

**U.S. DEPARTMENT OF ENERGY
OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT**

**NUCLEAR WASTE TECHNICAL REVIEW BOARD
FULL BOARD MEETING**

**SUBJECT: INTEGRATED REPORT ON SNL AND
M&O TOTAL SYSTEM PERFORMANCE
ASSESSMENTS: FOCUS ON
WHAT WAS LEARNED**

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**ARLINGTON, VIRGINIA
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Outline

- **Use of two approaches (SNL & M&O)**
- **Thermal loading**
- **Mode of emplacement and design alternatives**
- **General compliance**
- **Dose versus Complementary Cumulative Distribution Function (CCDF)**
 - **Technical challenges of dose calculations**
 - **Are insights different?**
- **Performance period**

**Use of Two Approaches:
Sandia National Laboratories (SNL) &
Management & Operating Contractor (M&O)**

Benefit of Dual Effort

- **Total System Performance Assessments (TSPAs) are complex undertakings**
 - **Opportunities for the analyst to influence the outcome**
 - **Analysts must make simplifying (abstracting) assumptions**
 - **Abstractions should reflect correct understanding of the physical system and reasonable data interpretation**

Benefit of Dual Effort

(Continued)

- **International Transport Code Intercomparison (INTRACOIN) exercise lessons:**
 - **Codes embodying the same conceptual model, but using different numerical techniques may yield comparable results for the same person**
 - **But they generally do not yield comparable results because of analysts' need to interpret the physical system; (both its initial and its boundary conditions)**
 - **Data sets generally do not allow unambiguous specification of these judgment-based model inputs**
 - **The analysts' experience and understanding is vital to the credibility of the analytical results**

TSPA-91: Also a Dual Effort

- **TSPA-91 was a dual effort (Sandia National Laboratories and the Pacific Northwest Laboratory [PNL])**
 - **Two different calculational capabilities were used**
 - **Output results were comparable, where the range of input parameters and major assumptions were comparable**
 - **Built confidence in the analyses, in the results, and in the tools used**

Example of TSPA-91 Benefit from Dual Modeling: Basaltic Volcanism Modeling

- **SNL used a simplified basaltic volcanism model to evaluate releases**
- **PNL used a more mechanistic model**
- **Published estimates for recurrence rates and the mechanics of intrusion were used**
 - **SNL scenarios were based on the work done for the Yucca Mountain Project**
 - **PNL scenarios were based on the more general regional volcanism literature**
- **Results: insignificant releases**

Dual Participation in TSPA-93: Building Credibility and Confidence

First Step: M&O (new team) benchmarking its capability by performing a set of comparative calculations using the RIP code with the TSPA-91 data set

- **This exercise showed the SNL data set, as published, was sufficient to recreate TSPA-91 results**
- **Also showed the RIP code, in the hands of capable analysts**
 - **Could be used to perform TSPAs**
 - **Is flexible**
 - **Can be used for sensitivity studies**
- **Work began early-1993; results published mid-1993**

Dual Participation in TSPA-93: Building Credibility and Confidence

(Continued)

Second Step: Ensure that needless differences in the two analyses would be avoided

- **To the extent practical, the M&O would use results of the extensive SNL data-gathering**
- **The structure of the RIP code, as compared with TSA, dictated differences in use and encoding of some data**
- **The structure of the RIP code, as compared with TSA, also dictated differences in analytical approach**

Dual Participation in TSPA-93: Building Credibility and Confidence

(Continued)

- **TSPA-93, however, was not a re-benchmark of RIP and TSA:**
 - **Purposeful differences in approach retained to assure additional insight into the TSPA problem**
 - **Purposeful differences in cases run retained to ensure additional insight into the problems being addressed**

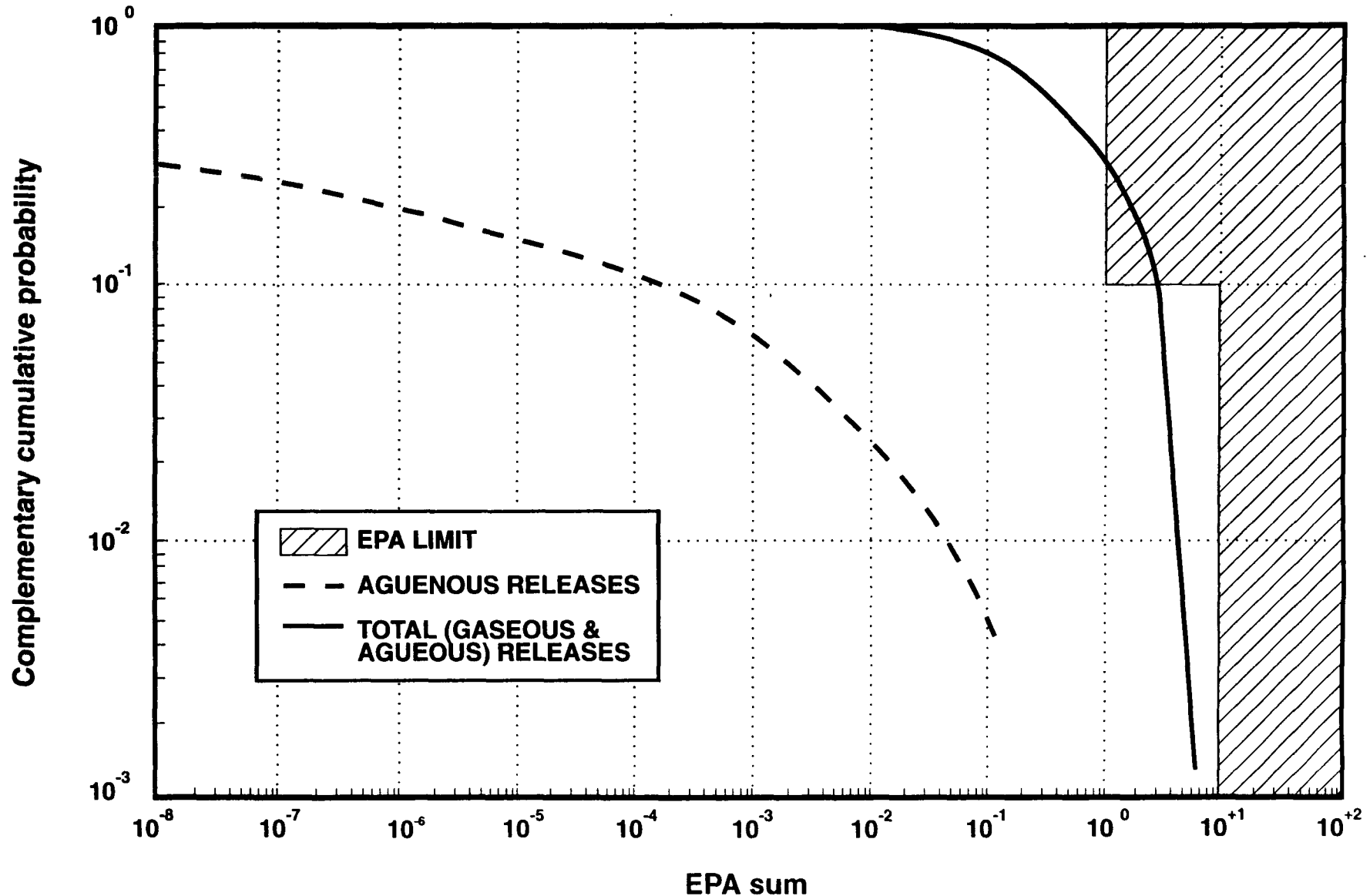
Common and Contrasting Approaches in TSA and RIP for TSPA-93

- **Often, the two codes used the same conceptual approach, but implementation differed in details**
- **Common data, approaches, and implementation contrasts are described in an appendix for**
 - **The approach to the one-dimensional approximation of unsaturated flow and transport**
 - **The composite-porosity conceptual model**
 - **Infiltration/flux distributions and climate change**
 - **Saturated zone flow and transport**
 - **Radionuclide solubilities and distribution coefficients**
 - **Waste package corrosion and near-field characteristics**

