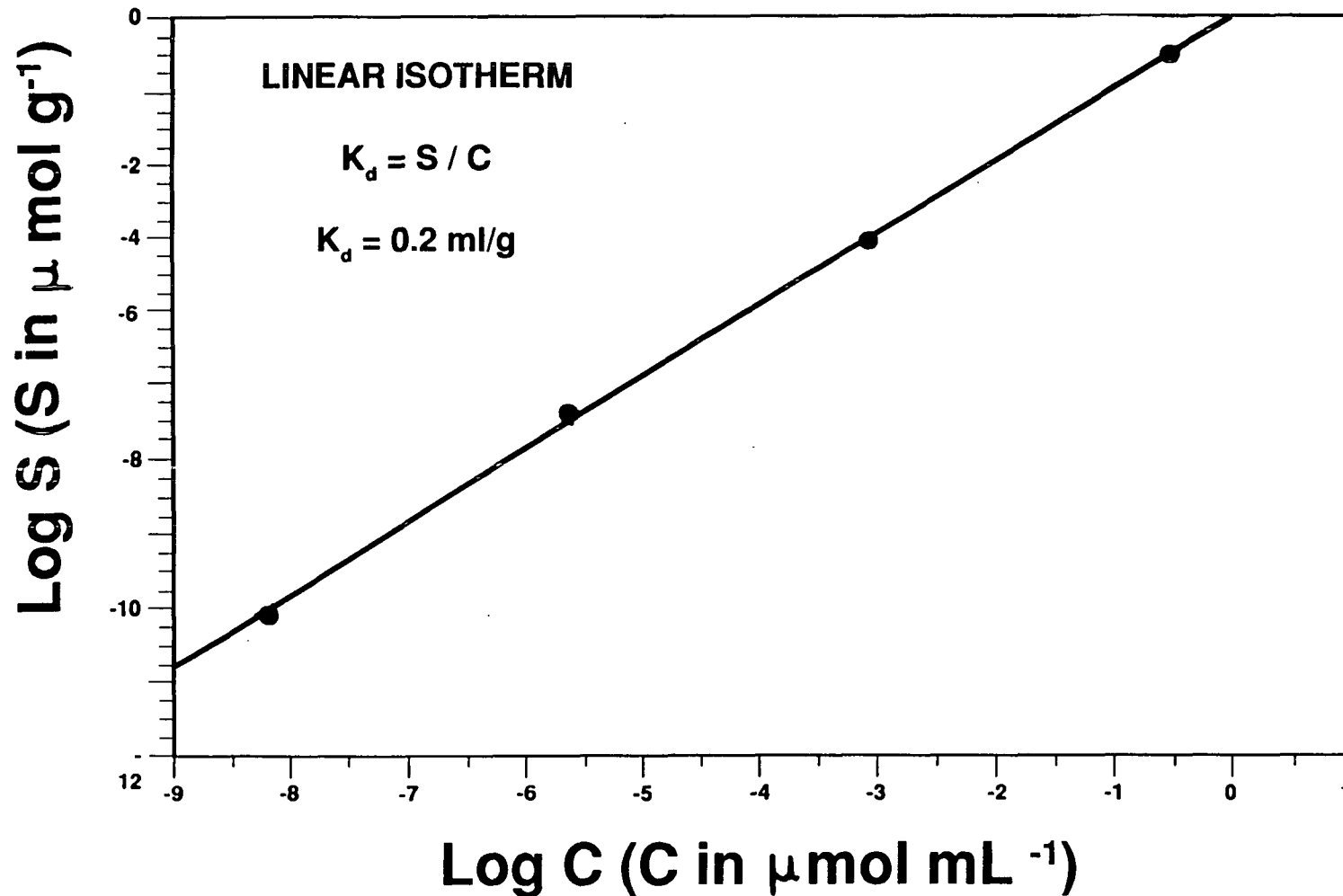
(CONTINUED)

DEVELOP: (1) EXPERIMENTAL TECHNIQUE

OBTAIN: (1) SORPTION RATIOS (R_d)
(2) SORPTION ISOTHERMS

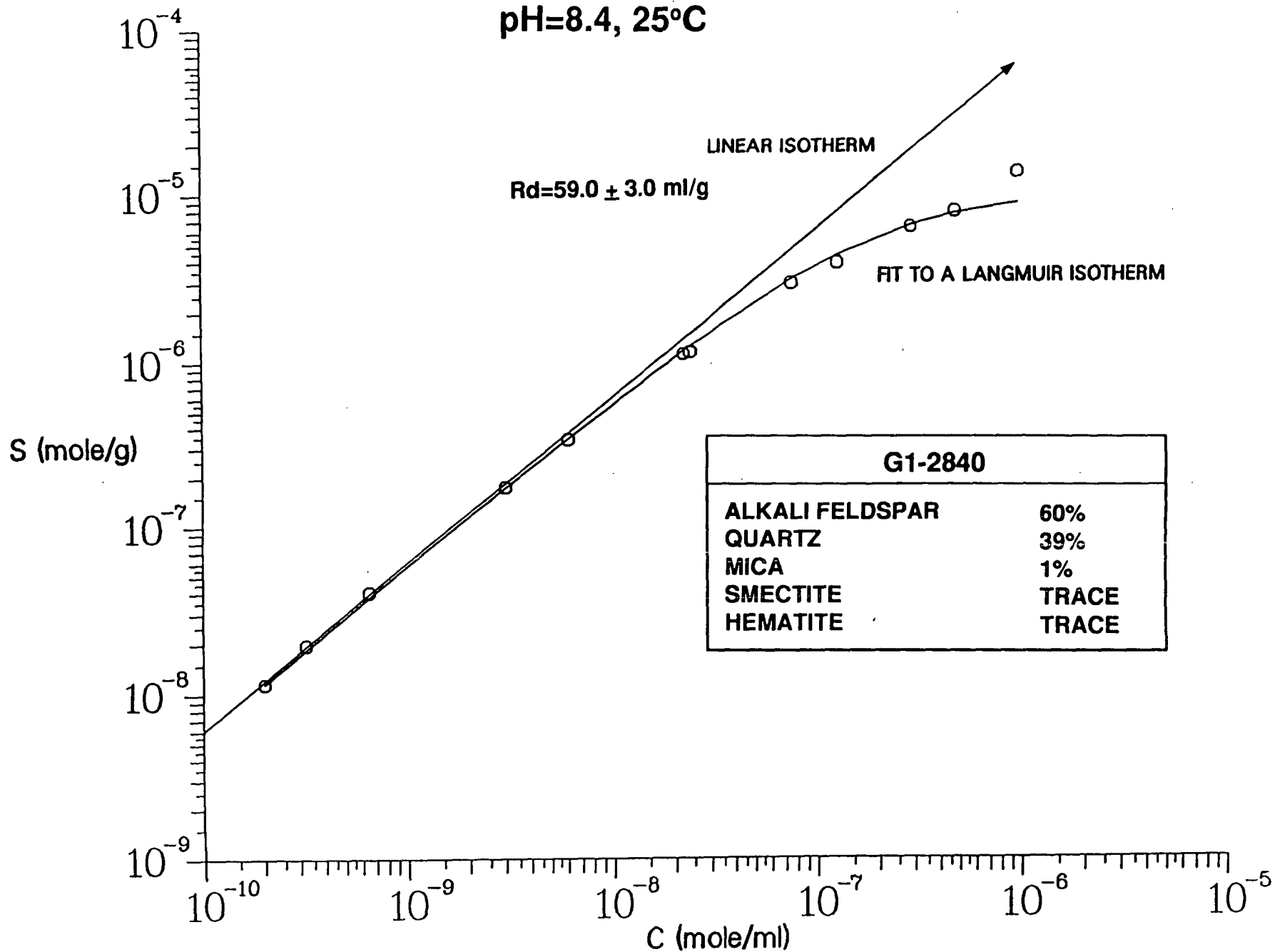
DERIVE: (1) R_d MATRIX FOR HYDROLOGIC UNITS
(2) PREDICTIVE EQUATIONS FOR
FRACTURE R_d 's

Tc SORPTION ON ZEOLITIC TUFF (AIR)

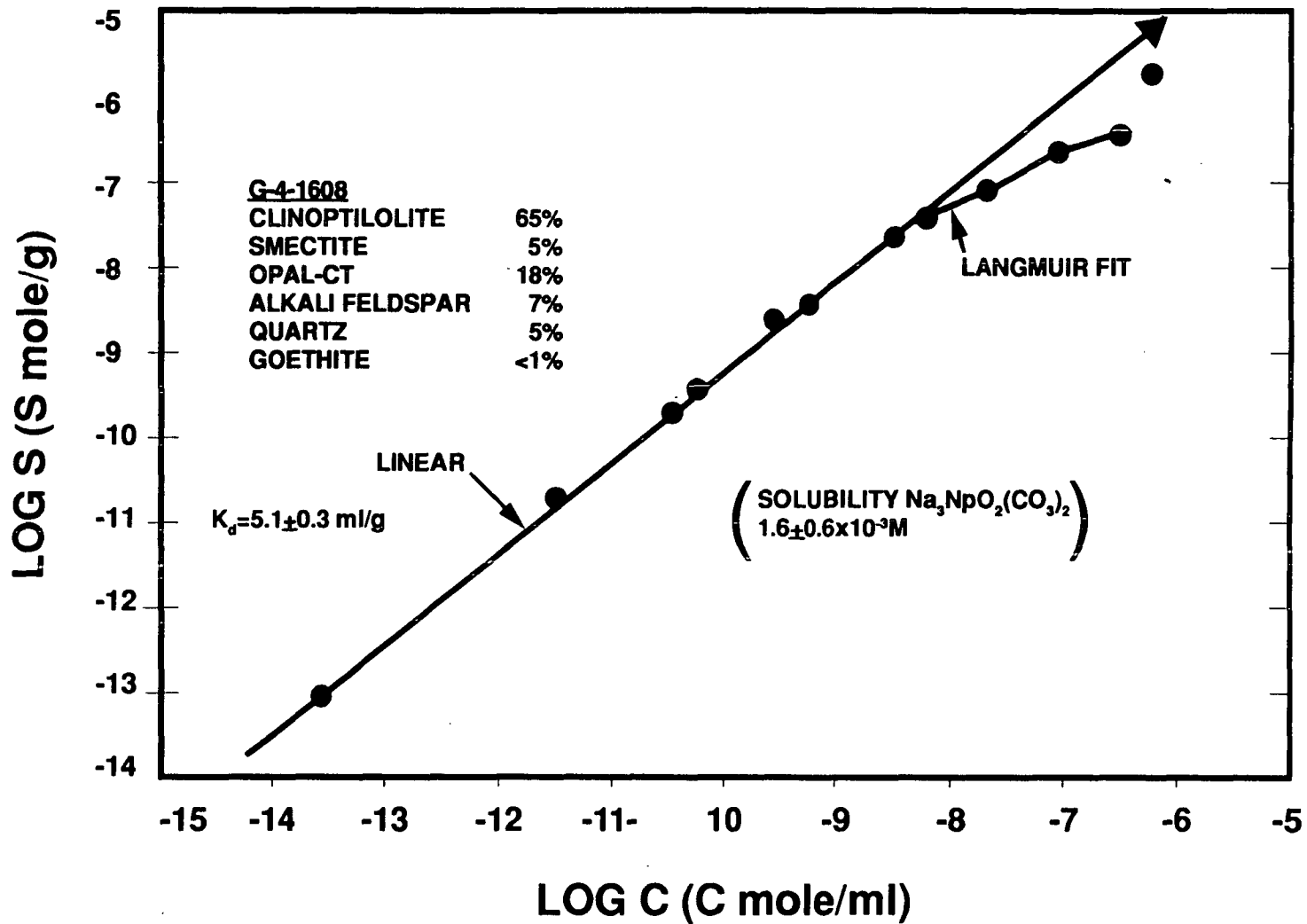


STRONTIUM SORPTION ISOTHERM FOR G1-2840 TUFF/J-13

pH=8.4, 25°C



Np ON ZEOLITIC TUFF (J-13;5% CO₂)



VALIDATION AND EXTRAPOLATION OF EXPERIMENTAL R_d DATA

● EXPERIMENTAL ARTIFACTS

- ADSORPTION TO WALLS OF CONTAINER**
- OVERSATURATION**
- EFFECTS OF ROCK CRUSHING**
- EXCESSIVE WATER/ROCK RATIOS**
- SOLID/LIQUID SEPARATIONS**
- SPECIES EQUILIBRIUM IN SOLUTION**

