

**SELENITE TRANSPORT IN
UNSATURATED TUFF
FROM YUCCA MOUNTAIN**

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OUTLINE

- **Determination of Transport Parameters Using UFA**
- **UFA Validation Experiments**
- **Tuff Hydraulic Conductivity as a Function of Water Content**
- **Fracture Flow in Tuff**
- **Batch Sorption Studies and UFA Retardation Tests**
- **Summary**

UNSATURATED FLOW APARATUS (UFA)

- **Combines ultracentrifugation with precision fluid flow through rotating seals**
- **Attains hydraulic steady-state in hours instead of months to years at low water contents**
- **Accelaration is a whole body force analogous to gravity so there are no physical changes in sample as occurs with pressure methods - no fracturing, no density changes, no collapsing of internal structure, no grain rearrangement**
- **-20° to 150°C; 10 to 10,000 g; 400 to 0.001 ml/hr**
- **Multicomponent and multiphase flow possible with whole body force**

The Primary Transport Parameters

K - Hydraulic Conductivity (water permeability)

$$q = K \cdot \nabla \psi$$

water flux = conductivity x pressure gradient

D - Diffusion Coefficient (static diffusion of single ions)

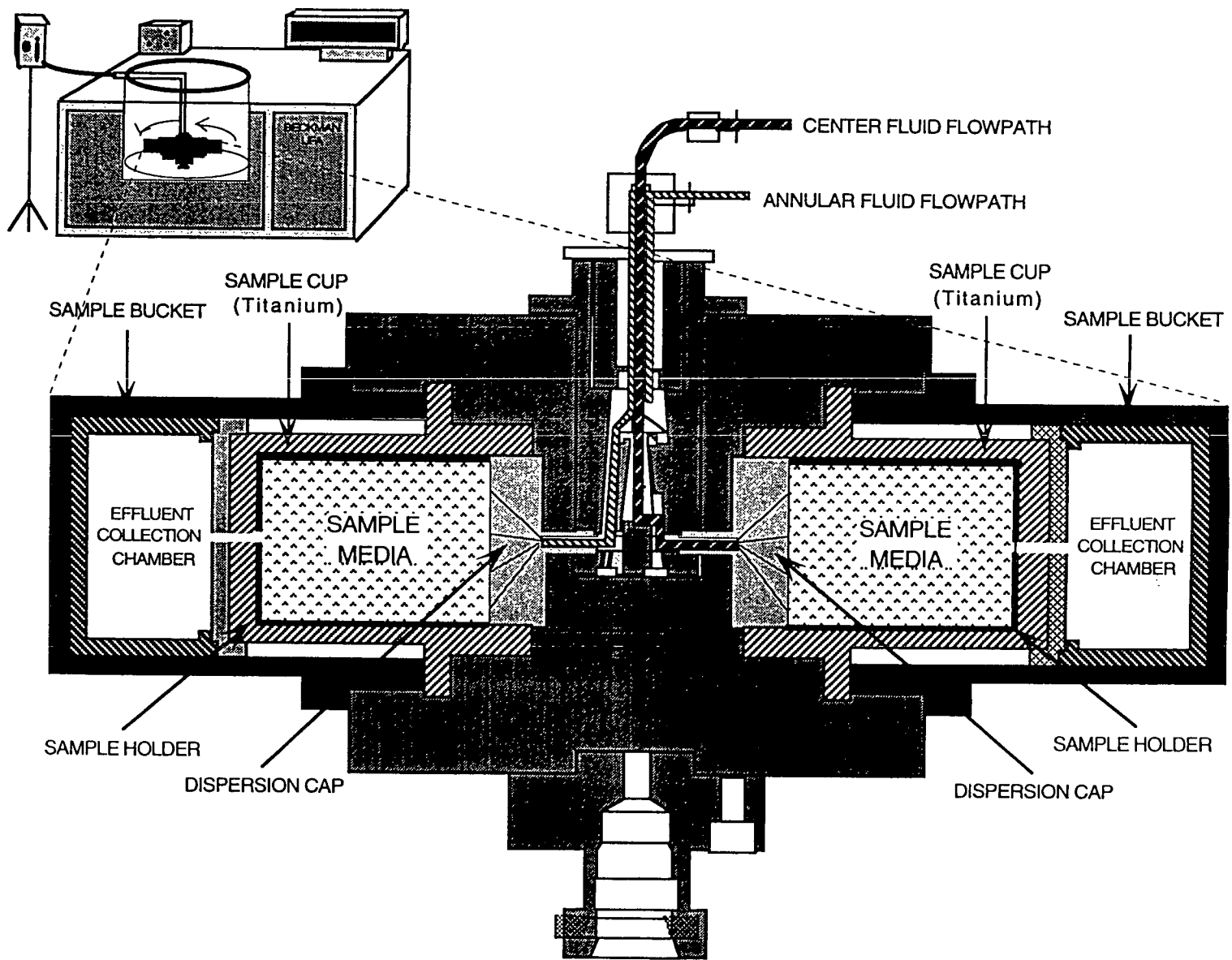
$$J = D \cdot \nabla \psi$$

ion flux = diffusion coefficient x concentration gradient

R_f - Retardation Factor (Chemical sorption and exchanges)