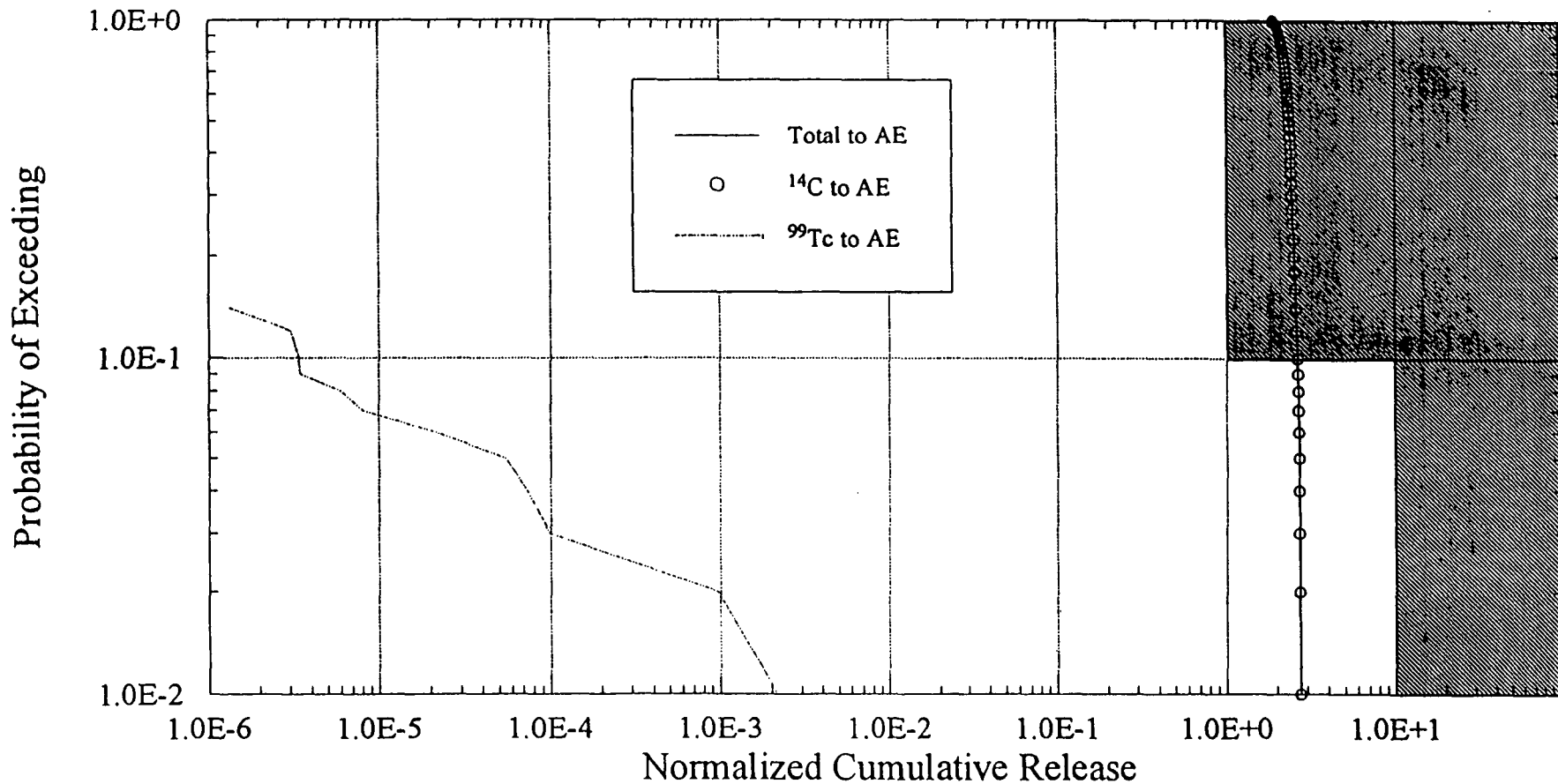
Meaning of SNL and M&O Modeling Differences

- **For the closest comparable cases (see following two viewgraphs) there were no differences in results that would have been meaningful from a compliance-calculation perspective**
- **Given these generally comparable results, it seems prudent that the performance assessment program now directs resources to**
 - **Evaluate the appropriateness of the conceptual model of unsaturated flow in view of alternatives**
 - **Link its modeling more directly to the results coming from the site program, especially its 3-D site-modeling effort**

Schematic of SNL CCDFs of Normalized Cumulative Release over 10,000 Years for Nominal Aqueous and Total Releases (57 kW/Ac; vertical emplacement, composite porosity model)



M&O CCDFs for Normalized Cumulative Releases over 10,000 years for Nominal Aqueous and Gaseous Releases (57kW/acre, 10 cm outer and 0.95 cm inner containers, horizontal emplacement, composite porosity approximation)



Thermal Loading

Thermal Loadings Evaluated

- **M&O analyses were conducted to represent three thermal loads**
 - 70.4 kW/ha (28.5 kW/acre)
 - 141 kW/ha (57 kW/acre)
 - 282 kW/ha (114 kW/acre)
- **SNL analyses evaluated**
 - 141 kW/ha (57 kW/acre)
 - 282 kW/ha (114 kW/acre)

Alternative Designs Investigated in TSPA-93

Vertical emplacement SCP design

alloy 825 @ 0.95 cm

In-drift emplacement MPC

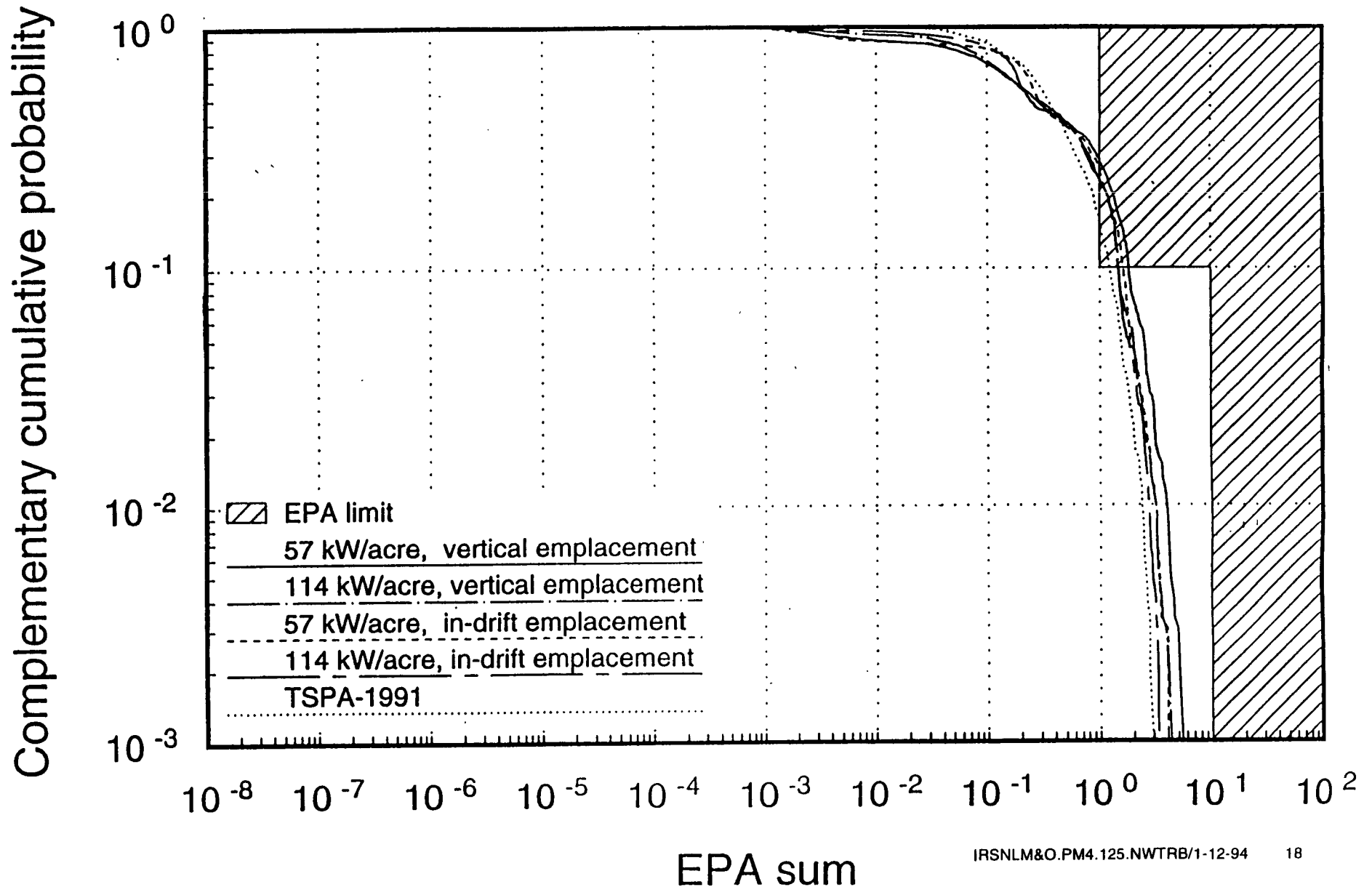
mild carbon steel @ 10, 20, or 45 cm
alloy 825 @ 0.95 cm and 3.5 cm