Am ADSORPTION ON WALLS OF CONTAINER

- GROUND WATER (J-13) + ²⁴¹Am + TEFLON CONTAINER

| <u>TRACED AND ACIDIFIED</u> | <u>TECHNIQUE</u> | <u>CONCENTRATION</u> |
|-----------------------------|------------------|---------------------------|
| IMMEDIATELY | I.D. | 7.1 X 10 ⁻¹² M |
| 1 DAY | I.D. | 6.7 X 10 ⁻¹² M |
| 3 WEEKS | I.D. | 4.5 X 10 ⁻¹² M |

- 35% ²⁴¹Am LOST TO WALLS OF CONTAINER IN 3 WEEKS

Am SORPTION ON DEVITRIFIED TUFF IN J-13 WATER

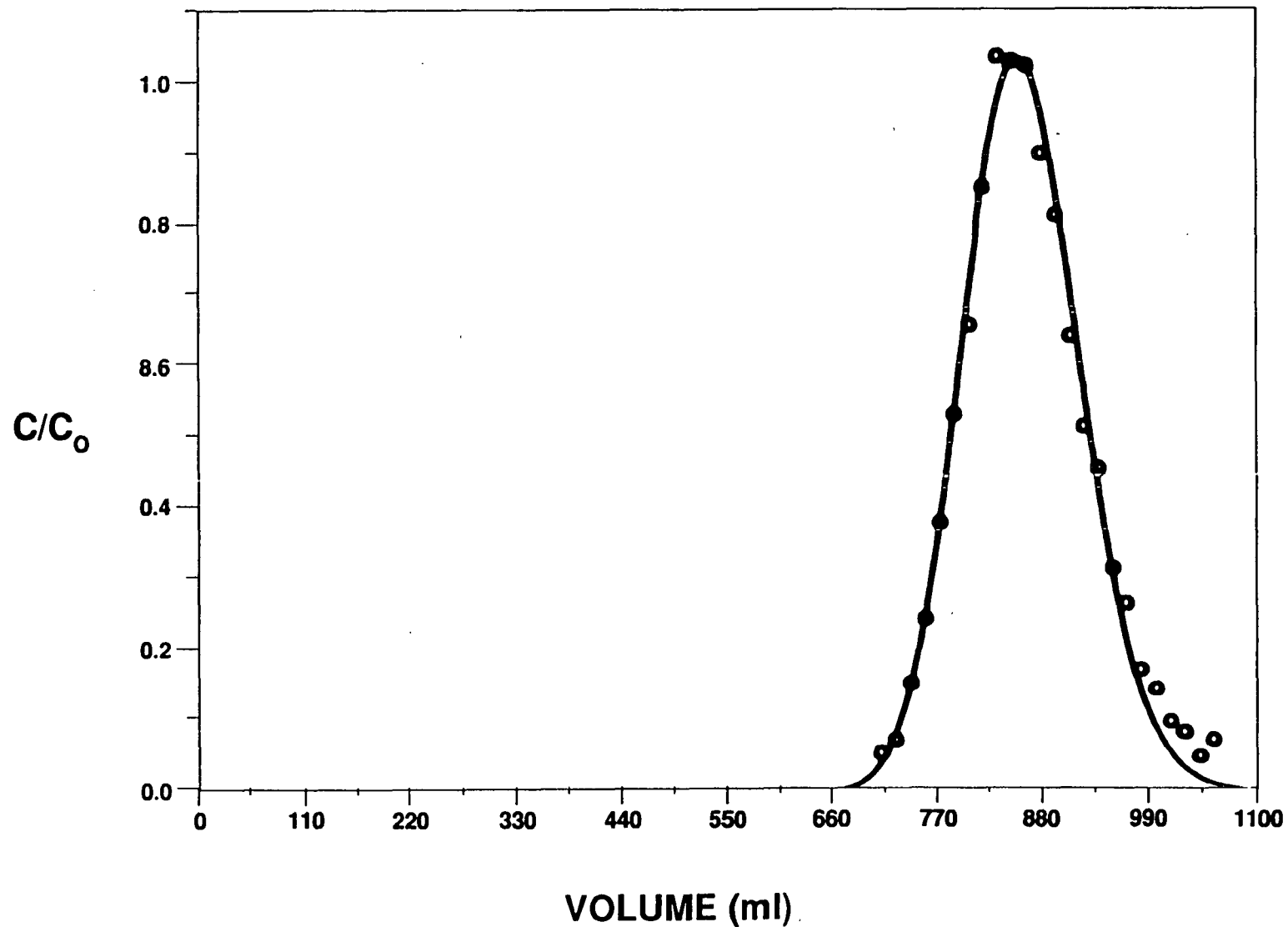
| <u>SAMPLE NO.</u> | <u>R_d (SORPTION)</u> | <u>R_d (DESORPTION)</u> | <u>INITIAL CONCENTRATION</u> |
|-------------------|---------------------------------|-----------------------------------|----------------------------------|
| GU3-688 | 14,000 | | 6.9x10 ⁻¹² M |
| G1-1833 | 4,200-5,300 | 5,900-8,900 | 1.0x10 ⁻⁷ M |
| GU3-433 | 2,900-3,800 | 6,000-14,000 | 2.1x10 ⁻⁷ M |
| JA-32 | 79-230 | 1,500-2,800 | 1.0x10 ⁻⁶ M |
| YM-22 | 1,100-1,500 | 1,900-3,100 | 1.0x10 ⁻⁷ M |
| YM-54 | 150-160 | 400-680 | 1.0x10 ⁻⁷ M |

SOLUBILITY OF SOLID AmOHCO₃ = 10⁻⁹ TO 10⁻¹⁰ M
pH = 8.0-8.5

R_d COMPARISON: TUFF WAFERS vs. CRUSHED TUFF

| <u>SAMPLE NO.</u> | <u>ELEMENT</u> | <u>R_d (WAFER) (ml/gm)</u> | <u>R_d (CRUSHED) (ml/gm)</u> |
|--|----------------|--|--|
| G1-1883 (DEVITRIFIED) | Ba | 210 | 180 |
| | Cs | 230 | 190 |
| | Sr | 27 | 22 |
| G1-1982 (DEVITRIFIED + CLAYS) | Ba | 800 | 800 |
| | Cs | 1,000 | 1,200 |
| | Sr | 80 | 62 |
| G1-1436 (ZEOLITIC) | Cs | 14,900 | 2,400 |
| | Sr | 95,500 | 87,000 |

G1-3658 CRUSHED-ROCK COLUMN, Sr SPIKE IN CLAY-RICH TUFF (J-13 WATER)



WATER/ROCK RATIO EXPERIMENTS ZEOLITIC TUFF (G4-1502)

ULTRACENTRIFUGATION EXPERIMENTS

R_d 's (ml/g)

| <u>W/R RATIO</u> | <u>Ba</u> | <u>Cs</u> | <u>Sr</u> |
|------------------|------------------|----------------|------------------|
| 5:1 | 6,970 (2,400) | 14,600 (4,200) | >10,500 |
| 10:1 | 46,700 (14,000) | 13,900 (1,400) | >32,400 |
| 20:1 | 81,100 (3,900) | 23,800 (2,200) | >27,900 |
| 30:1 | 123,000 (25,000) | 31,100 (770) | 108,000 (40,000) |

ULTRAFILTRATION EXPERIMENTS

R_d 's (ml/g)

| <u>W/R RATIO</u> | <u>Ba</u> | <u>Cs</u> | <u>Sr</u> |
|------------------|------------------|----------------|------------------|
| 5:1 | 69,200 (4,900) | 17,900 (800) | 92,500 (55,900) |
| 10:1 | 106,000 (25,400) | 33,500 (3,100) | 169,600 (10,900) |
| 20:1 | 236,000 (4,100) | 43,200 (3,700) | 207,900 (9,050) |
| 30:1 | 433,800 (70,300) | 44,700 (2,150) | 322,100 (5,100) |

"MECHANISTIC" SORPTION STUDIES

- SELECT "KEY" MINERALS
 - CHARACTERIZE SURFACE PROPERTIES OF MINERALS SELECTED
 - OBTAIN ISOTHERMS FOR "IMPORTANT" RADIONUCLIDES
 - INVESTIGATE NATURE OF SORBED SPECIES
 - DEVELOP MODELS FOR SORPTION BEHAVIOR
-
- EVALUATE EXISTING R_d DATABASE
 - DEVELOP PREDICTIVE CAPABILITIES BASED ON MODELS OF SORPTION BEHAVIOR AND SITE DATA

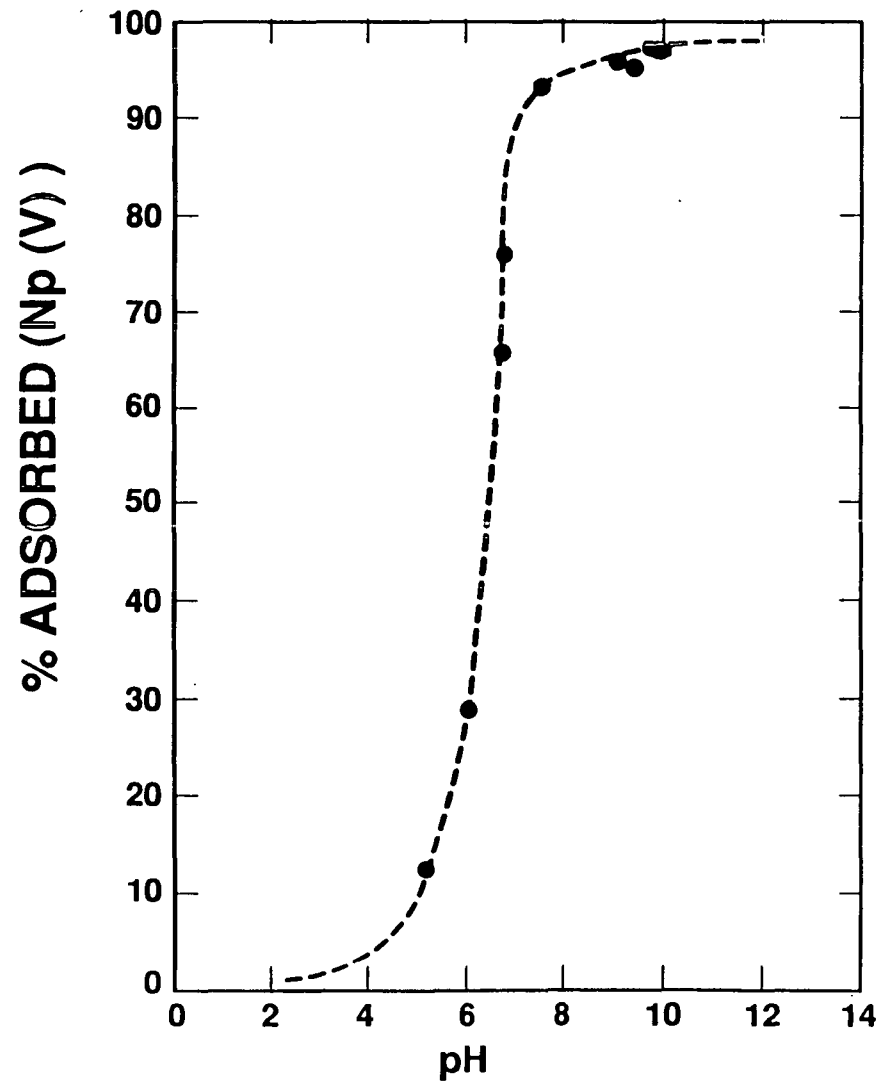
Np PURE MINERAL R_d 's

| <u>MINERAL</u> | <u>FORMULA</u> | <u>R_d (ml/g)^{1,2}</u> |
|-----------------------|---|--|
| HEMATITE (SYNTHETIC) | Fe_2O_3 | 5.1×10^4 |
| GOETHITE (SYNTHETIC) | $FeO(OH)$ | 5.1×10^4 |
| HOLLANDITE | $Ba(Mn^{2+}, Mn^{4+})_8O_{16} \cdot xH_2O$ | 7.8×10^3 |
| ROMANECHITE (NATURAL) | $(Ca, Mn)(Mn^{2+}, Mn^{4+})_4O_9 \cdot 3H_2O$ | 1.5×10^3 |
| CALCITE (NATURAL) | $CaCO_3$ | 390 |
| CALCITE (SYNTHETIC) | $CaCO_3$ | 21 |
| MONTMORILLONITE | $(Al_{1.37}Fe_{0.19}Mg_{0.46})(Si_{3.84}Al_{0.16})O_{10}(OH)_2$ | 78 |
| CLINOPTILOLITE | $(Na, K)_6(Al_6Si_{30}O_{72}) \cdot 20H_2O$ | 30 |