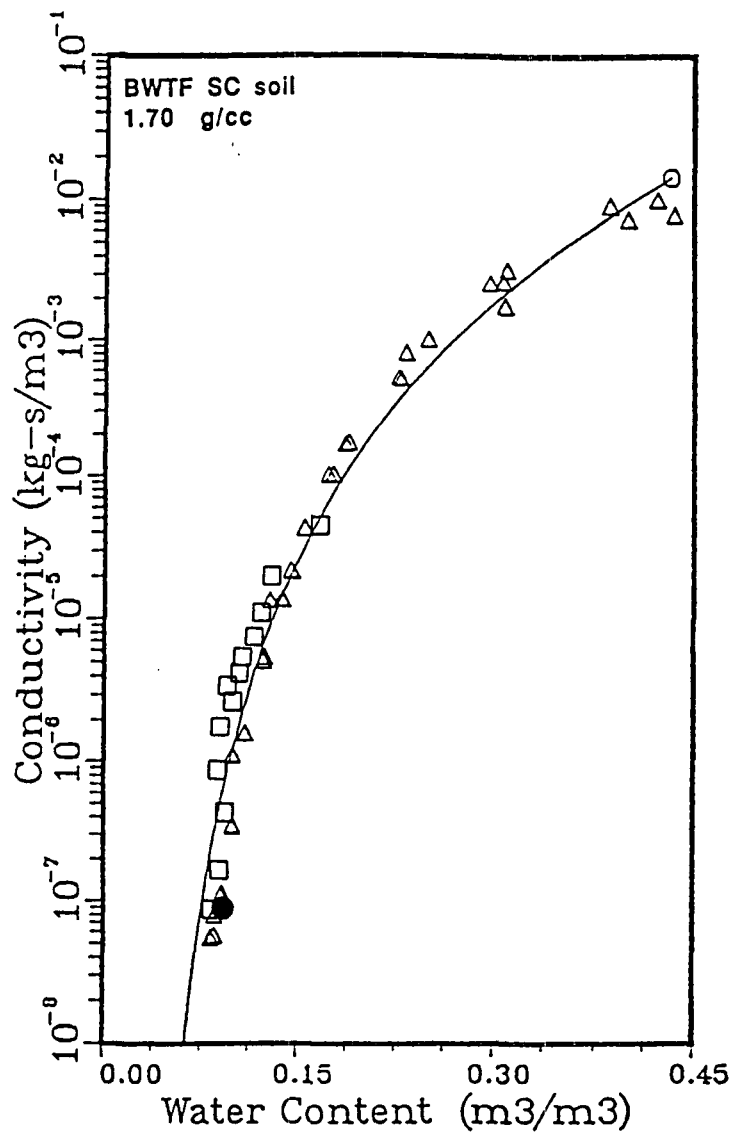
$$R_f = V_{gw} \div V_c$$

UFA Hy-Sed 10.0 Rotor With New Mechanical Seal Design



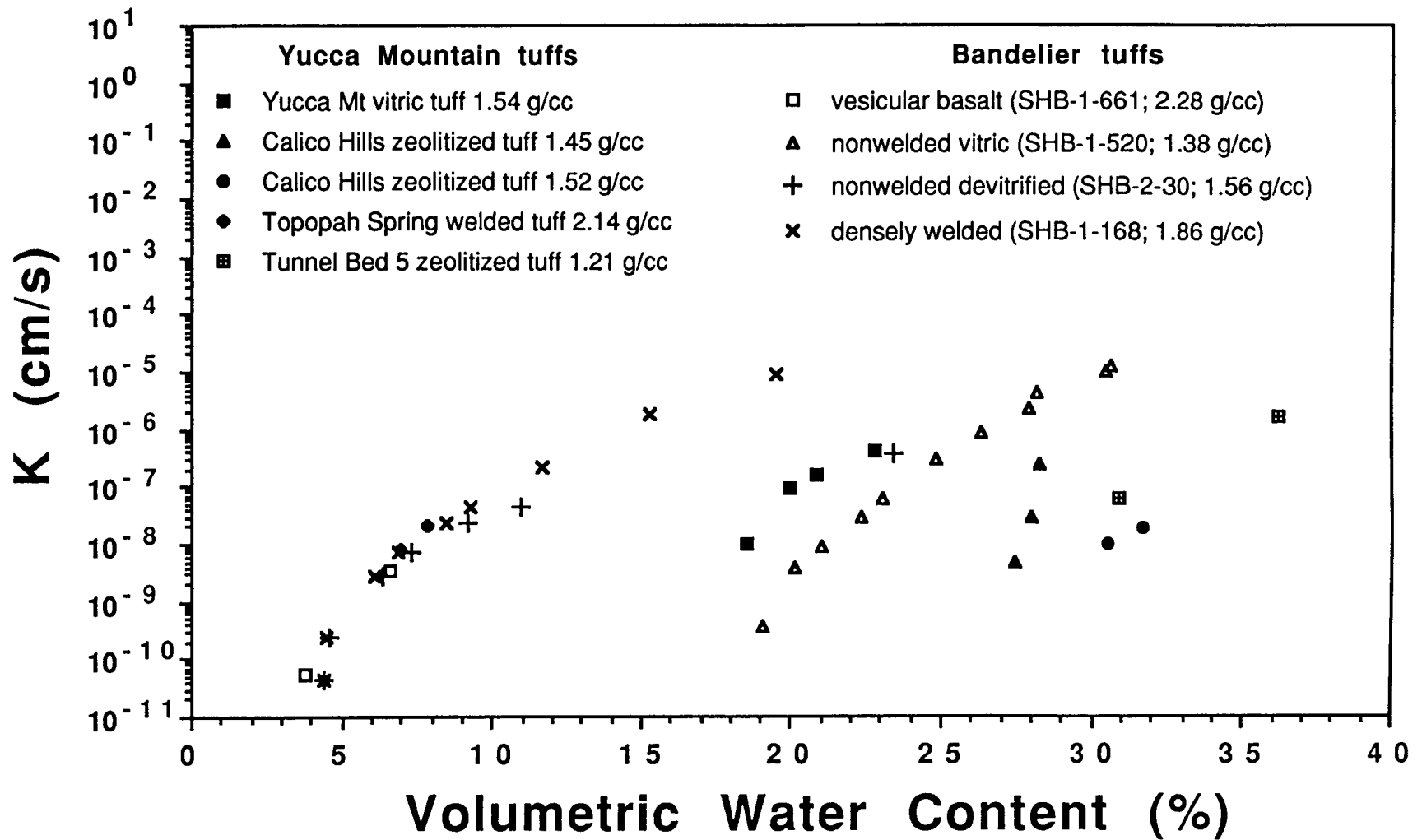
After the water content is fixed in the sample and the material is at hydraulic steady-state, transport parameters can be determined from a variety of associated methods.

- Hydraulic conductivity can be determined from the driving force and flux.**
- The electrical conductivity can be measured for determination of diffusion coefficients using the Nernst-Einstein equation.**
- The effluent can be monitored/collected/analyzed for chemical changes, retardation effects, and determination of partitioning.**



- UFA™ measurements made over 3-days
- △ Traditional column experiments made over 1-year
- Average of field lysimeter measurements made over 13-years
- Mualem estimation derived from curve-fitted water-retention data made over 6-weeks