Alternative Thermal Loads (kW/Ac)		
28	57	114
	✓	✓
✓	✓	✓

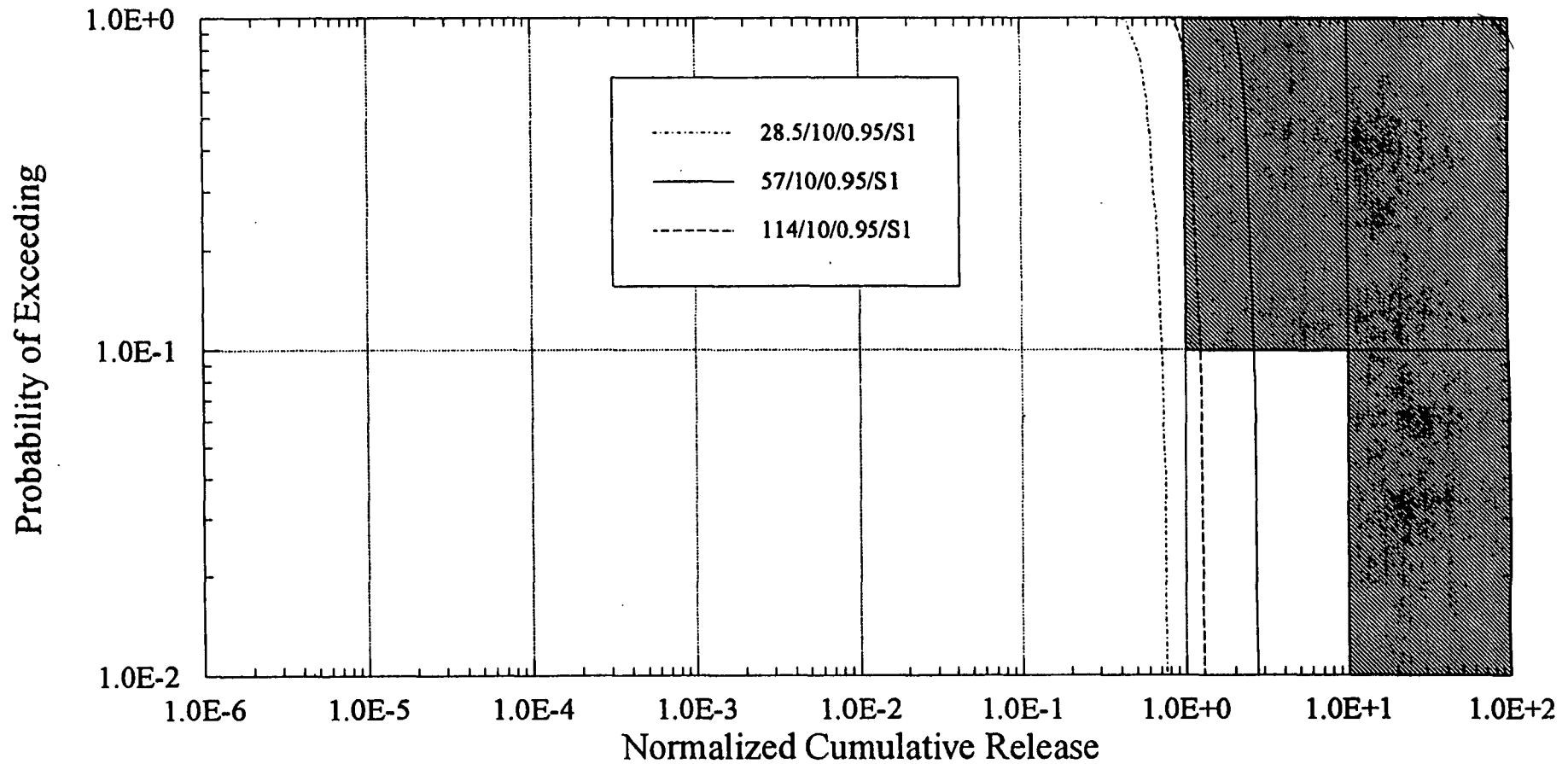
Thermal Loading Results

- **There was little difference between the 57 kW/acre and 114 kW/acre cases for the 10,000-year CCDFs in the SNL analyses**
- **In the M&O analyses, the 28 kW/acre case seemed to give the best performance result, followed closely by the 114 kW/acre case**
- **The apparent differences in performance attributable to thermal loadings directly reflect how much time waste packages spend in the temperature range of 80-100°C, the temperature range, where corrosion rates are highest**
- **Corrosion models used were based on a limited experimental record and expert judgement: work is needed to provide more definitive corrosion models for engineered system materials**

CCDFs of Nominal Cumulative Release (Aqueous and Gaseous) Over 10,000 years for the Four Cases and for TSPA-91



Thermal Loading--100 Realization at 10,000 Years: CCDF of Releases to the AE at 10,000 Years





Mode of Emplacement and Design Alternatives

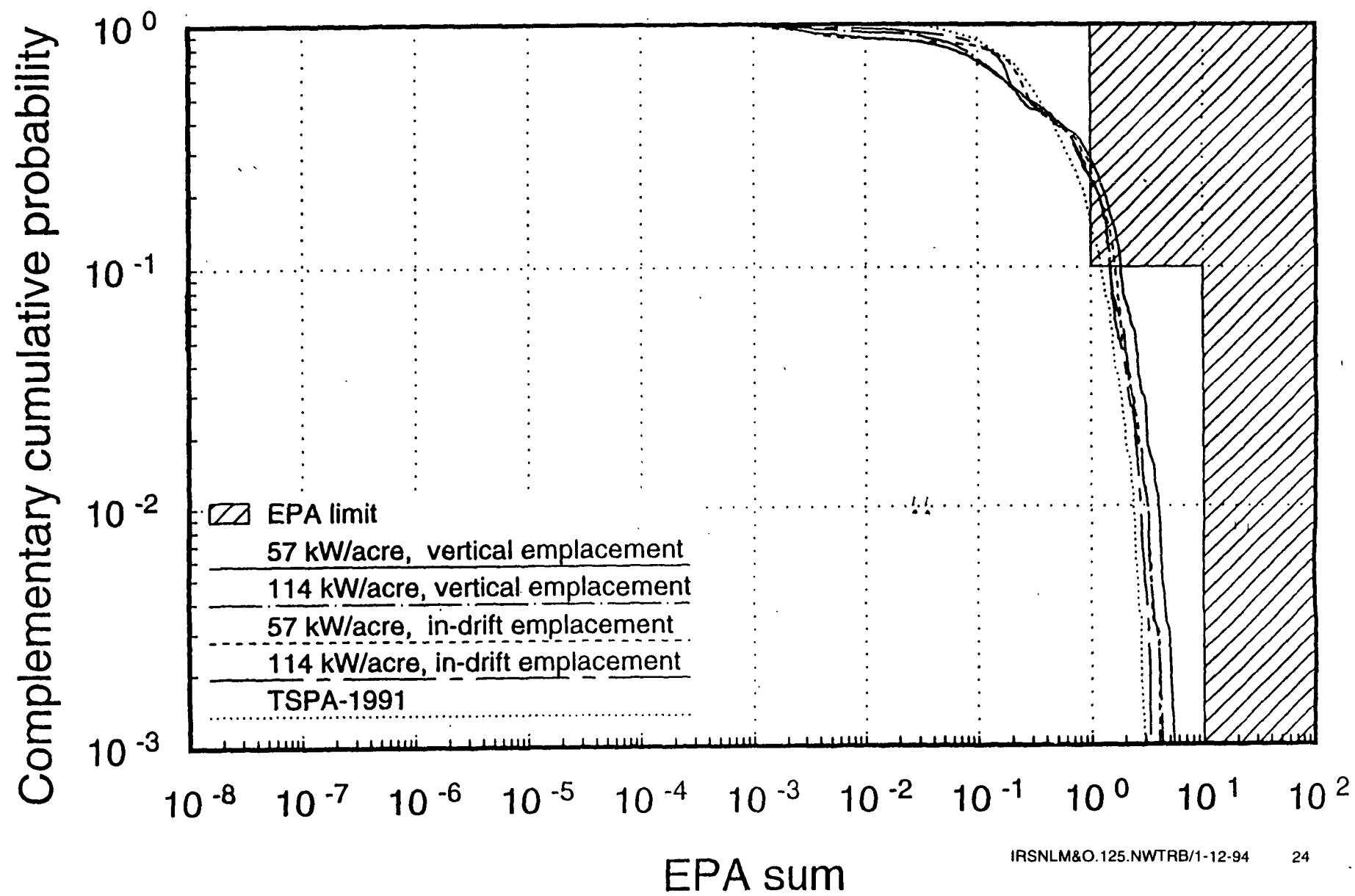
Cutaway of a Drift Showing Comingled Waste Package