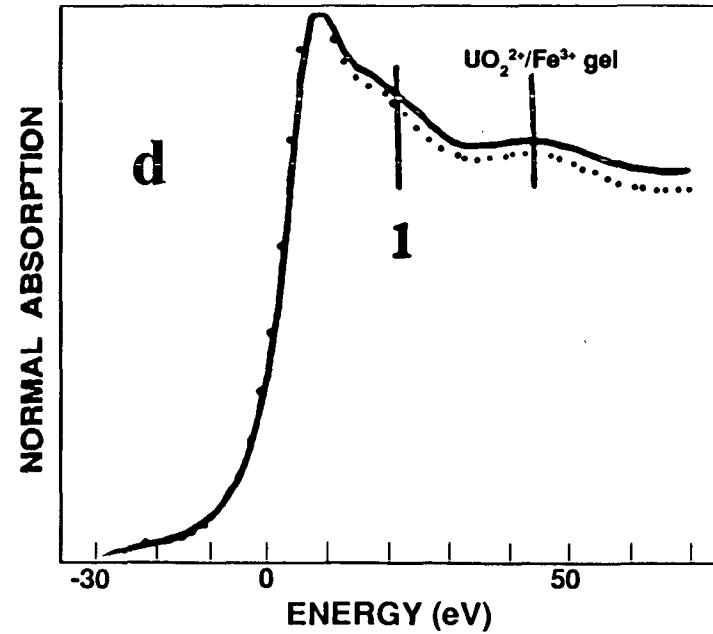
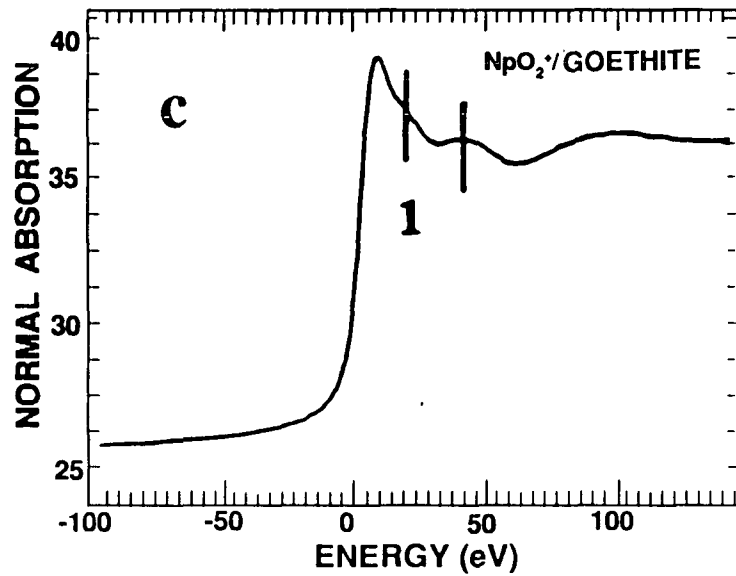
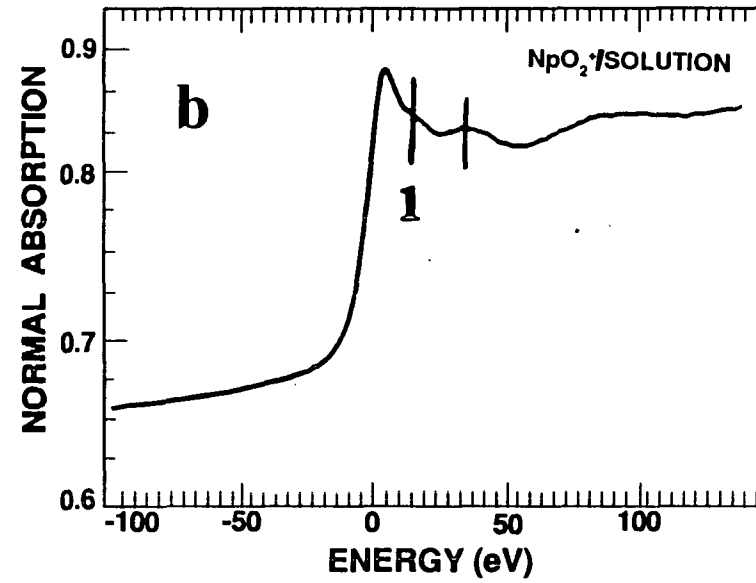
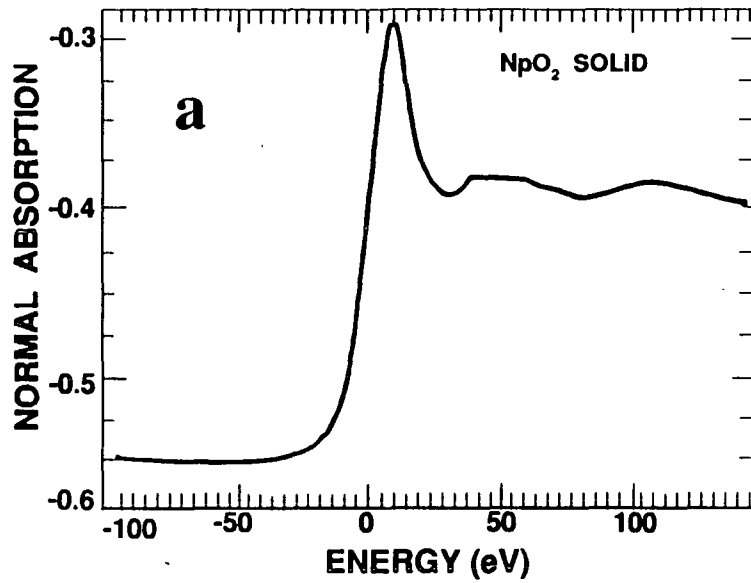
¹ DISTILLED WATER BUFFERED AT pH = 8.5 WITH SODIUM CARBONATE/BICARBONATE

² NOT CORRECTED FOR DIFFERENCES IN SURFACE AREAS

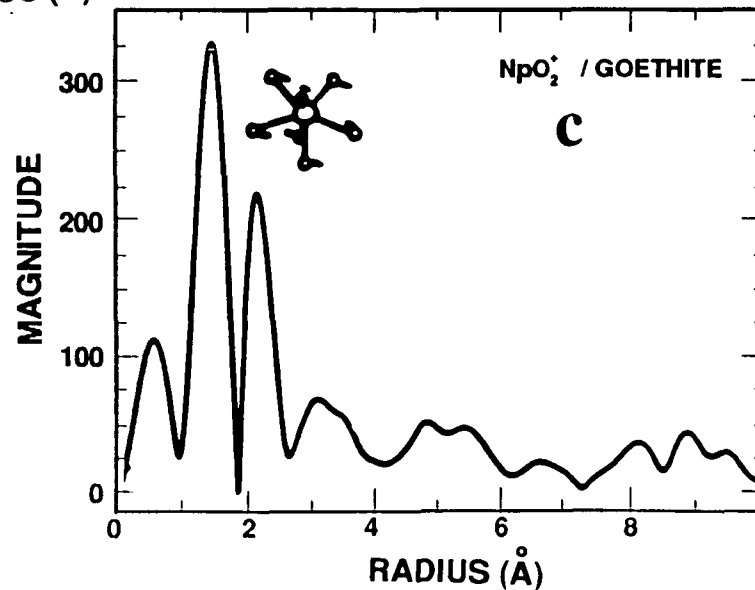
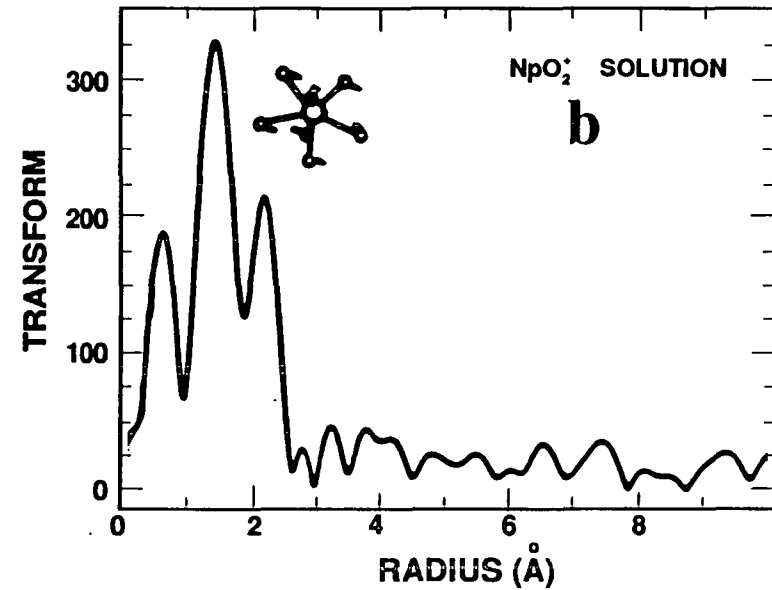
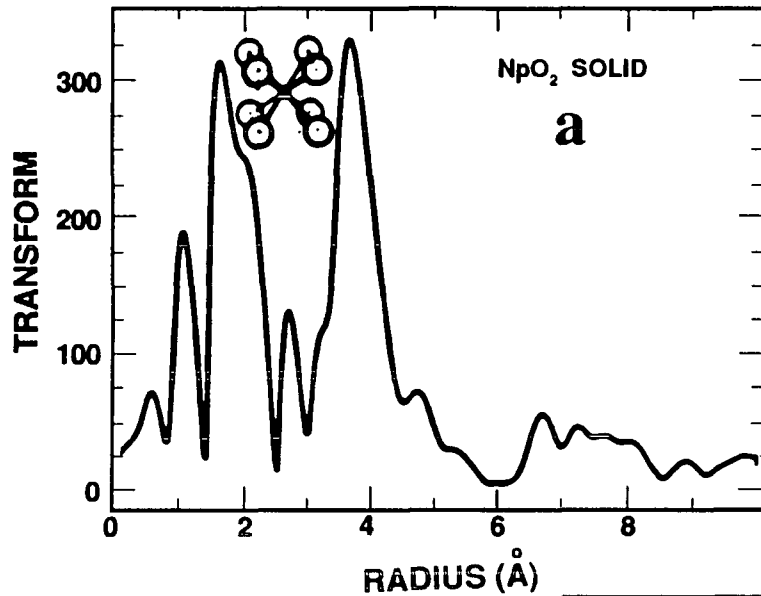
ADSORPTION OF Np (V) ON GOETHITE



