



U.S. Department of Energy
Office of Civilian Radioactive Waste Management

Assumptions and Results from Components of the Waste Form Degradation Model

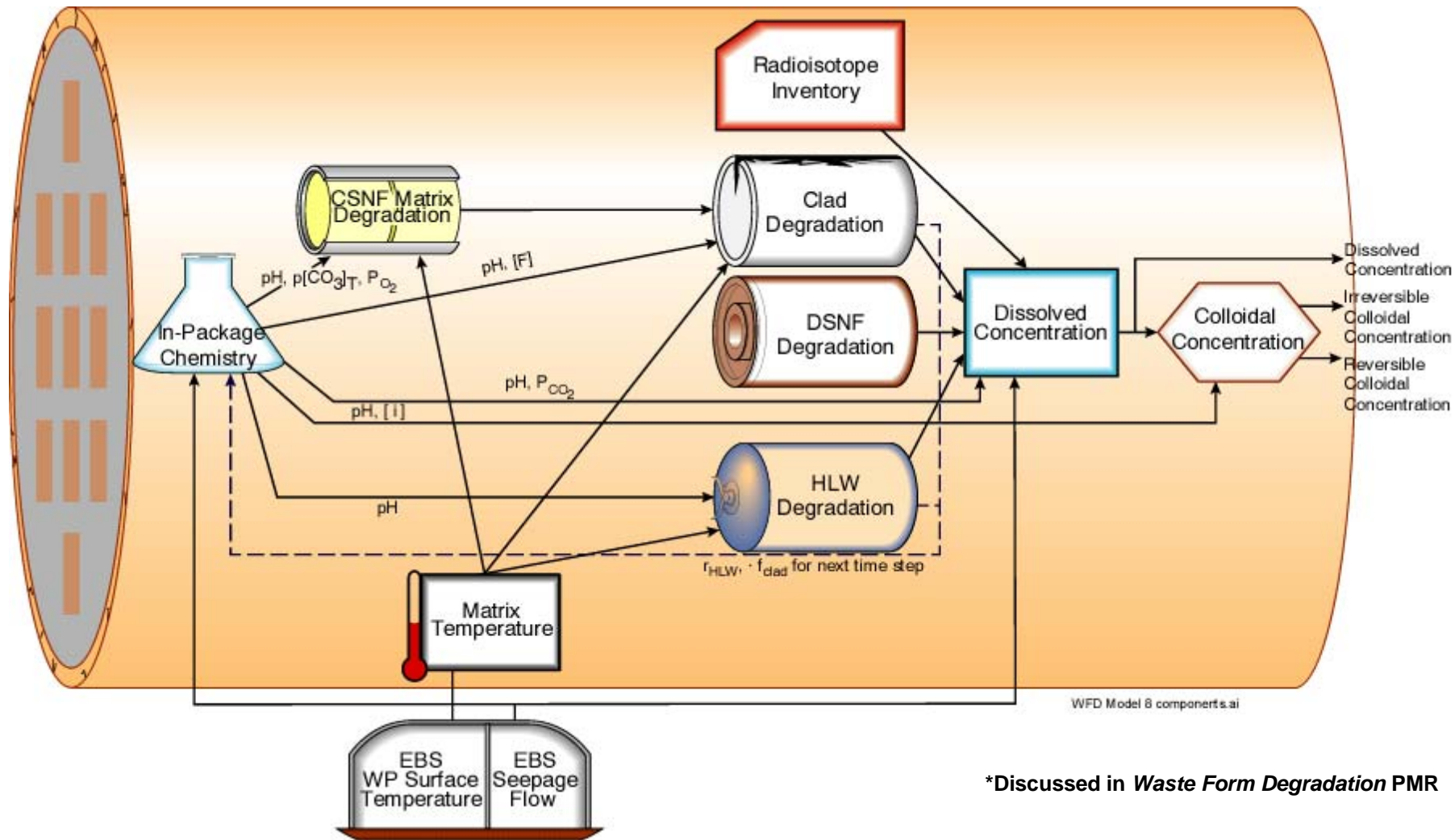
Presented to:
Nuclear Waste Technical Review Board

Presented by:
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Civilian Radioactive Waste Management System
Management and Operating Contractor