Cutaway of a Drift Showing Comingled Waste Package

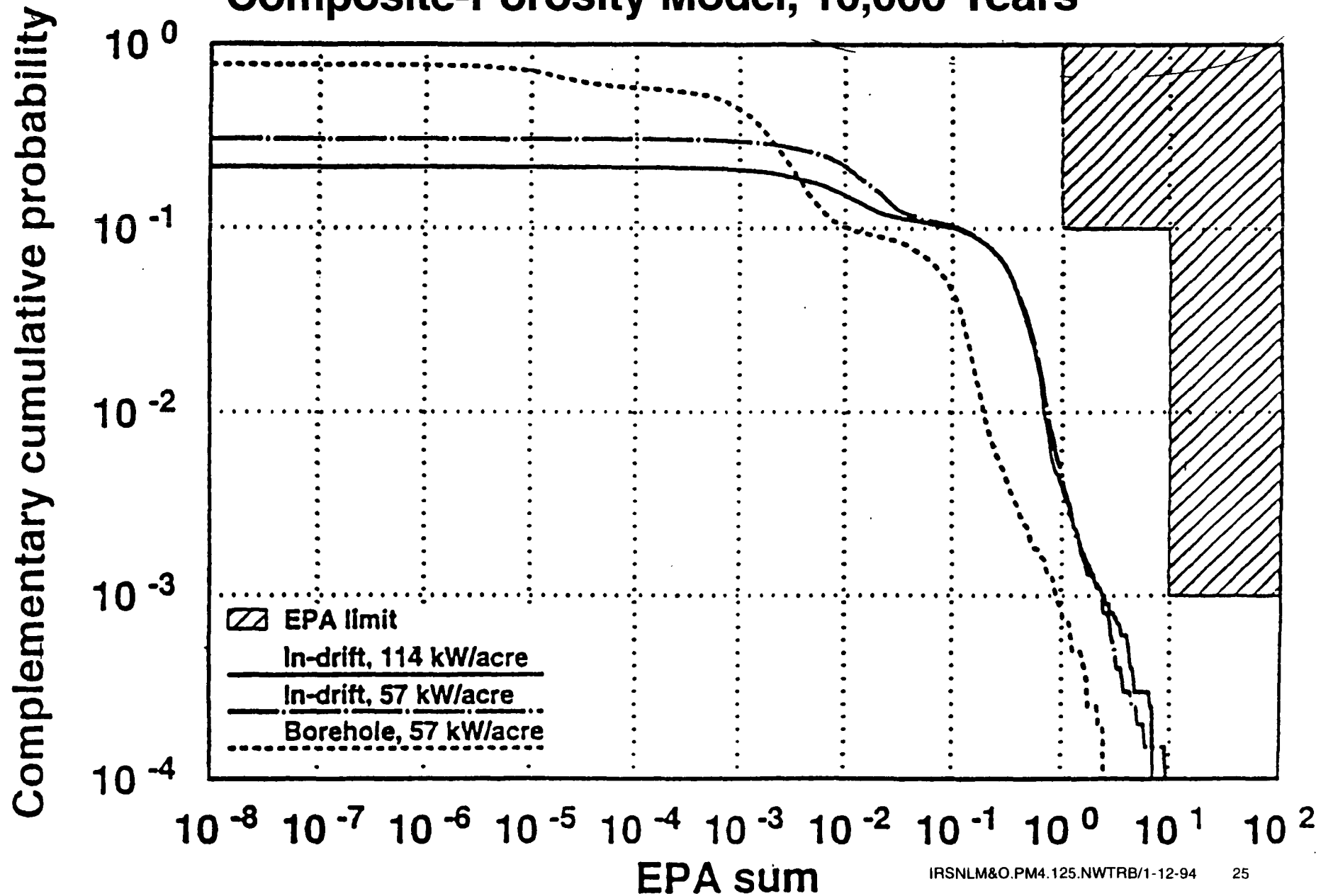
Emplacement Mode

- **Only SNL evaluated emplacement mode, results were non-significant differences in 10,000-year analyses for the nominal case**
- **For the human intrusion scenario analyses, the borehole case performed slightly better simply because of the lesser horizontal area that a vertical package represents as compared with the same package laid horizontally**

CCDFs of Nominal Cumulative Release (Aqueous and Gaseous) Over 10,000 Years for the Four Cases and for TSPA-91



CCDFs of Nominal Cumulative Release for ~~Animal~~ and Human Intrusion Scenarios, Aqueous Pathway, Composite-Porosity Model, 10,000 Years



Waste Package Design Variations

- **M&O addressed the following designs for spent fuel waste packages:**
 - **Three outer corrosion-allowance material thicknesses**
 - **Two inner corrosion-resistant material thicknesses**
- **SNL analyses evaluated the following spent fuel waste packages:**
 - **Two sizes**
 - **Two outer-container wall thicknesses**

Alternative Designs Investigated in TSPA-93

Vertical emplacement SCP design

alloy 825 @ 0.95 cm

In-drift emplacement MPC

mild carbon steel @ 10, 20 or 45 cm
alloy 825 @ 0.95 cm and 3.5 cm

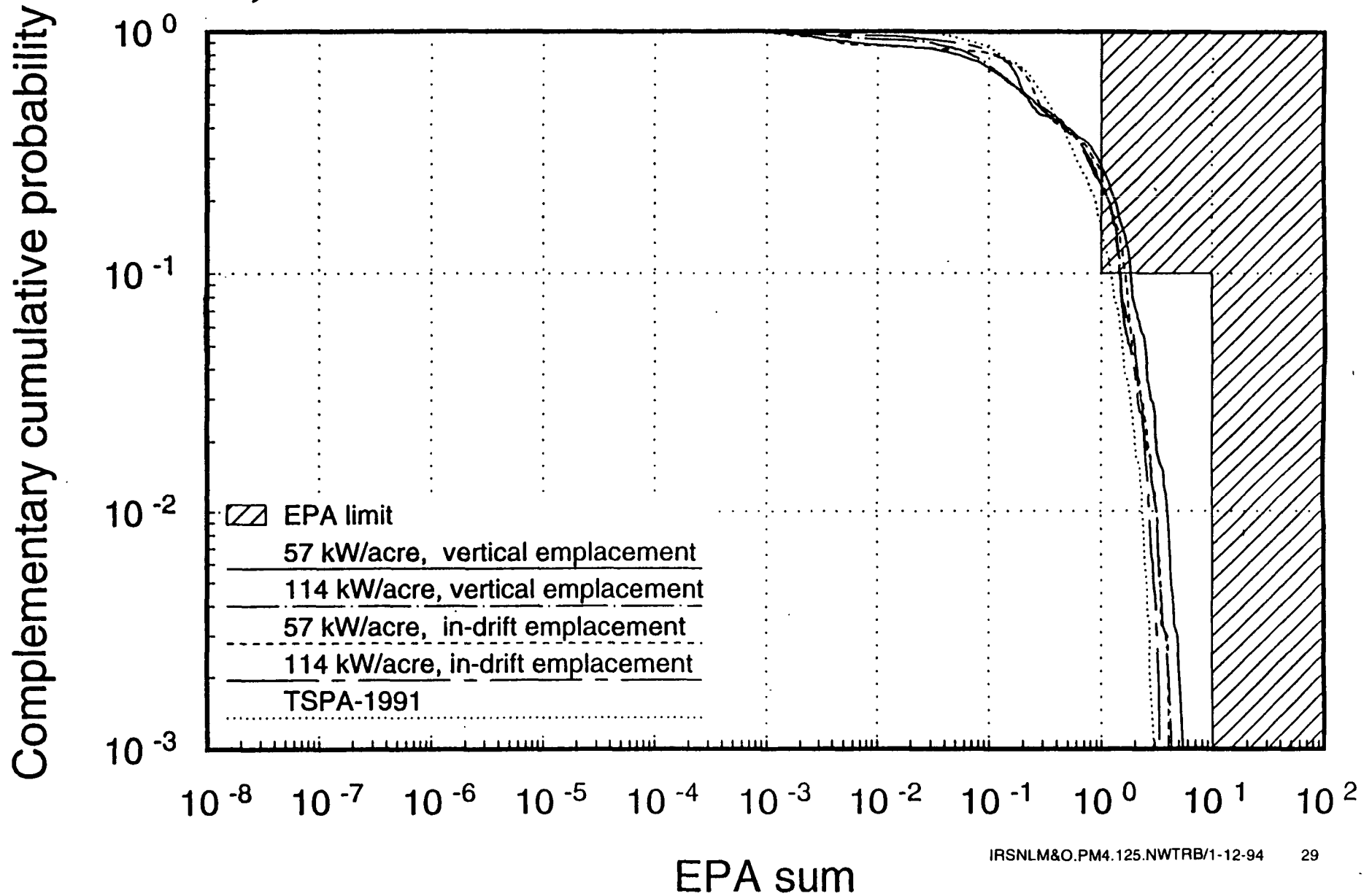
Alternative Thermal Loads (kW/Ac)		
28	57	114
	✓	✓
✓	✓	✓