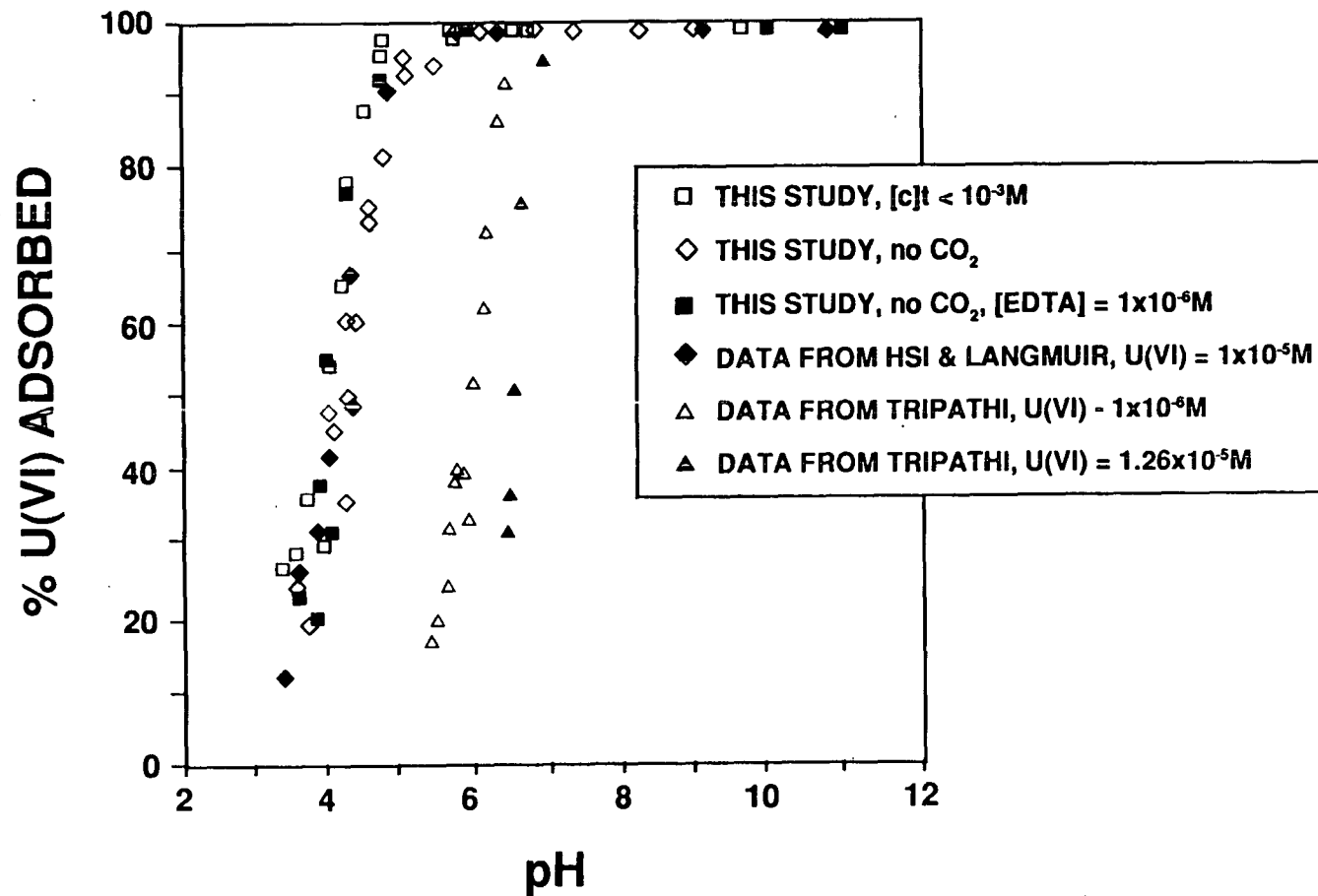
NEXAFS SPECTRA OF Np



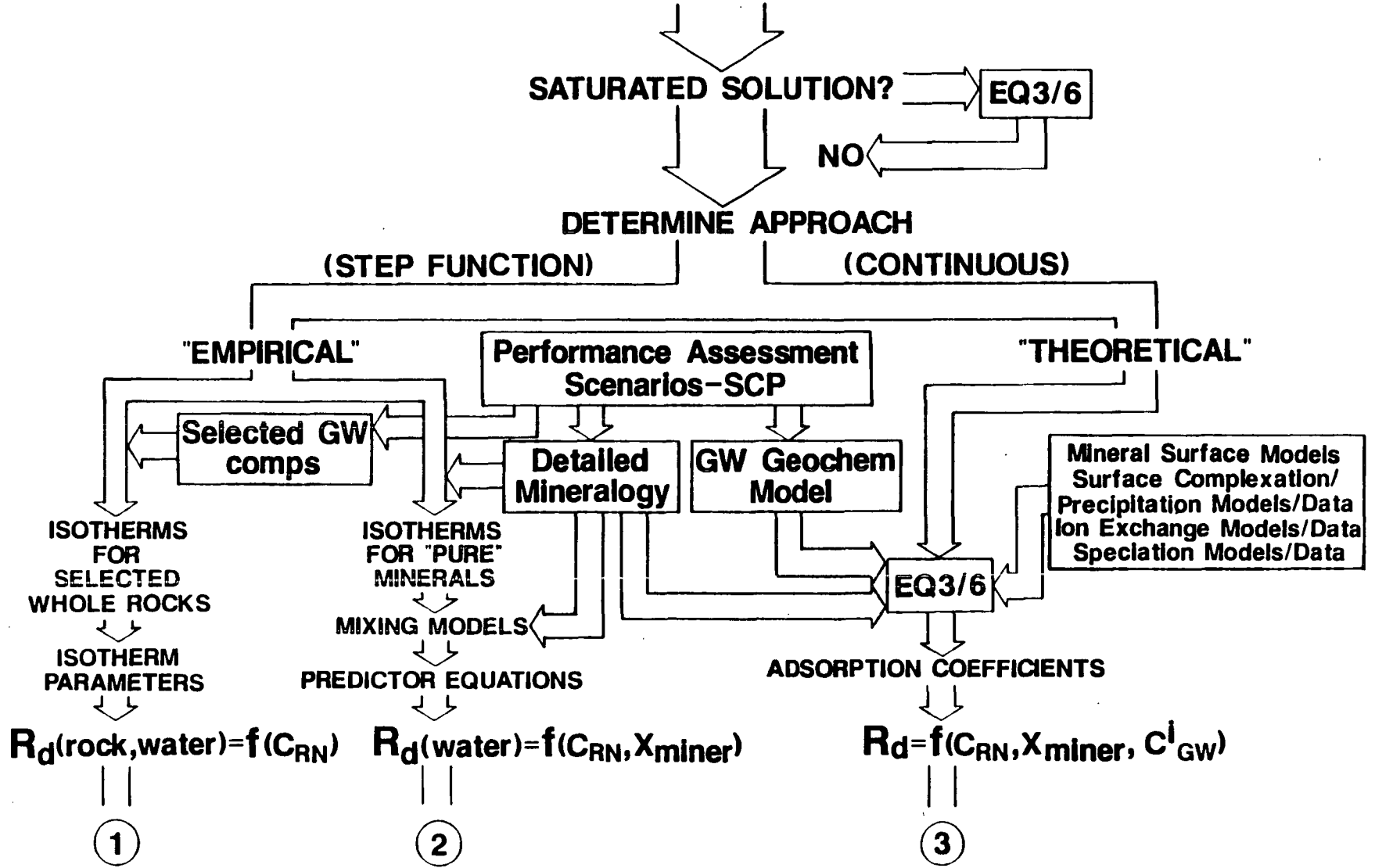
FOURIER TRANSFORM OF NEXAFS SPECTRA OF Np



U(VI) - ADSORPTION ONTO GOETHITE
I=0.1M NaClO₄, U(VI) = 1.0 x 10⁻⁶M
GOETHITE CONCENTRATION: 1g/l



CONCEPTUAL STRATEGIES FOR OBTAINING R_d 's



DYNAMIC TRANSPORT TASK: PURPOSE

- **TEST THE VALIDITY OF K_d 's FROM BATCH MEASUREMENTS FOR CALCULATING THE RETARDATION OF RADIONUCLIDES BY ADSORPTION ON MINERALS**
- **MEASURE THE EFFECTS OF DIFFUSION AND DISPERSION ON THE TRANSPORT OF RADIONUCLIDES**
- **PROVIDE EXPERIMENTAL EVIDENCE FOR SPECIATION AND/OR COLLOID FORMATION**
- **MEASURE COLLOID FILTRATION COEFFICIENTS IN YUCCA MOUNTAIN TUFF**
- **STUDY RADIONUCLIDE MIGRATION IN UNSATURATED TUFF**

DETERMINATION OF OTHER TRANSPORT PARAMETERS

- I. ANION EXCLUSION VOLUMES**
- II. DISPERSION PARAMETERS FROM
SOLID ROCK COLUMNS**
- III. DISPERSION/ R_d RELATIONSHIP**

DYNAMIC TRANSPORT TASK: SCOPE

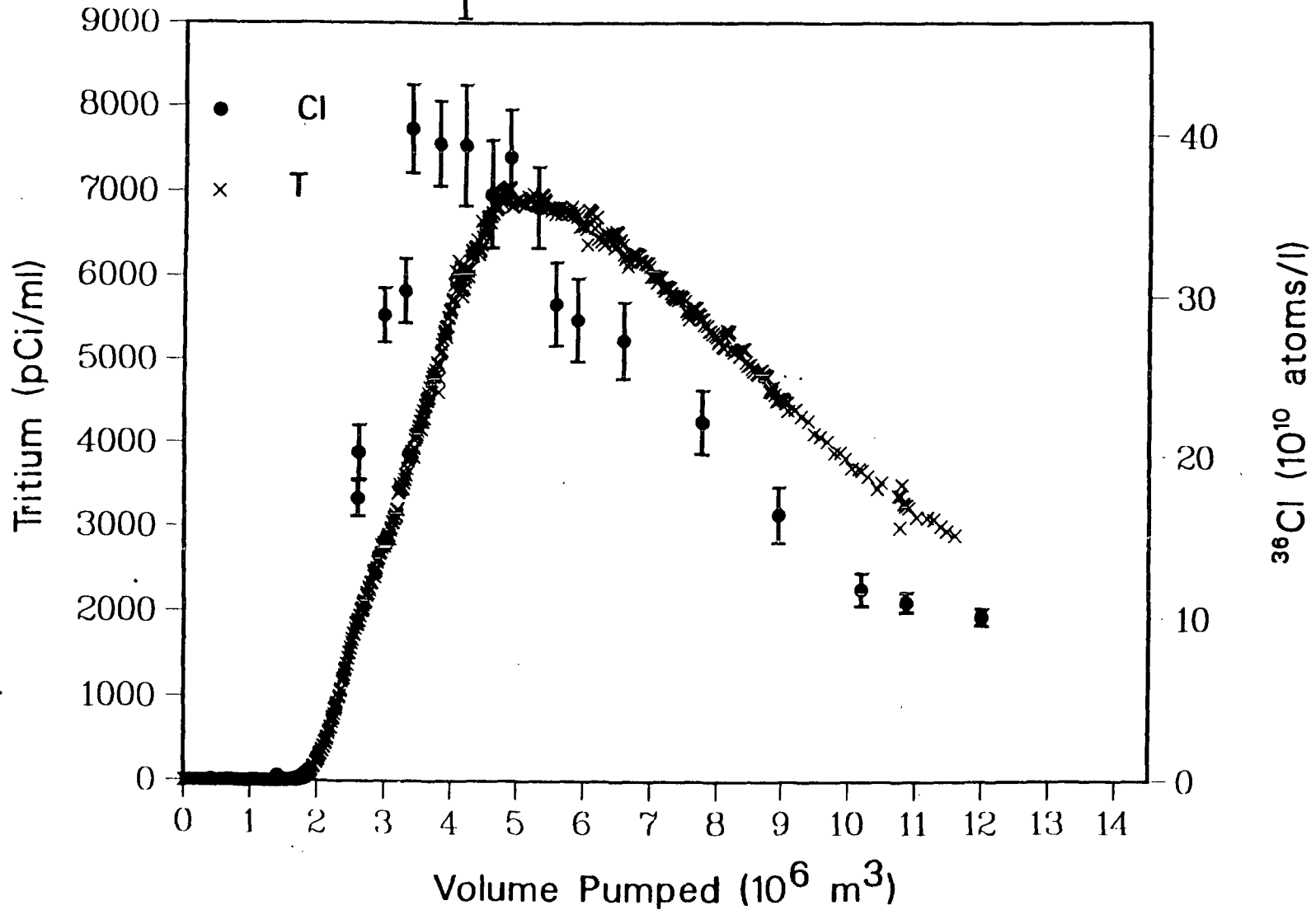
- **CRUSHED TUFF COLUMNS**
- **ADSORPTION KINETICS**
- **UNSATURATED TUFF COLUMNS**
- **FRACTURED TUFF COLUMNS**
- **COLLOID FILTRATION**
- **DIFFUSION CELLS**
- **SORPTION KINETICS WITH INTACT TUFF**
- **UNSATURATED DIFFUSION CELLS**

CRUSHED TUFF COLUMNS: CATION SORPTION

COMPARISON OF CRUSHED TUFF COLUMNS WITH BATCH SORPTION EXPERIEMENTS

| SAMPLE | ELEMENT | BATCH K_d | R_f (calc.) | R_f (meas.) |
|---------|---------|-------------|---------------|---------------|
| 1-2334 | Sr | 180 | 250 | 102 |
| | Ba | 1,400 | 1,940 | 1,180 |
| | Cs | 1,200 | 1,670 | 1,630 |
| YM-22 | Sr | 60 | 128 | 50 |
| | Ba | 890 | 1,890 | 723 |
| | Cs | 255 | 540 | 266 |
| YM-38 | Cs | 13,000 | 54,000 | 49,000 |
| G1-3116 | Sr | 2,300 | 9,146 | 1,065 |
| | Ba | 120,000 | 480,000 | 8,300 |
| | Cs | 5,900 | 23,000 | 7,100 |

OBSERVATION OF ANION EXCLUSION AT RNM-25 (CAMBRIC) FIELD TEST



STRUCTURAL DATA FOR ZEOLITES

ANALCIME

| | |
|---------------------|------------|
| DENSITY | 2.24 g/cc |
| VOID VOLUME | 0.18 cc/cc |
| INTERSTITIAL VOLUME | 0.089 cc/g |
| CHANNEL APERTURE | 2.6 Å |
| KINETIC DIAMETER | 2.6 Å |

CLINOPTILOLITE

| | |
|---------------------|------------|
| DENSITY | 2.16 g/cc |
| VOID VOLUME | 0.34 cc/cc |
| INTERSTITIAL VOLUME | 0.21 cc/g |
| KINETIC DIAMETER | 3.5 Å |