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YUCCA
MOUNTAIN
PROJECT

Waste Form Degradation Model* has Eight Components



*Discussed in *Waste Form Degradation PMR*

Process Model Factors Affecting Radionuclide Release from Waste Form

Key Attributes of Performance	Process Model Factor	TSPA-SR Input Parameters
Radionuclide Mobilization and Release from the Engineered Barrier System	In Package Environments	<ul style="list-style-type: none"> pH – f (region, time) Total dissolved carbonate (CO_3^{2-}) – f (region, time) Oxygen fugacity – f (region, time) Ionic strength – f (region, time) Fluoride – f(region, time) CO_2 fugacity Volume of water in the waste package/waste form cell
	Cladding Degradation and Performance	<ul style="list-style-type: none"> Fraction of surface area of Zircaloy-clad CSNF exposed as a function of time
	CSNF Degradation and Performance	<ul style="list-style-type: none"> CSNF intrinsic dissolution rate
	DSNF Degradation and Performance	<ul style="list-style-type: none"> DSNF intrinsic dissolution rate
	HLW Degradation and Performance	<ul style="list-style-type: none"> HLW intrinsic dissolution rate Specific surface area
	Dissolved Radionuclide Concentration	<ul style="list-style-type: none"> Concentration limits (solubilities) for all isotopes
	Colloid-Associated Radionuclide Concentrations	<ul style="list-style-type: none"> Types of waste form colloids Concentration of colloids K_d and/or K_c for various colloid types Fraction of inventory that travels as irreversibly attached onto colloids
	In-Package Radionuclide Transport	<ul style="list-style-type: none"> Porosity of corrosion products – f (time) Saturation of corrosion products – f (time) Evaporation – f (temperature, relative humidity, composition)
	EBS (Invert) Degradation and Performance	<ul style="list-style-type: none"> Thermally perturbed saturation in the invert – f (waste type, region, time, climate) Porosity of the invert Diffusion coefficient Volumetric flux through the invert – f (climate, time) Saturation in the invert after thermal pulse – f (time)

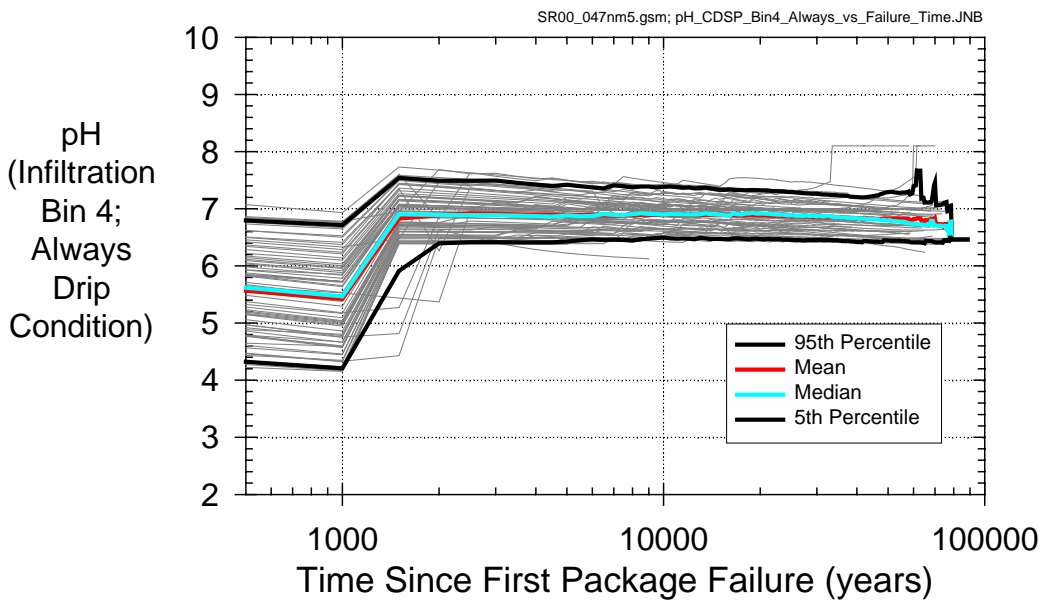
Assumptions of In-Package Chemistry Component*