Waste Package Design

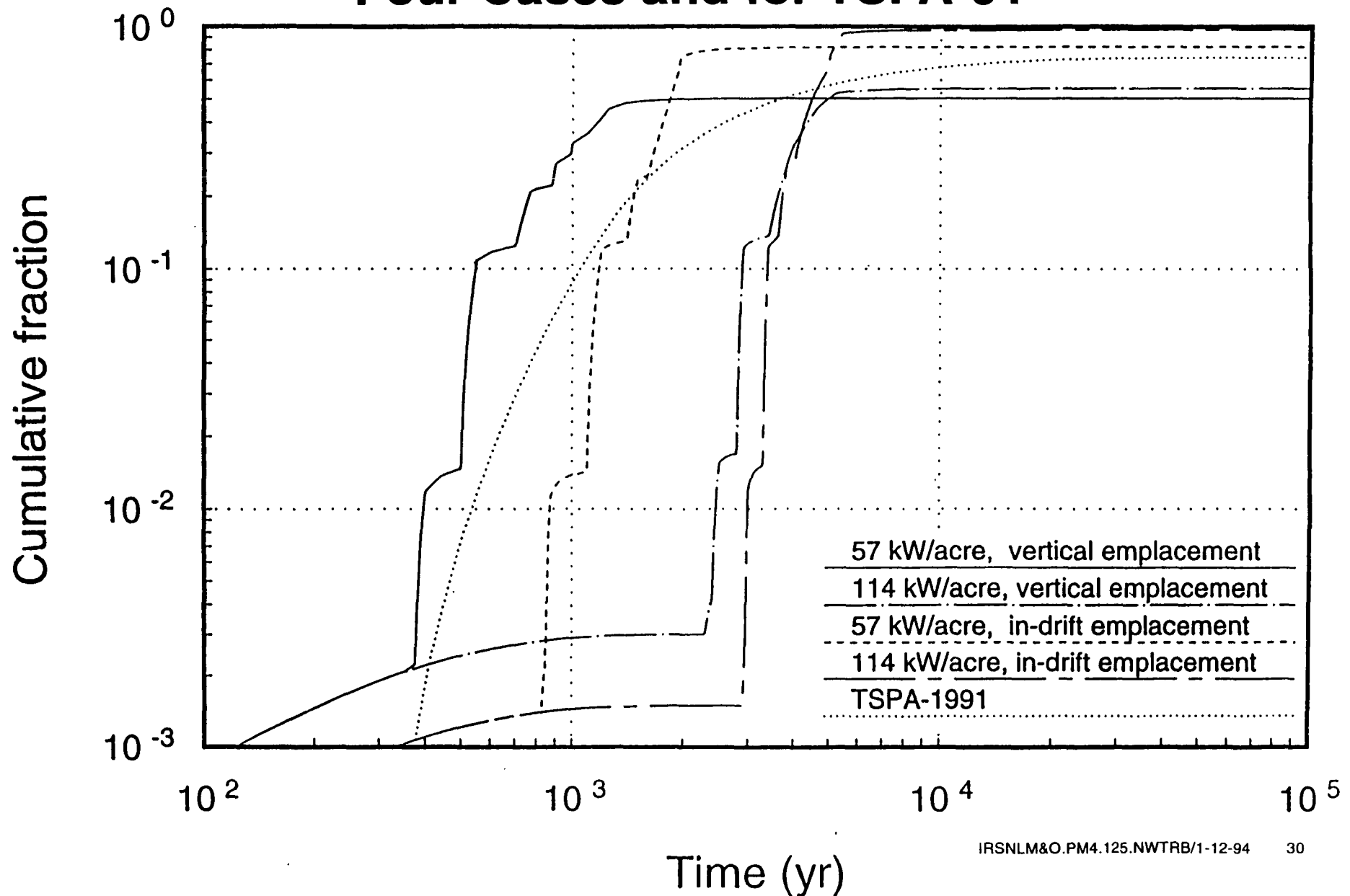
- **In terms of design, the SNL emplacement mode determined whether or not the waste package was 0.95 cm alloy 825 (borehole) or had an additional 10 cm overpack (in-drift)**
 - **Although there were differences in cumulative waste-package failure distributions, these differences were not significant in terms of 10,000-year cumulative releases**
- **M&O analyses addressed additional overpack thicknesses of 20 and 45 cm, and for the 10 cm case, a thicker inner barrier (3.5 cm)**
 - **Only the 45 cm mild steel overpack had a significant impact on performance up to 100,000 years**

CCDFs of Nominal Cumulative Release (Aqueous and Gaseous)

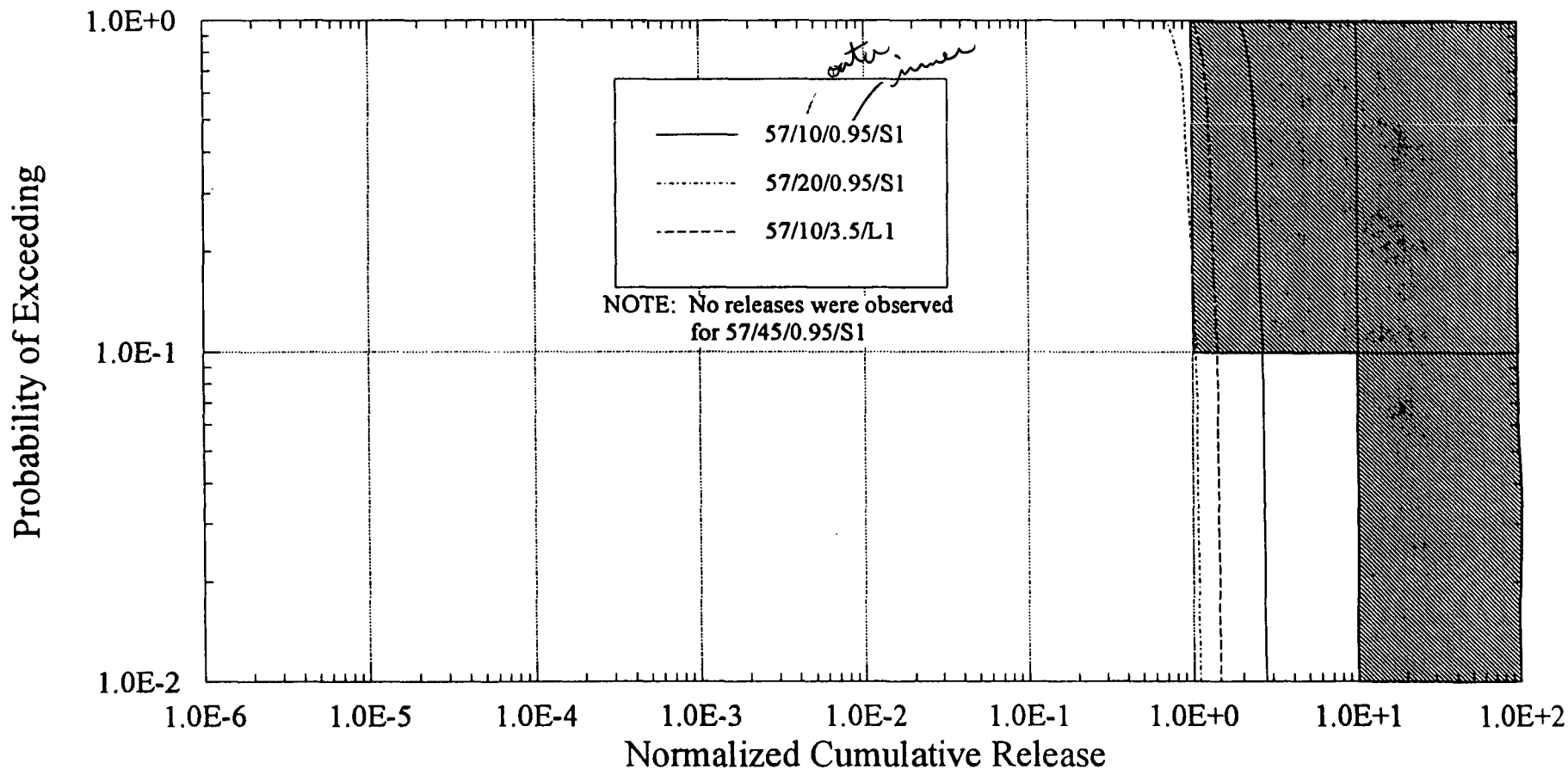
Over 10,000 Years for the Four Cases and for TSPA-91