MORDENITE

| | |
|--------------------------|-------------|
| DENSITY | 2.13 g/cc |
| VOID VOLUME | 0.28 cc/cc |
| INTERSTITIAL VOLUME | 0.15 cc/g |
| CHANNEL APERTURE (LARGE) | 6.7 x 7.0 Å |
| CHANNEL APERTURE (SMALL) | 2.9 x 5.7 Å |
| KINETIC DIAMETER | 3.9 Å |

EFFECTIVE IONIC RADII

| ANION | IONIC RADIUS Å |
|-------------------------------|-------------------|
| F ⁻ | 1.38 ⁷ |
| Cl ⁻ | 1.81 ⁷ |
| I ⁻ | 2.16 ⁷ |
| NO ₃ ⁻ | 2.68 ⁸ |
| SO ₄ ⁻ | 2.88 ⁸ |
| TcO ₄ ⁻ | 3.13 ⁹ |

ANION EXCLUSION VOLUMES

| <u>SAMPLE IDENTIFICATION</u> | <u>MEASURED (ml/g)</u> | <u>CALCULATED^a (ml/g)</u> | <u>CALCULATED^b (ml/g)</u> |
|------------------------------|------------------------|--------------------------------------|--------------------------------------|
| USWG2-339 | 0.056±0.010 | 0.030±0.006 | — |
| USWG2-1951 | 0.20±0.03 | 0.112±0.020 | 0.145±0.028 |
| USWG2-2017 | 0.13±0.01 | 0.109±0.020 | 0.142±0.025 |
| USWG2-2698 | 0.069±0.009 | 0.072±0.008 | 0.09±0.011 |
| USWG3-1868 | 0.035±0.001 | 0.033±0.004 | 0.035±0.004 |

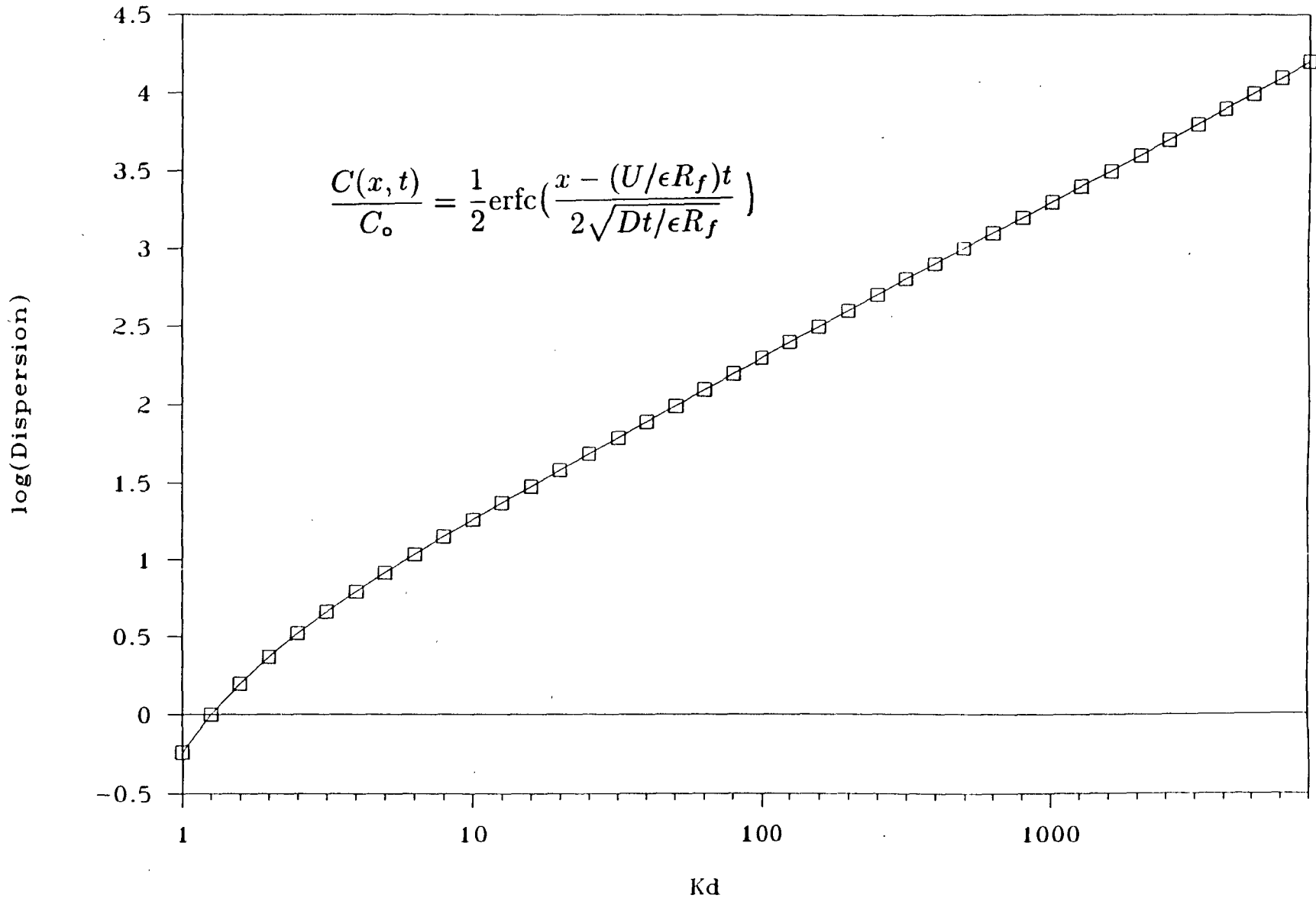
^a BASED ON VOID VOLUME

^b BASED ON INTERSTITIAL VOLUMES OF DEHYDRATED ZEOLITES

HOW DOES DISPERSION AFFECT THE MIGRATION OF CONTAMINANTS?

- **THE BREAKTHROUGH OF CONTAMINANTS IS BROADENED BY DISPERSION. DISPERSIVITY IS EQUIVALENT TO THE HEIGHT OF THEORETICAL PLATE (AS IT IS REFERRED TO IN ANALYTICAL CHEMISTRY)**
- **A BROADENED BREAKTHROUGH CURVE RESULTS IN THE EARLY ARRIVAL OF A FRACTION OF TOTAL CONTAMINANT**
- **IF THE DISPERSIVITY IS LARGE, THE PEAK CONCENTRATION OF A CONSERVATIVE TRACER WILL OCCUR AT A TIME EARLIER THAN ANTICIPATED BASED ON THE POROSITY AND FLOW RATE ALONE**

DISPERSION vs K_d



COMMON ASSUMPTIONS IN HYDROLOGY

- TRANSPORT OF RADIONUCLIDES IN POROUS MEDIA HAS BEEN CONSIDERED A DIFFUSIVE PROCESS,

$$\text{div}(D\text{grad}C - UC) = \frac{\epsilon\partial C}{\partial t}$$

THIS APPROACH ASSUMES THAT A HETEROGENEOUS AQUIFER CAN BE TREATED AS AN EQUIVALENT HOMOGENEOUS POROUS MEDIUM

- THE EXISTENCE OF A REPRESENTATIVE ELEMENTARY VOLUME, REV. THE PRINCIPLE THAT VARIATIONS IN MACROSCOPIC VARIABLES OCCUR ONLY ON A SMALL SCALE, i.e., THE SCALE OF A PORE DIAMETER
- THAT DISPERSION CAN ALWAYS BE TREATED AS FICKIAN
- THE MIGRATION OF SORBING CONTAMINANTS CAN BE PREDICTED USING THE RETARDATION FACTOR,

$$R_f = 1 + \frac{K_d\rho_b}{\epsilon}$$

NEW THEORIES OF CONTAMINANT MIGRATION

- STOCHASTIC MODELS ALLOW ONE TO CONSIDER HETEROGENEITY IN TERMS OF STATISTICAL PROPERTIES (MEAN, VARIANCE, COVARIANCE, ...). A SIMPLE CASE IS A STRATIFIED POROUS MEDIUM WITH FLOW PARALLEL TO THE STRATIFICATION. THE ADVECTION DISPERSION EQUATION IN RANDOM VARIABLES, ξ AND ζ , IS