Characteristic Curves for the BWTF Soil Obtained Using Four Different Methods

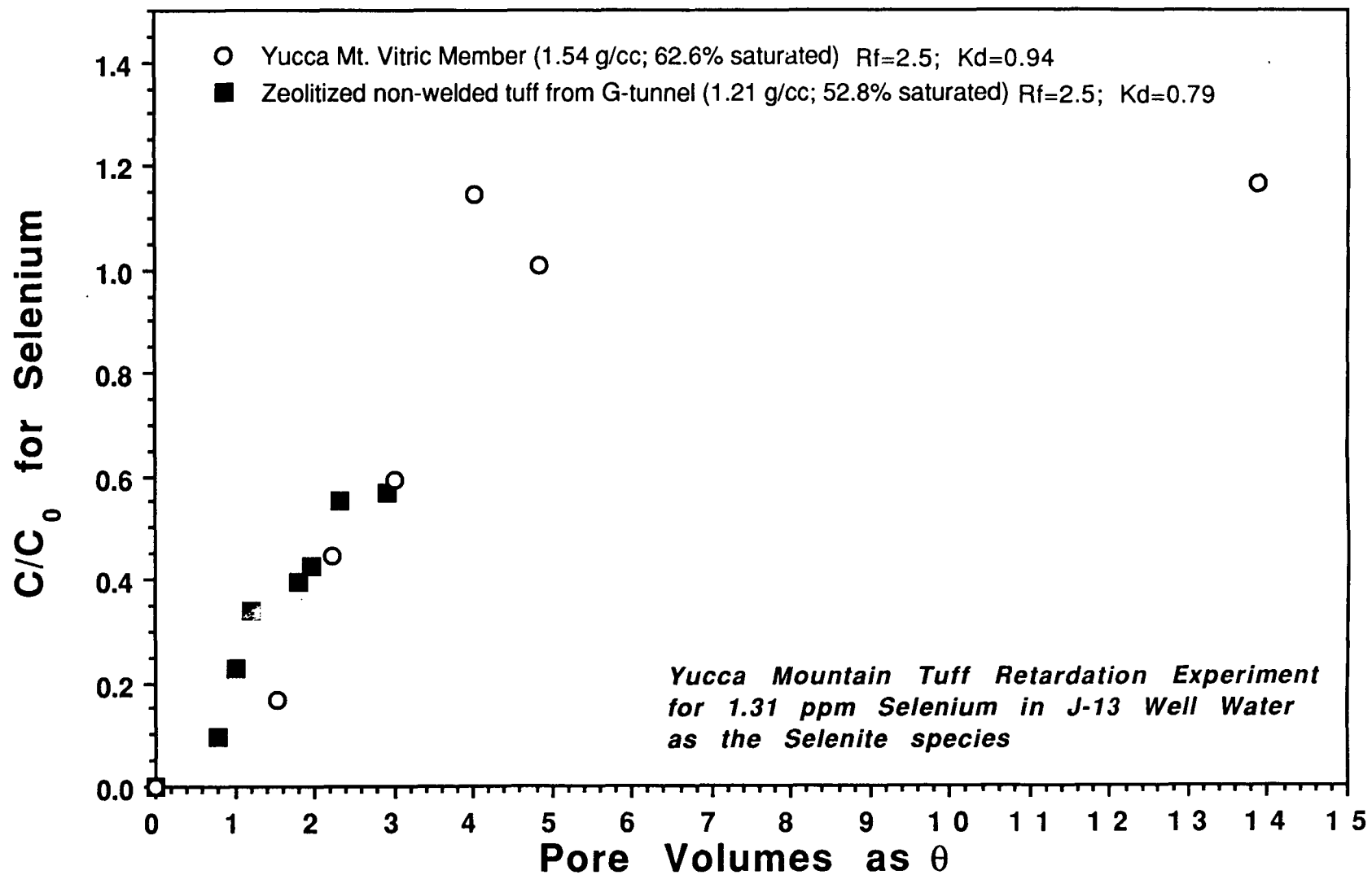


Unsaturated Hydraulic Conductivities for Various Tuffs.