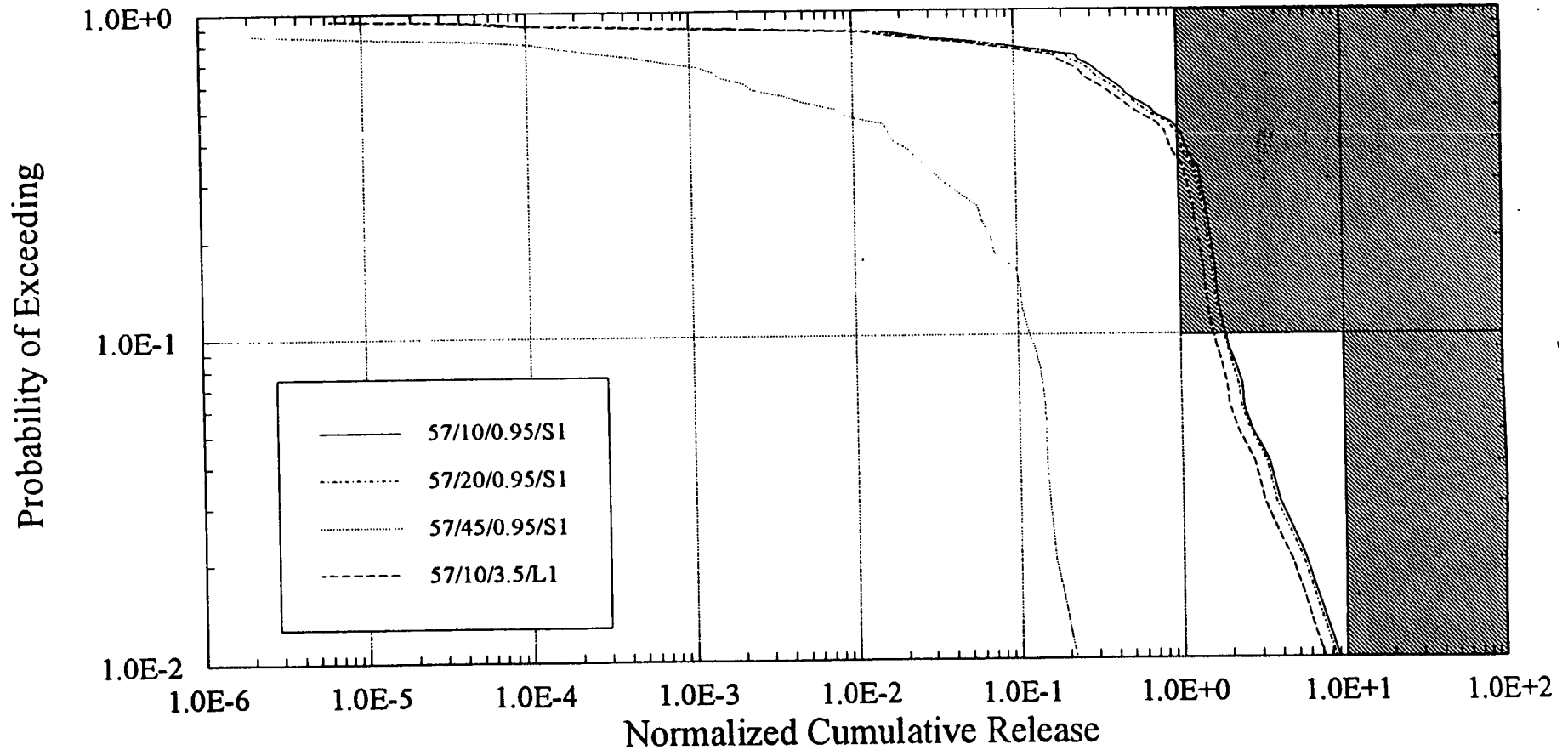
Distribution of Container-Failure Time for the Four Cases and for TSPA-91



Container Thickness--100 Realizations at 10,000 Years: CCDF of Releases to the AE at 10,000 Years



Container Thickness--100 Realizations at 100,000 Years: CCDF of Releases to the AE at 100,000 Years





General Compliance

Compliance with 40 CFR Part 191 and 10 CFR Part 60

- **The Environmental Protection Agency's general environmental standard (not currently applicable to Yucca Mountain)**
 - **Aqueous releases generally were five orders of magnitude below requirements**
 - **Gaseous releases of C-14 generally violated requirements**
- **The Nuclear Regulatory Commission's 10 CFR 60.112 engineered barrier system requirements were not evaluated in TSPA-93**

Dose versus Complementary Cumulative Distribution Function (CCDF)

- **Are insights different?**

Significance of Parameters for Release and Dose Results

- **Key site issue is conceptual model for flow and transport through fractured-porous media and the magnitude of unsaturated zone percolation flux**
- **Most analyses of the hydrologic flow regime in the unsaturated zone (whether ambient or thermally perturbed) assume composite porosity flow model**
- **Validity of this assumption and its impact on predicted performance should be more rigorously evaluated**

Significance of Parameters for Release and Dose Results

(Continued)

- **The representation of the possible increase in flux that may be attributable to future climate changes is uncertain and important to either result**
- **Secondary effects of climate change: increased saturated zone flux and mixing depth are important to dose**
- **Doses from gaseous release of C-14 to accessible environment not evaluated in terms of dose in TSPA-93**

Dose versus Complementary Cumulative Distribution Function (CCDF)

Technical Challenges of Dose Calculations

Saturated Zone is of Particular Significance to Dose Results

- **Aqueous release to accessible environment relatively insensitive to flow in the saturated zone**
 - **Unsaturated zone travel-time long compared to saturated zone travel-time**
- **Doses from aqueous releases at the accessible environment directly related to the flux through the saturated zone**
 - **If a dose-based standard is promulgated, a greater understanding of the saturated zone will be required**

Biosphere Modeling Necessary for Definitive Dose Calculations

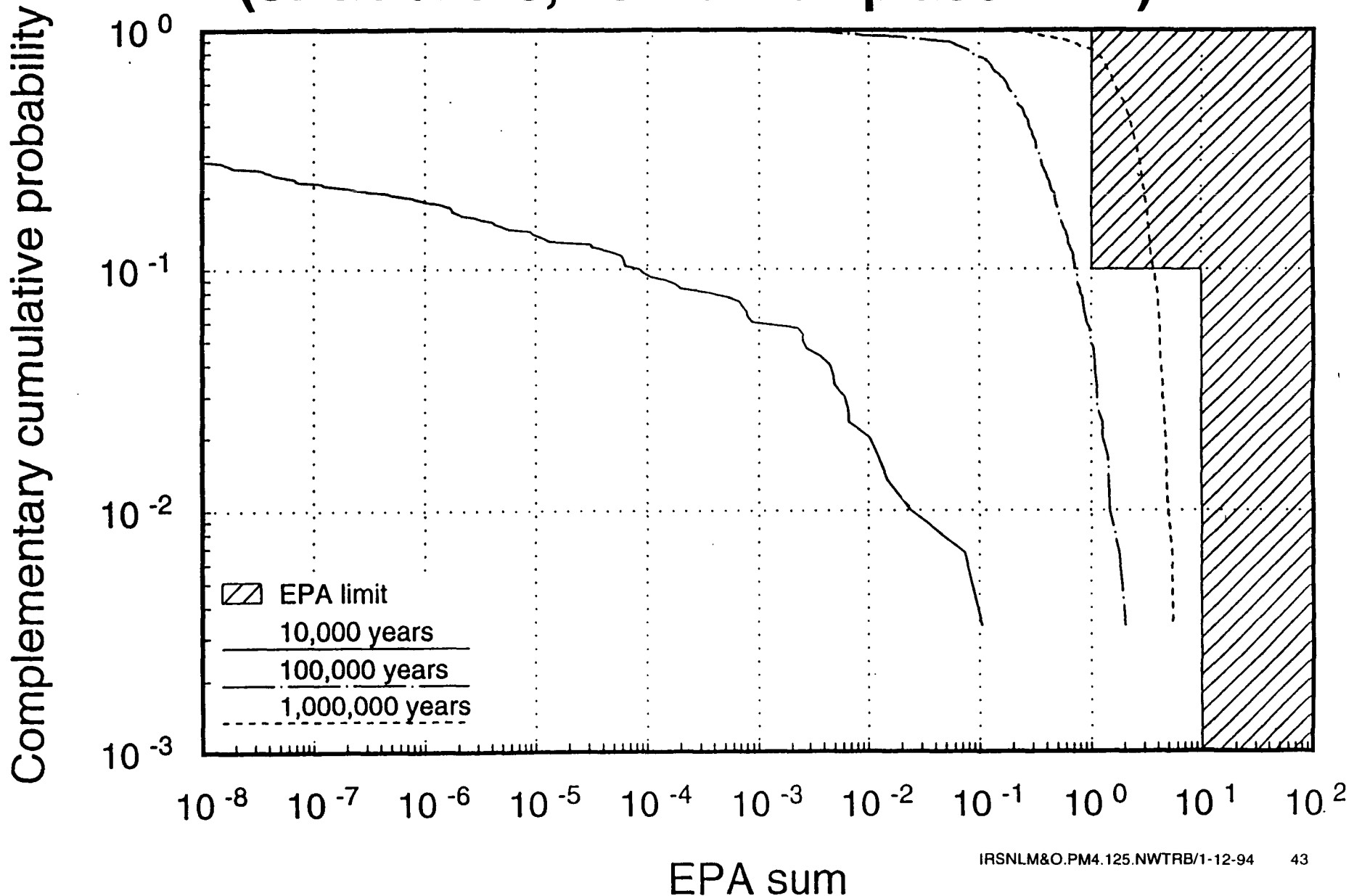
- **Biosphere modeling needs to address climate change and human development**
- **Reference biospheres specific to Yucca Mountain, over time, would be needed**
- **A comprehensive list of features, events, and processes (FEPs) of relevance for biosphere modeling would need to be developed**
- **Defensible method must be used for screening and combining FEPs into biosphere models**
- **There may be greater uncertainty in long-term biosphere modeling than in geosphere modeling**