$$X_t = \xi + \int_0^t u(Z_t) d\tau$$

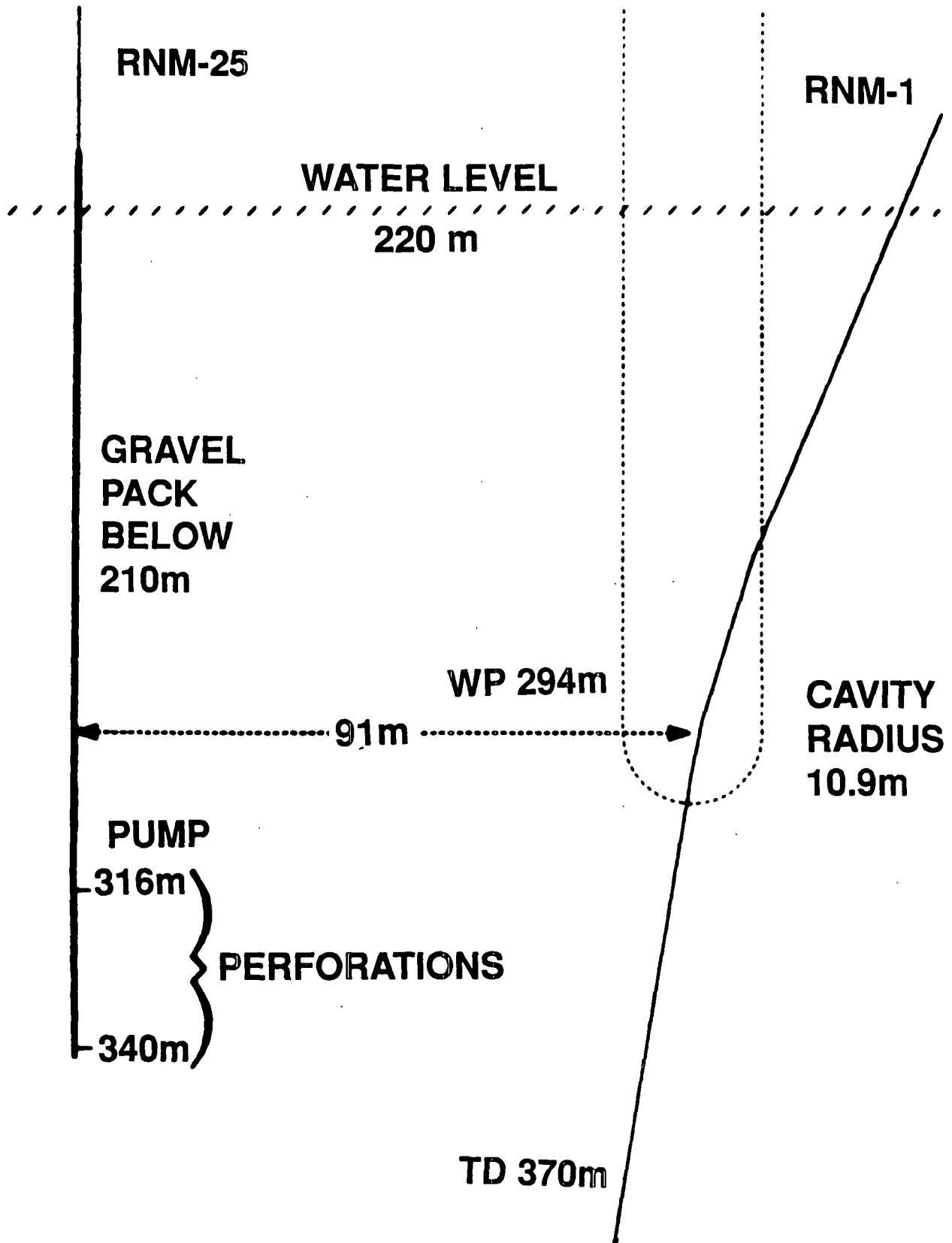
$$Z_t = \zeta_t$$

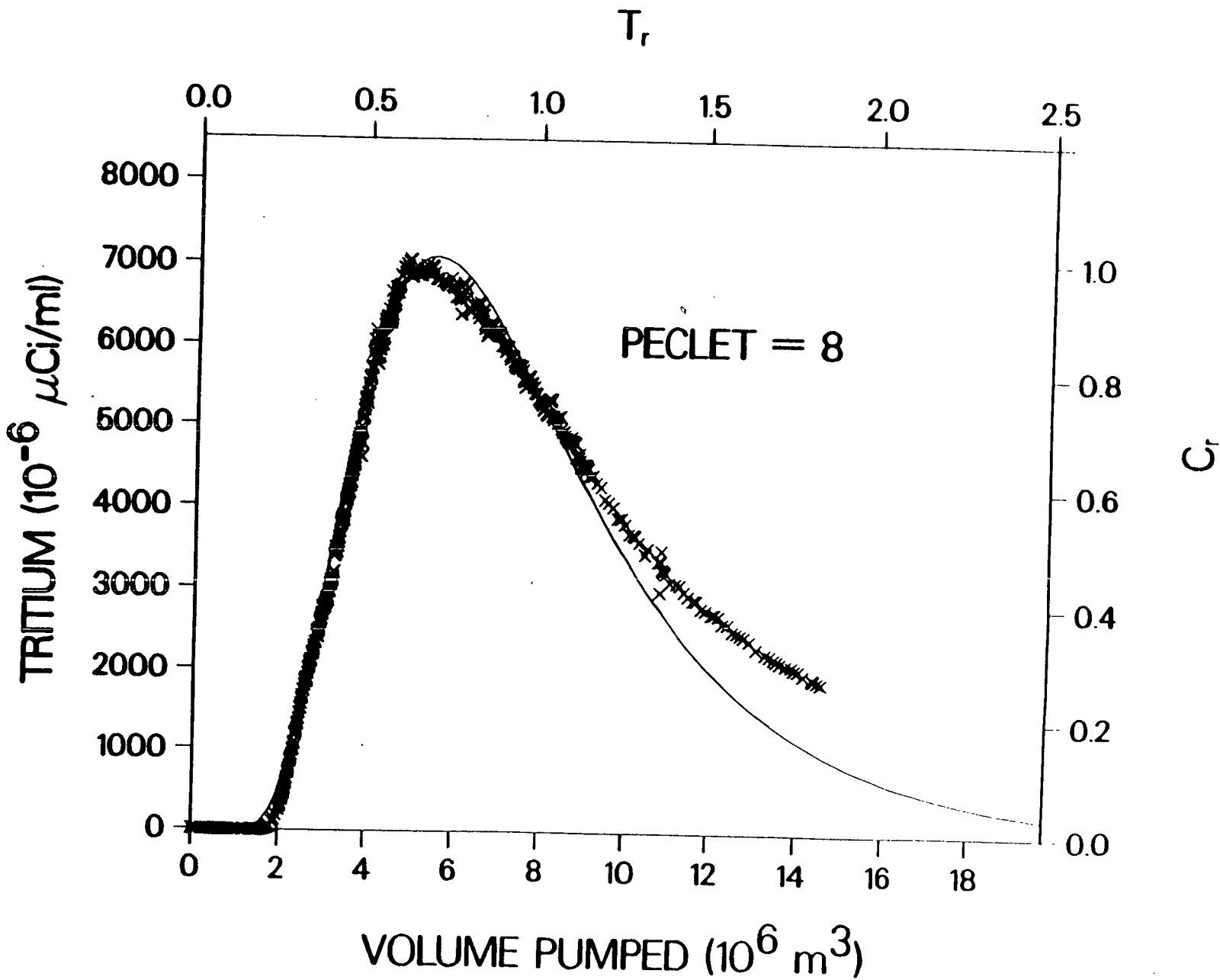
- THE EQUIVALENT DISPERSION IN THIS TREATMENT IS

$$D_A = D_L + t^{-1} \int_0^t (t - \tau) \frac{1}{2(\pi D_T \tau)^{\frac{1}{2}}} \cdot \int_{-\infty}^{+\infty} \exp\left(-\frac{s^2}{4D_T \tau}\right) \text{Cov}(s) ds d\tau$$

- IT CAN BE SHOWN FROM THIS EQUATION THAT DISPERSION IS STRICTLY FICKIAN ONLY WHEN THE COVARIANCE FUNCTION IS EQUAL TO THE FIRST DERIVATIVE OF THE DELTA FUNCTION. THE PORE STRUCTURE WHICH ENABLES THE USE OF REV PRINCIPLE APPROXIMATES THIS COVARIANCE FUNCTION
- THIS STOCHASTIC APPROACH DEMONSTRATES THAT THE CONVENTIONAL DIFFUSION EQUATION IS ONLY APPLICABLE TO A SUBSET OF SPATIAL DISTRIBUTIONS OF PERMEABILITY, i.e., THOSE WHERE THE GRAPH OF CONDUCTIVITY HAS A FRACTAL DIMENSION GREATER THAN 1.5

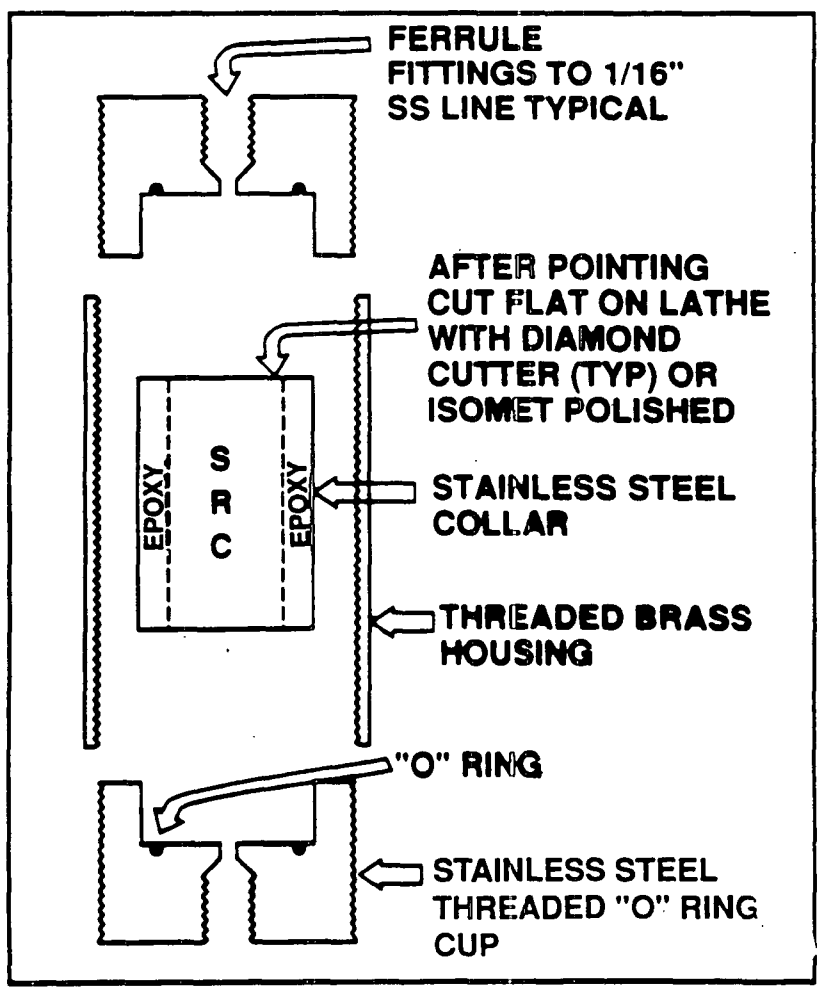
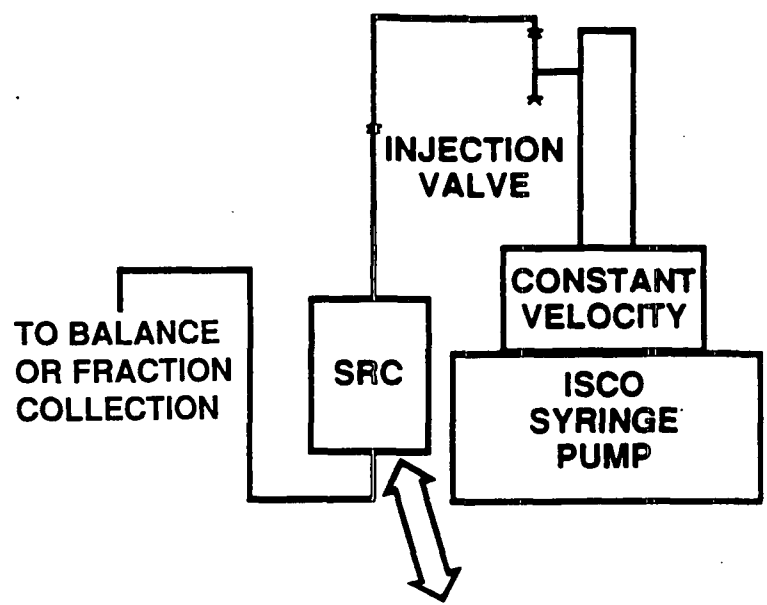
SCHEMATIC OF CAMBRIC FIELD TEST