Results of Se Sorption onto zeolitic tuff (from G tunnel) in J-13

Particle size of wet-sieved tuff: 75 - 500 μm

Initial Se Concentration, ppm	Pretreatment Period, Days	Sorption Period, Days	pH after Sorption	Kd (ml/g)
1.1	6.9	0.04	8.4	-0.2
1.1	6.9	0.04	8.4	0.3
1.1	6.8	13.9	8.5	0.0
1.1	6.8	13.9		0.2
0.5	6.8	13.9	8.6	4
0.5	6.8	13.9		3
0.4	6.8	13.9	8.3	20
0.4	6.8	13.9		10
0.02	6.8	13.9	8.3	40
0.02	6.8	13.9		30



Selenite Breakthrough Curves

Batch Sorption Experimental Procedure

Pre-treatment Step

- 1g of wet-sieved tuff equilibrated with 20 ml of J-13 groundwater
- Phases separated by centrifugation

Sorption Step

- Pre-treated tuff equilibrated with 20 ml of Se solution in J-13
- Phases separated by centrifugation
- Amount of Se in liquid phase determined by ICP-MS
- Amount of Se in solid phase calculated by difference

Controls

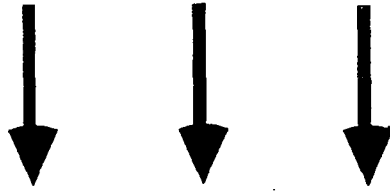
- Containers without tuff material utilized to monitor Se precipitation and/or sorption onto walls

Table 1. J13 WellWater Chemistry* Spiked with Selenite for Retardation Experiments

Na	44.3 ppm
K	4.0
Mg	1.81
Ca	12.1
Si	28.7
Se (as SeO₂)	1.40
Sr	0.036
B	0.141
pH	7.8
F	2.2
Cl	7.5
SO₄	19.0
NO₃	2.9
NO₂	14.0
HCO₃	119

*IC and ICP emission by Karl Pool at PNL

J13 Well Water
5 ml/hr
7500 rpm



$\theta = 7.9\%$
 $K = 2.07 \times 10^{-8} \text{ cm/s}$

$\theta = 0\%$



← infiltrating
water front

— 200 μ width
fracture

Paintbrush Tuff

$\rho = 2.41 \text{ g/cm}^3$

THE RETARDATION FACTOR

$$R_f = V_{\text{groundwater}}/V_{\text{contaminant}} = 1 + \rho K_d/n$$

R_f = retardation factor

V = velocity

n = porosity

ρ = bulk density

K_d = contaminant distribution coefficient

Which porosity should be used for n ?

total (θ_s)

volumetric water content (θ)

effective (mobile vs. dead-end pores)

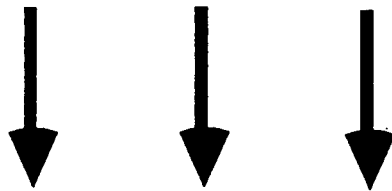
FRACTURE FLOW IN THE UFA™

- ③ The UFA™ can effectively uncouple the matric potential from the Darcy driving force.
- ③ In the UFA™, in situations where $d\psi/dr \ll \rho\omega^2r$, the centrifugal force is the dominant Darcy driving force, radially-symmetric and 1-dimensional.
- ③ However, the matric potential, while no longer important as a Darcy driving force, still acts in 3-dimensions and still is important in redistributing water and determining fluid flow paths.

Therefore, observed capillary phenomena are the same in the UFA™ as in the field, e.g., fractures desaturate in a stepwise manner with decreasing aperture size.

- ③ Care must be taken when investigating synthetic materials that have ideal, smooth-walled, planar fractures radially symmetric to the axis of rotation, situations not encountered in natural systems.

J13 Well Water
2 ml/hr
7500 rpm



$\theta \approx 7.0\%$
 $K = 8.28 \times 10^{-9} \text{ cm/s}$



infiltrating
water front

$\theta = 0\%$

200 μ width
fracture

Paintbrush Tuff

$\rho = 2.41 \text{ g/cm}^3$

SUMMARY

- **Available information suggests that batch sorption data can be used to predict transport under unsaturated conditions**
- **UFA is being utilized to further assess the validity of batch sorption data under unsaturated conditions**
 - ⊗ **Se and U in J13 well water at ppb to ppm**
 - ⊗ **Topopah Spring, borehole G4 - 268.6', 272.5'**
 - ⊗ **Calico Hills, borehole G4 - 1503.9', 1510', 1529'**
- **UFA will be used to study unsaturated soluble and colloid species transport through fractured tuff**
 - ⊗ **UFA is conservative with respect to colloids**