Performance Period

Reasons for Conducting Analyses Over Time-Periods Greater than 10,000 Years

- **Evaluate consequences associated with long-lived radionuclides not released in 10,000 years**
- **Provide "better insight on the long-term performance of disposal alternatives"**
- **Compare results with other countries that consider dose over longer time-periods**
- **Prepare for discussions with the National Academy of Sciences Committee on the Review of Applicable Standards for Yucca Mountain**

Distribution of Cumulative Aqueous Release (57 kW/acre, vertical emplacement)



When Considering the 10,000 Yr Time-Period

- **Virtually all (greater than 99.99%) of the release to the accessible environment is the result of C-14**
- **Cumulative aqueous release to the accessible environment has about a 90% probability of being less than 10^{-6} of the EPA limit**
- **Aqueous releases are generally insignificant over 10,000 years, but are very sensitive to the percolation flux and the conceptual model for fracture-matrix interaction**

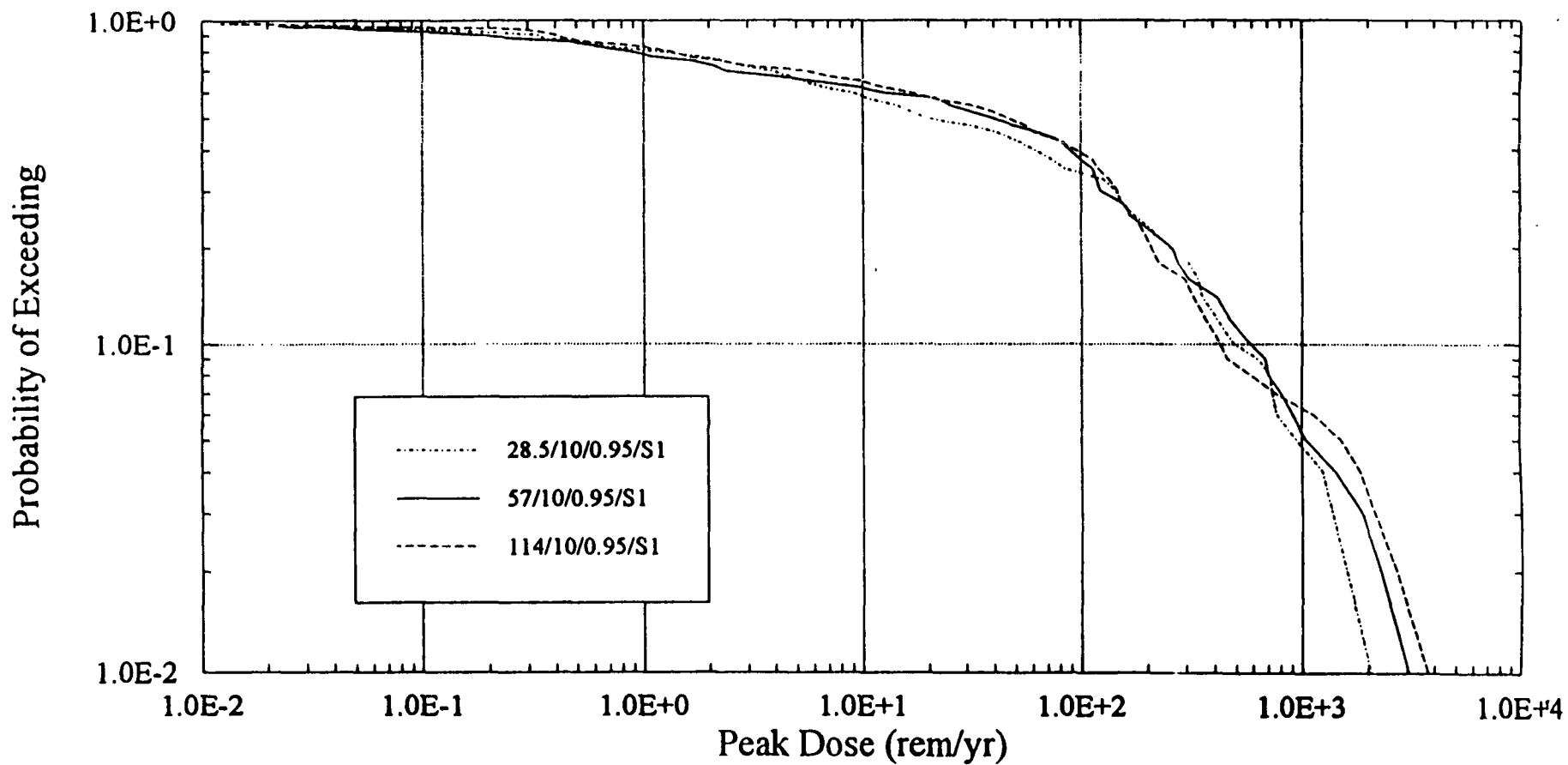
For the 100,000 Yr Time-Period

- **Gaseous release accounts for half of total release**
- **Remainder is provided by unretarded aqueous species, primarily ^{99}Tc**
- **Generally, cumulative aqueous radionuclide release over 100,000 years is insensitive to the thermal load and outer barriers less than 20 cm**
- **Outer barriers on the order of 45 cm, especially when combined with low thermal loads, yield 100,000 yr waste package**