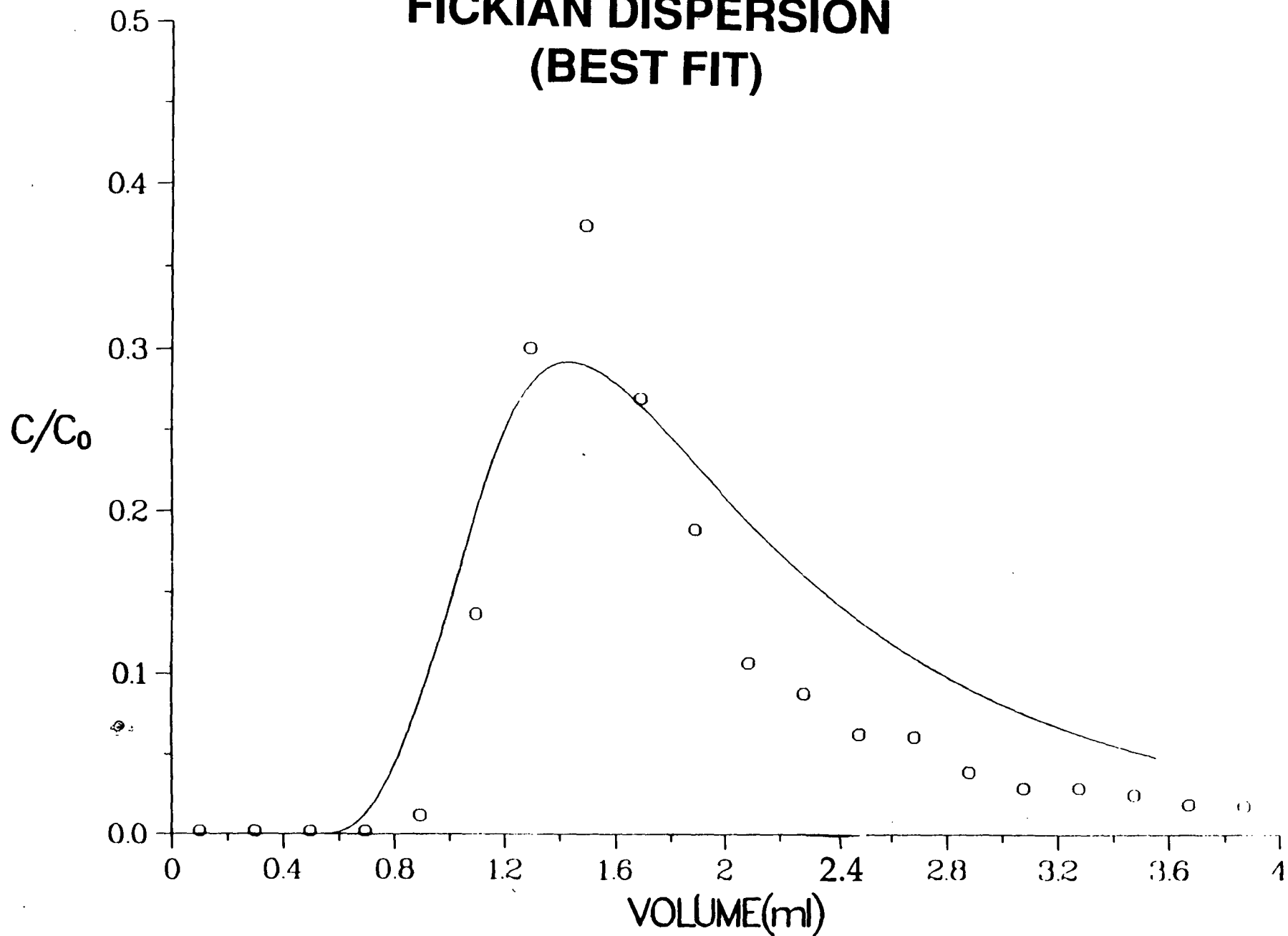


SOLID ROCK COLUMN SET-UP DRAWING

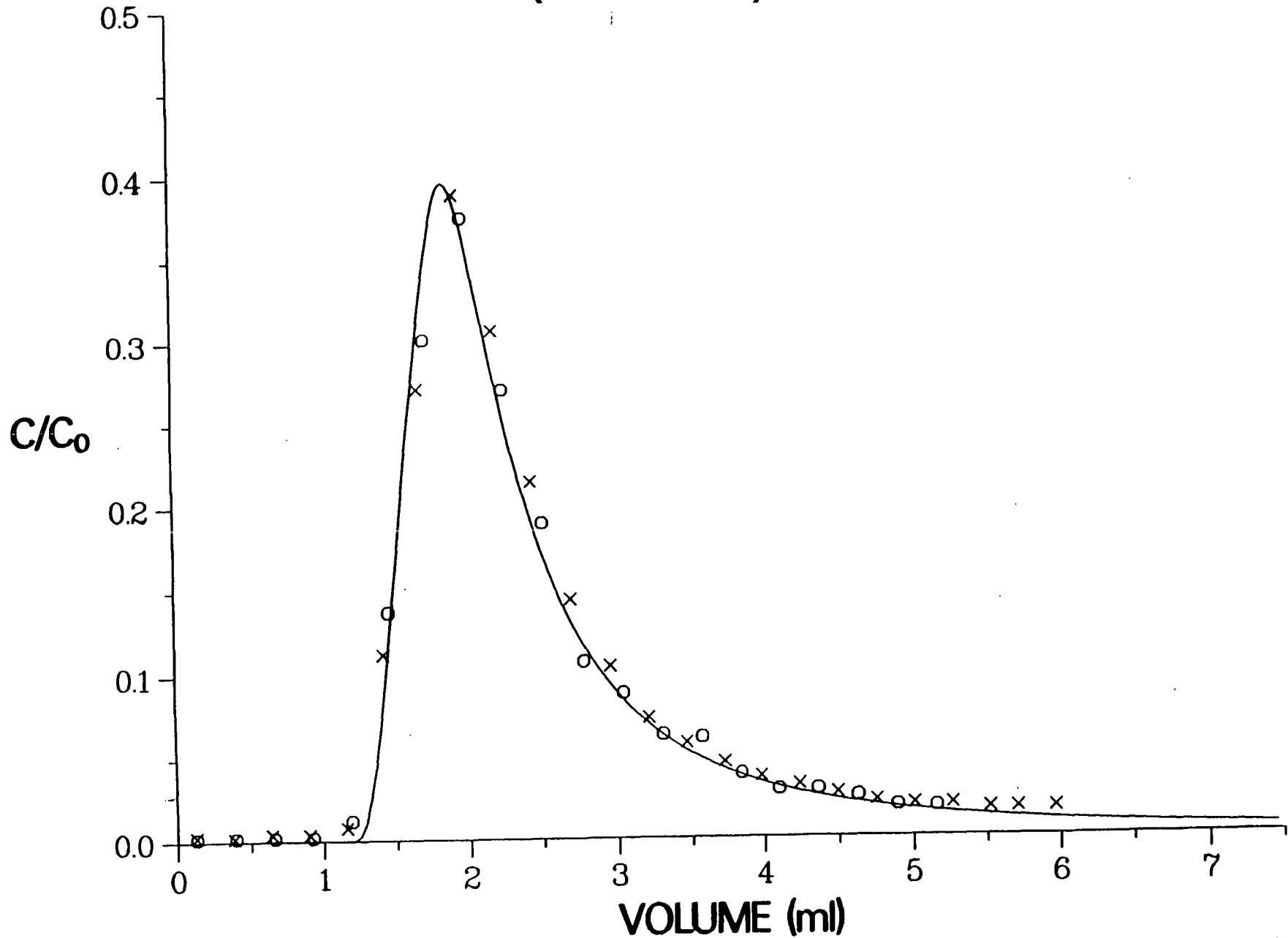
SET UP OF SYRINGE PUMP AND SOLID ROCK COLUMN



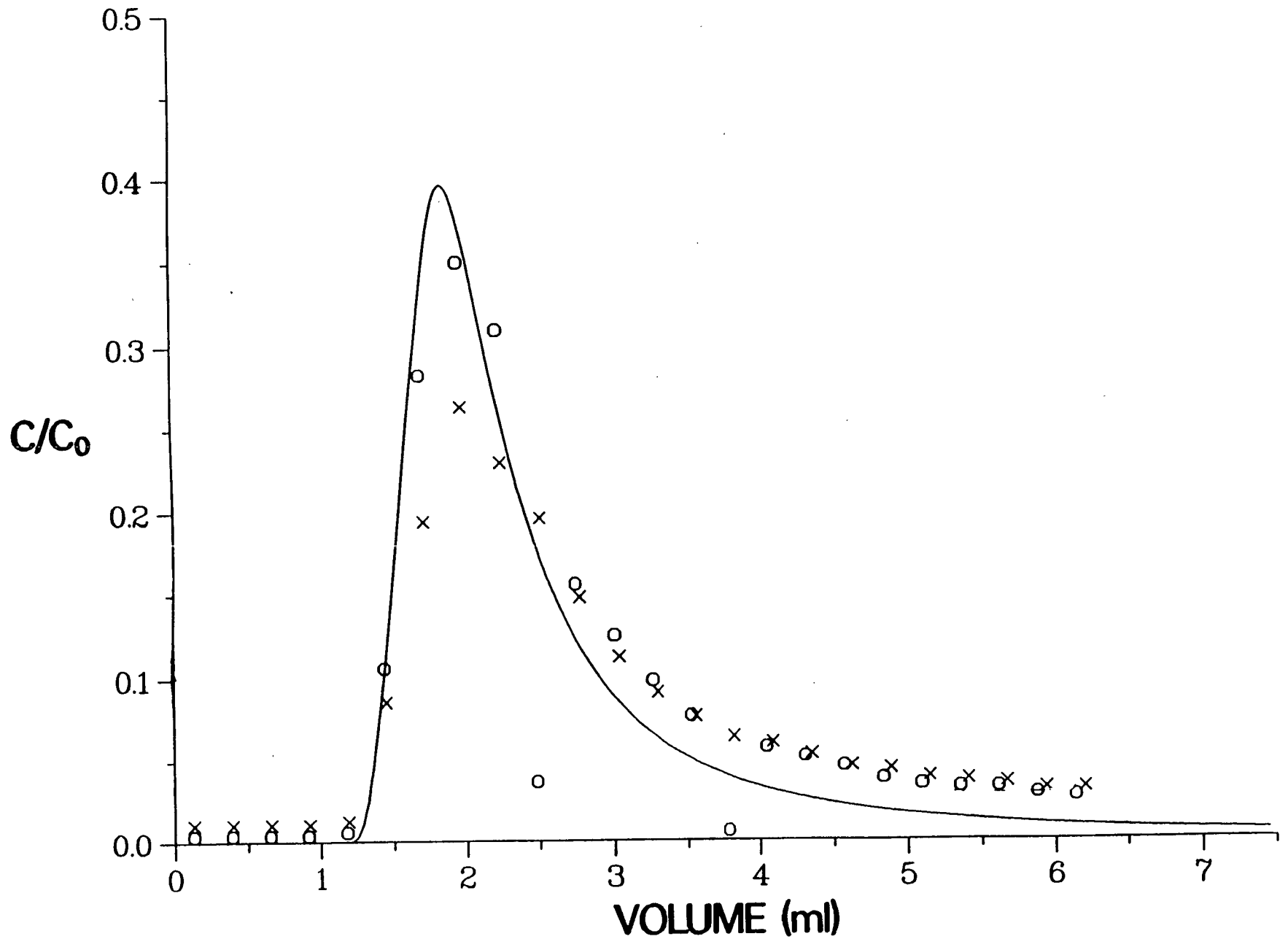
**Tpt SRC 1 TRITUM RUN
FICKIAN DISPERSION
(BEST FIT)**



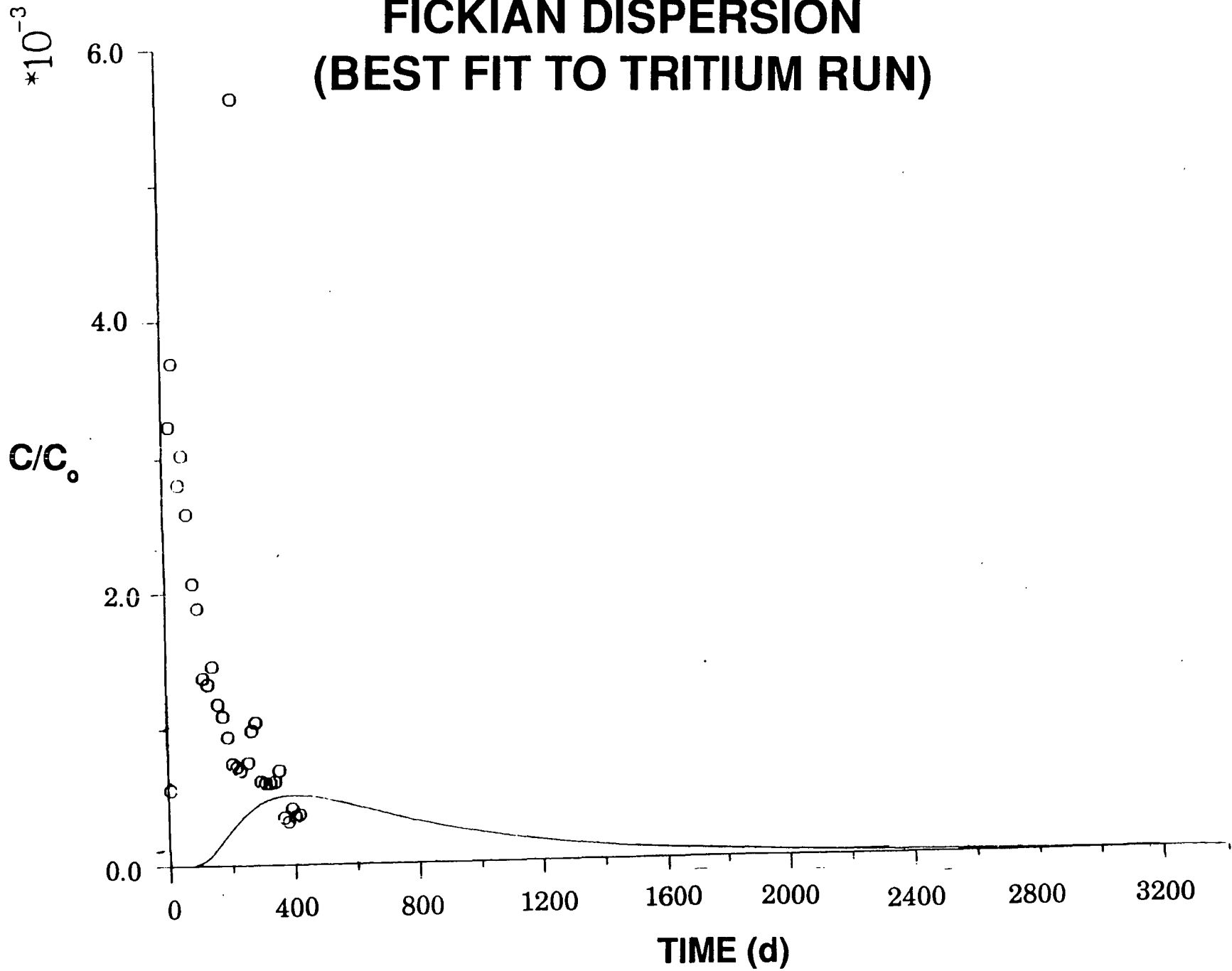
Tpt OUTCROP SRC 1 TRITIATED WATER RUNS
NON-FICKIAN DISPERSION
(BEST FIT)



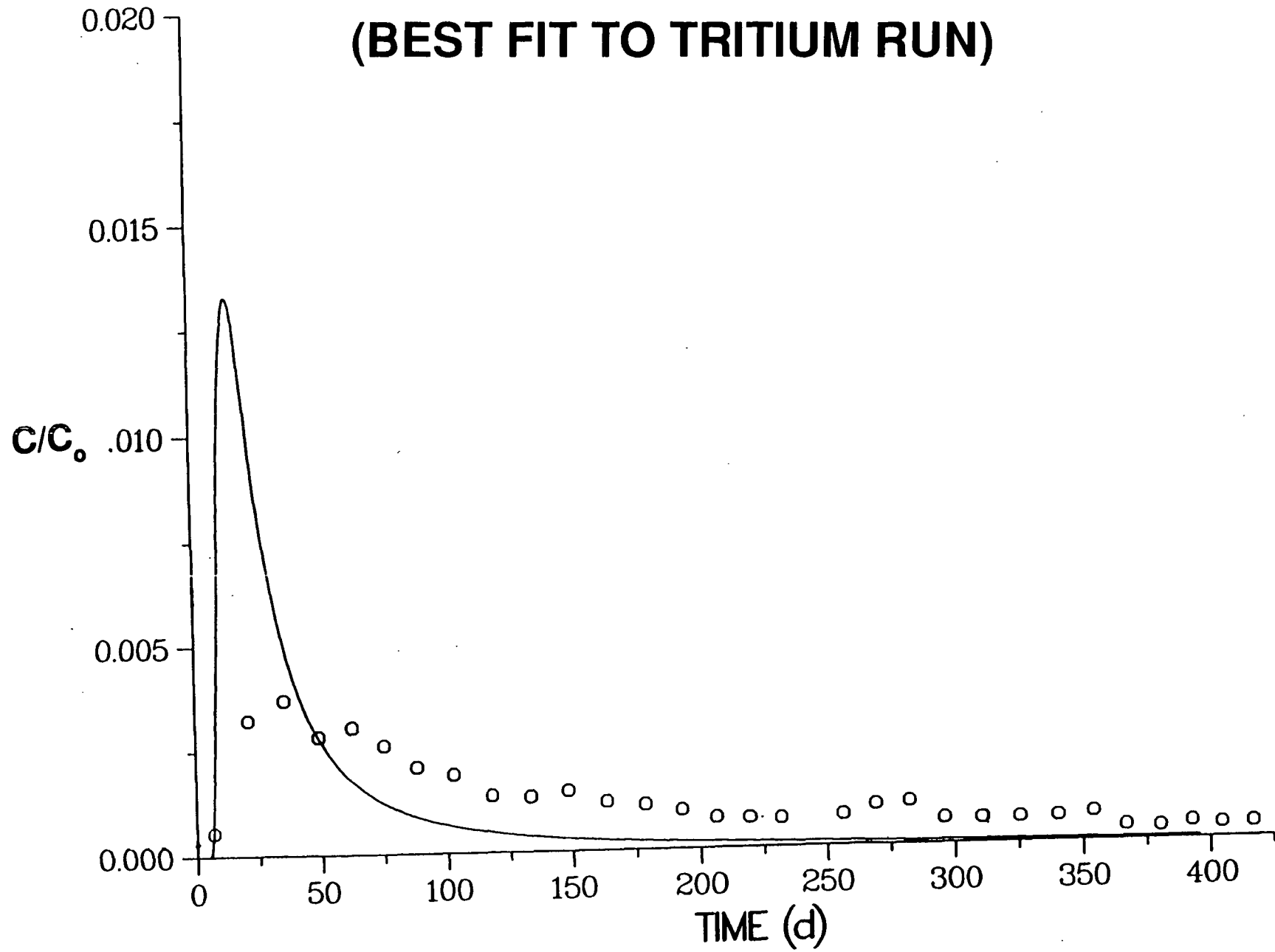
Tpt OUTCROP SRC 1 PERTECHNETATE RUNS



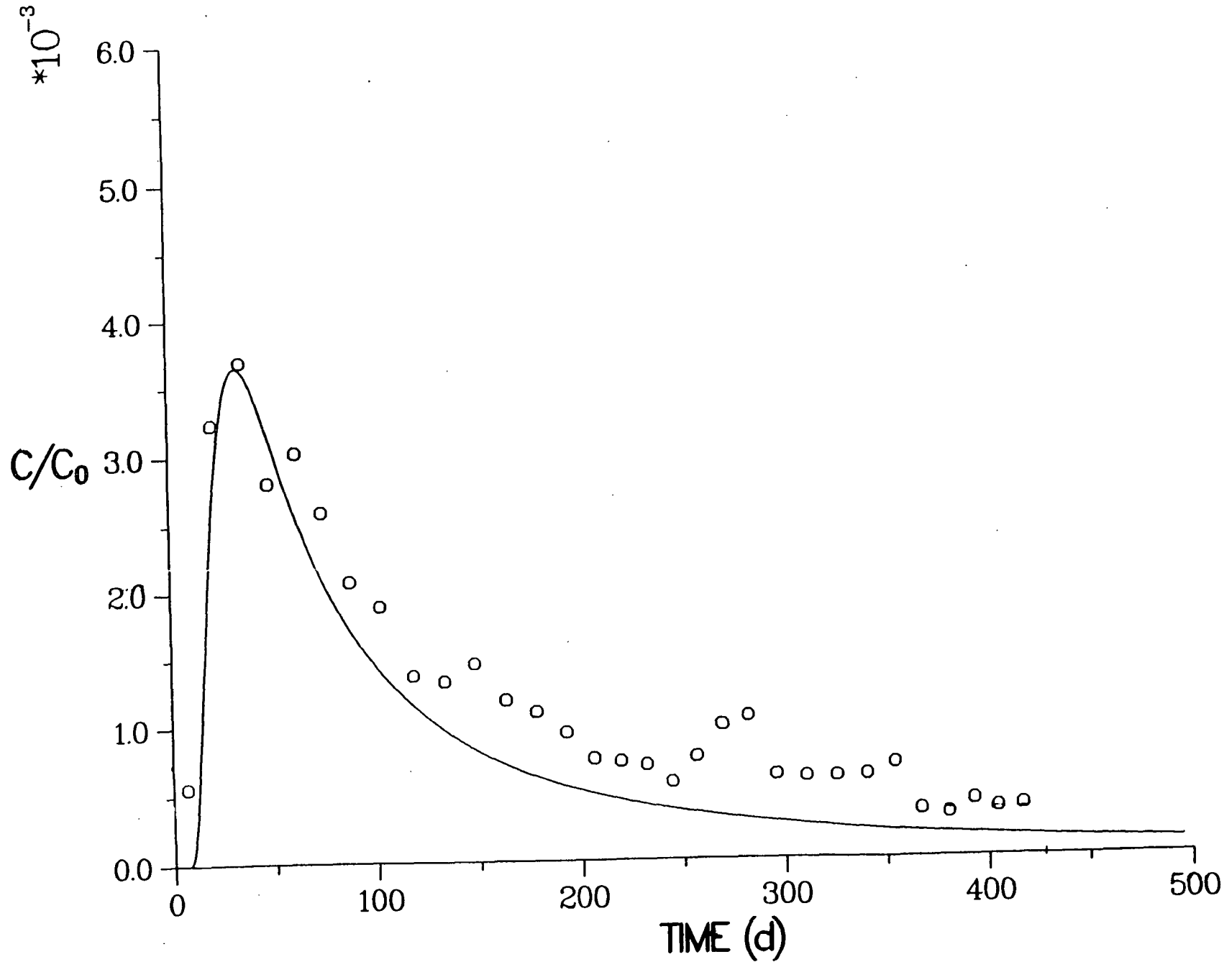
Tpt OUTCROP SRC 1 STRONTIUM RUN FICKIAN DISPERSION (BEST FIT TO TRITIUM RUN)



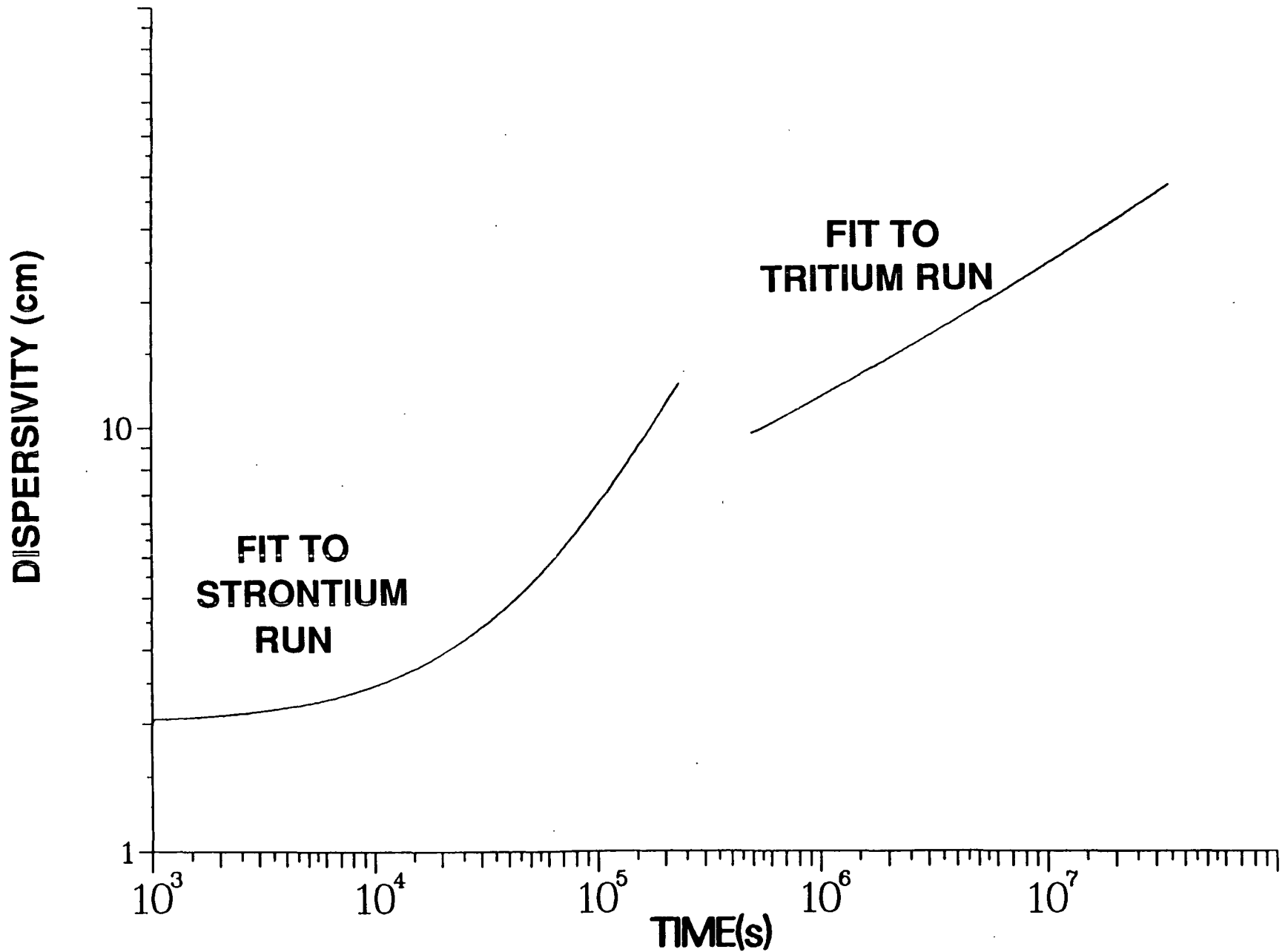
**Tpt OUTCROP SRC 1 STRONTIUM RUN
NON-FICKIAN DISPERSION
(BEST FIT TO TRITIUM RUN)**



Tpt OUTCROP SRC 1 STRONTIUM RUN NON-FICKIAN DISPERSION



DISPERSIVITY vs TIME (TOPOPAH SRC 1)



INTACT TUFF COLUMNS: CONCLUSIONS

- DISPERSIVITIES ARE LARGE AND APPEAR TIME DEPENDENT FOR POROUS FLOW THROUGH INTACT DENSELY WELDED TUFF
- PEAK ARRIVALS FOR SORBING TRACER APPEAR MUCH EARLIER THAN EXPECTED FROM BATCH SORPTION K_d 'S UNLESS TIME DEPENDENT DISPERSION IS INVOKED
- RADIOASSAYS OF COLUMN SECTIONS EXHIBIT NONUNIFORM SORPTION OF RADIONUCLIDES
- PERTECHNETATE RETAINS THE SAME DISPERSION AS TRITIATED WATER, BUT THERE IS A LOSS OF TRACER IN THE FRAN RIDGE OUTCROP SAMPLES
- PERTECHNETATE HAS A MUCH GREATER DISPERSION THAN TRITIATED WATER, BUT THERE IS NO LOSS OF TRACER IN THE CALICO HILLS SAMPLES
- HETEROGENEITY IS AN IMPORTANT FACTOR EVEN AT THE LABORATORY SCALE

CONCLUSIONS

- **BATCH R_d MEASUREMENTS AUGMENTED BY ISOTHERM AND MECHANISTIC STUDIES SHOULD YIELD A DEFENSIBLE DATABASE FOR USE IN PERFORMANCE ASSESSMENT CALCULATIONS**
- **LARGER SORPTION COEFFICIENTS MAY BE REQUIRED TO MITIGATE THE EFFECTS OF DISPERSION IF THE GEOCHEMICAL BARRIER IS TO FUNCTION EFFECTIVELY**