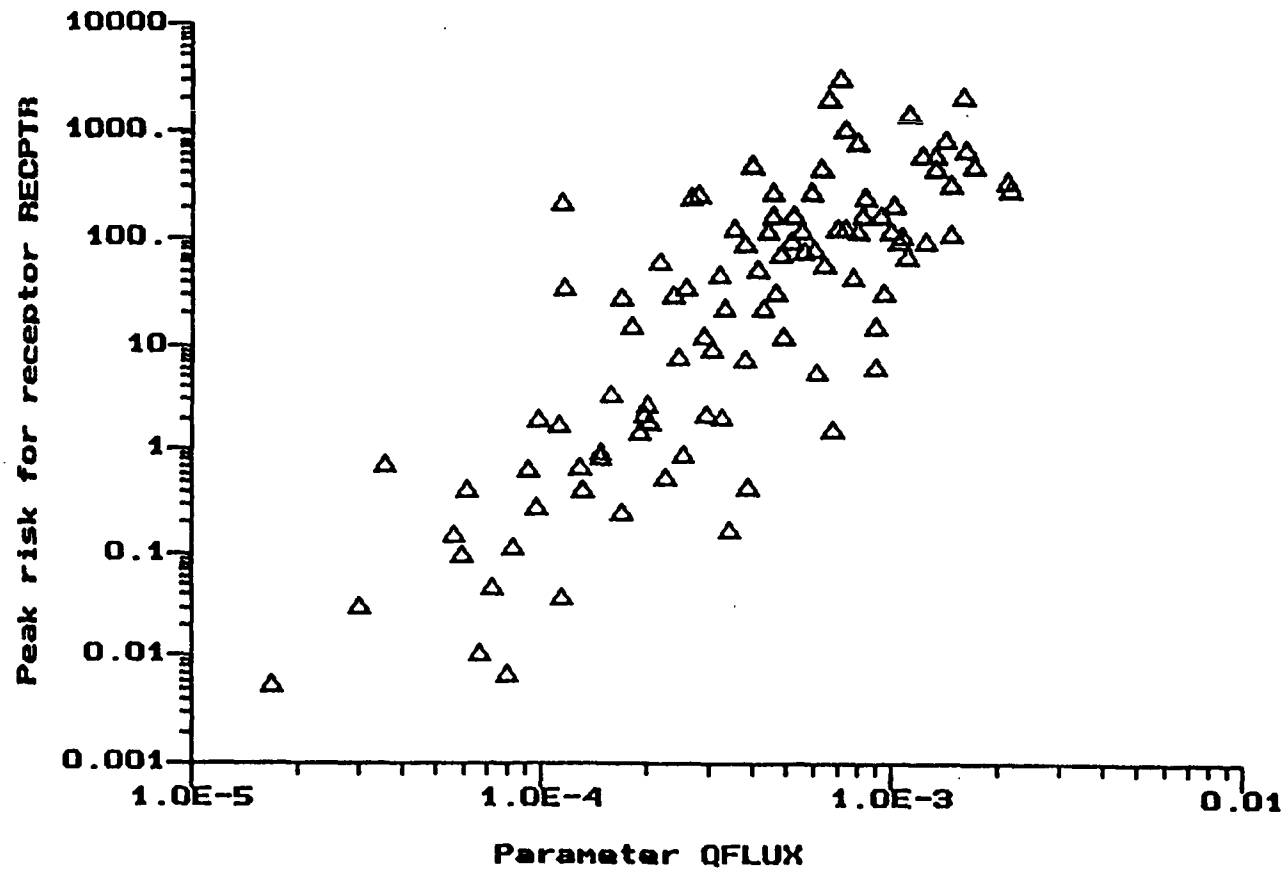
Doses Over the 1,000,000 Yr Time-Period

- **Peak doses generally attributable to ^{237}Np**
- **Where this is not the case, either there is low flux through the unsaturated zone, high Np retardation, or low Np solubility**
- **Peak dose over 1,000,000 years is insensitive to thermal loads and waste package design**
- **Peak dose is sensitive to saturated-zone mixing depth**
- **Dose also sensitive to dose-conversion factors**

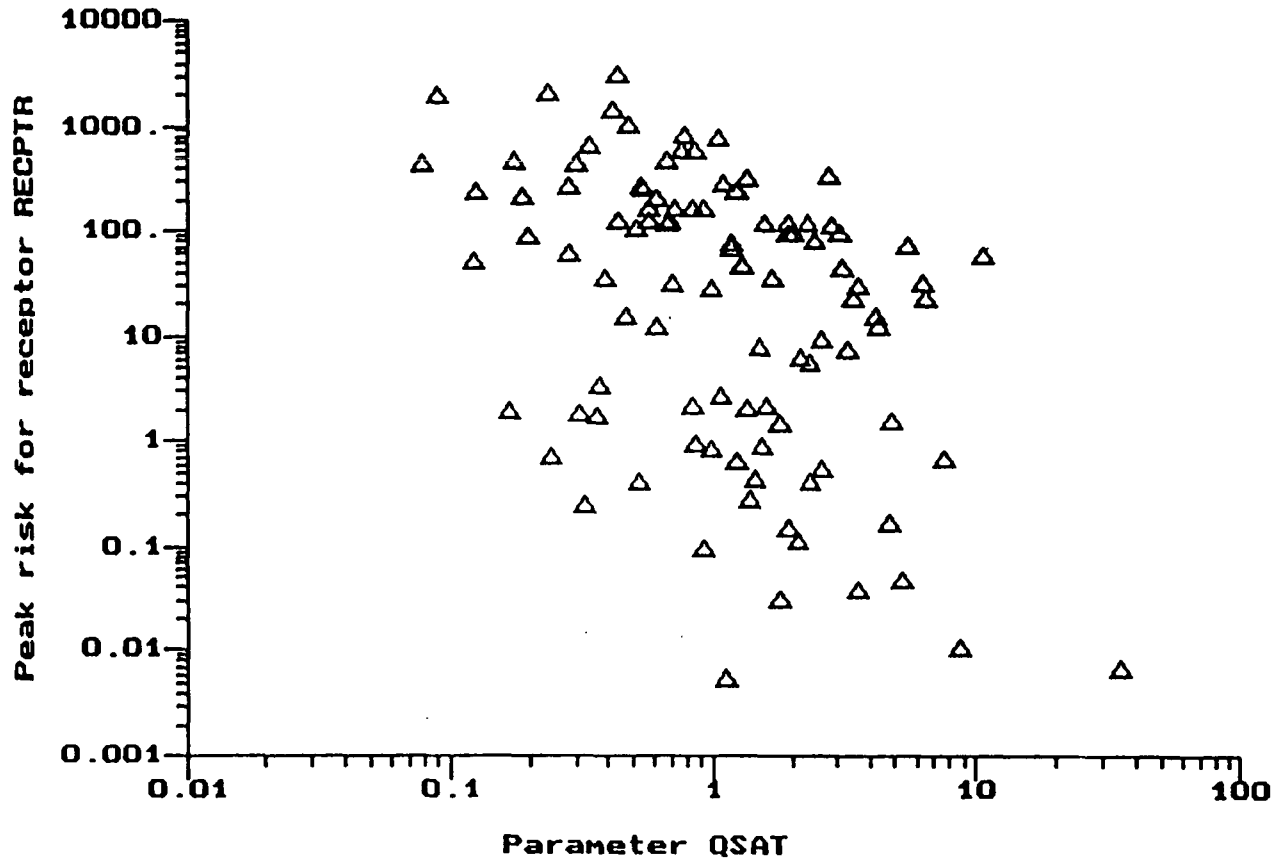
Peak Dose up to 1,000,000 Yrs: Alternate Thermal Loads



Sensitivity of Peak Dose to Percolation Flux



Sensitivity of Peak Dose to Saturated Zone Flux



Appendix

Common and Contrasting Approaches in TSA and RIP for TSPA-93

- **Often, the two codes used the same conceptual approach, but implementation differed in details**
- **Common: one-dimensional approximation of unsaturated zone flow and transport problem, with implementation contrasts**
 - **TSA used 8 and 5 flow tubes, respectively, for modeling releases from representative locations for the lower and higher thermal-loading cases**
 - **RIP used 9 flow tubes to model releases from spent fuel and high-level waste containers**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

- **Common: Composite-porosity conceptual model, with implementation contrasts:**
 - **TSA is capable of invoking a separate "Weeps" fracture-flow conceptualization, with no matrix flow**
 - **TSA assumed fracture flow when the flux value of an iteration exceeded a probabilistic value of Topopah Spring saturated matrix conductivity**
 - **RIP allowed matrix flow to continue regardless of flux**
 - **TSA used slightly higher dispersion values than RIP**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

- **Common: Exponential initial infiltration distribution with a mean of 0.5 mm/yr with implementation contrasts:**
 - **TSA wetter climate, with a probability of 1 over 100,000 yrs, multiplies initial distribution by 20**
 - **RIP wetter climate, a linear increase culminating in a 3-fold multiplication of the initial distribution**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

- **Common: Saturated-zone flow and transport modeling basis, with implementation contrasts:**
 - **TSA used the midpoint of breakthrough curve arrival times in SNL three-dimensional saturated-zone flow and transport analyses to calculate effective velocities**
 - **RIP directly used velocities from the same SNL calculations**
 - **TSA sampled from an linear distribution of vertical mixing depths from 10 to 500 m**
 - **RIP used a single value of 50 m**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

- **Common: Radionuclide solubilities and distribution-coefficients with implementation contrasts:**
 - **TSA: distribution used as obtained from expert elicitation**
 - **RIP: solubility distributions corrected for temperature and pH**
- **Common: Gas flow and transport modeling basis (work by Ross, under SNL contract), with no significant implementation contrasts**
- **Common: Dose modeling basis (conversion factors used in TSPA-91) with no implementation contrasts**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

Near-field implementation contrasts:

- **Inventory for aqueous release**
 - **TSA: 8 radionuclides adjusted for ingrowth prior to analysis (no chains)**
 - **RIP: 39 radionuclides; 4 decay chains**
- **Aqueous release and transport**
 - **TSA: release dependent on spatially variable flux**
 - **RIP: release diffusion controlled, activated by liquid saturation of >8%**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

Very near-field characteristics contrasts:

- **TSA: backfill, higher temperatures, dry oxidation**
- **RIP: no backfill, lower temperatures, no dry oxidation**
- **TSA: if temperature $> 100^{\circ}\text{C}$, no liquid water, no corrosion**
- **RIP: liquid water present above 100°C , corrosion if liquid saturation $> 8\%$ (sensitivity studied)**
- **TSA: pitting corrosion rate defined by mean of higher of three growth rate LLNL distributions**
- **RIP: pitting corrosion rate varied over the range of the middle of these same three distributions**

Common and Contrasting Approaches in TSA and RIP for TSPA-93

(Continued)

- **M&O TSPA-93 did not consider human intrusion or volcanic disruption**
- **SNL TSPA-93 did consider human intrusion and volcanic disruption**
- **SNL and M&O relied on input from data interpretation and detailed modeling conducted by other participants, including LLNL, LANL, USGS, SNL, and M&O**