- Cladding, HLW, and steel degradation rates, and fixed gas pressures (CO_2 and O_2) control bulk chemistry (pH , $[\text{CO}_3]_{\text{T}}$, $[\text{i}]$, and $[\text{F}]$)
- Bulk chemistry, in turn, influences five other components: CSNF degradation, HLW degradation, DSNF degradation, radionuclide solubility, and colloid stability
- Bulk chemistry approximated by well mixed, always oxidizing, full bathtub scenario
- Chemical condition in WP dominates; thus, J-13 well water can be used (e.g. no influence of evaporation assumed)

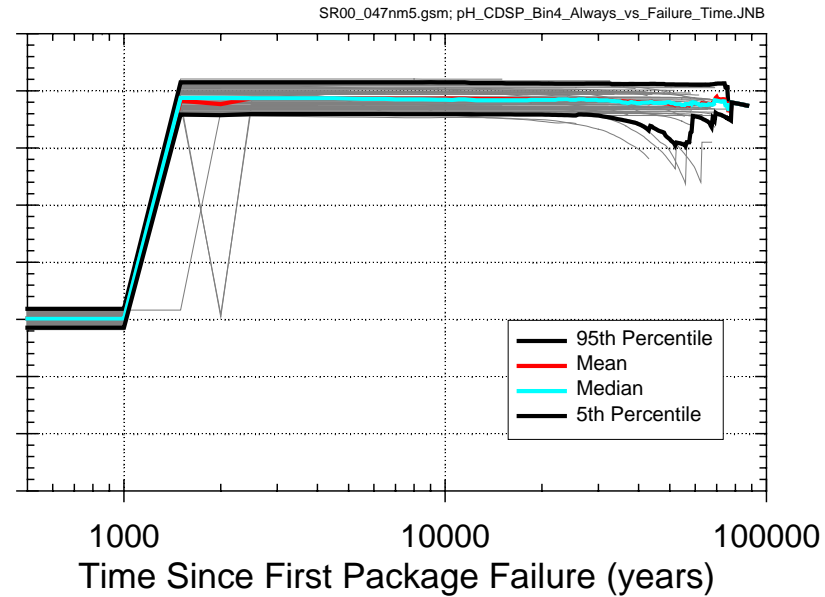
* Discussed in *In-Package Chemistry Abstraction* AMR

Uncertainty of pH Greater in CSNF Waste Packages

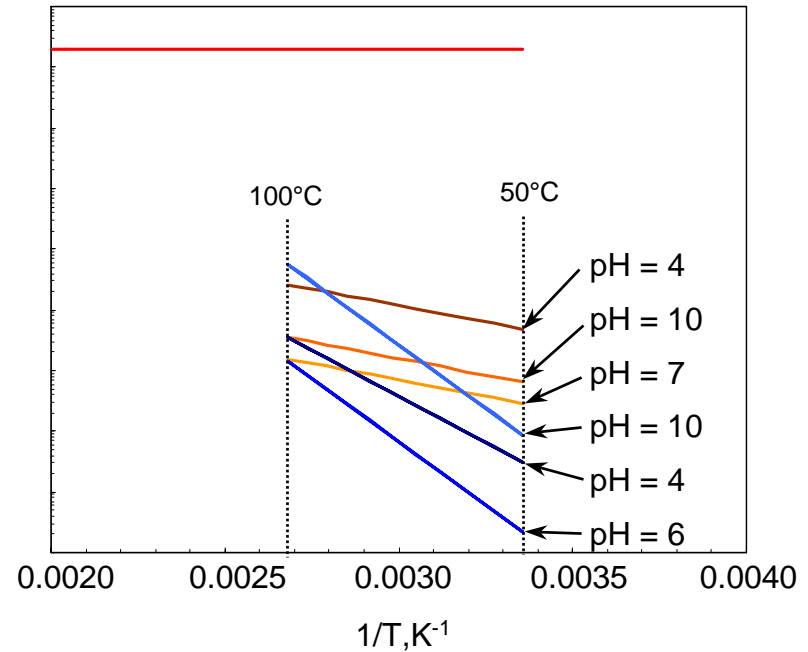
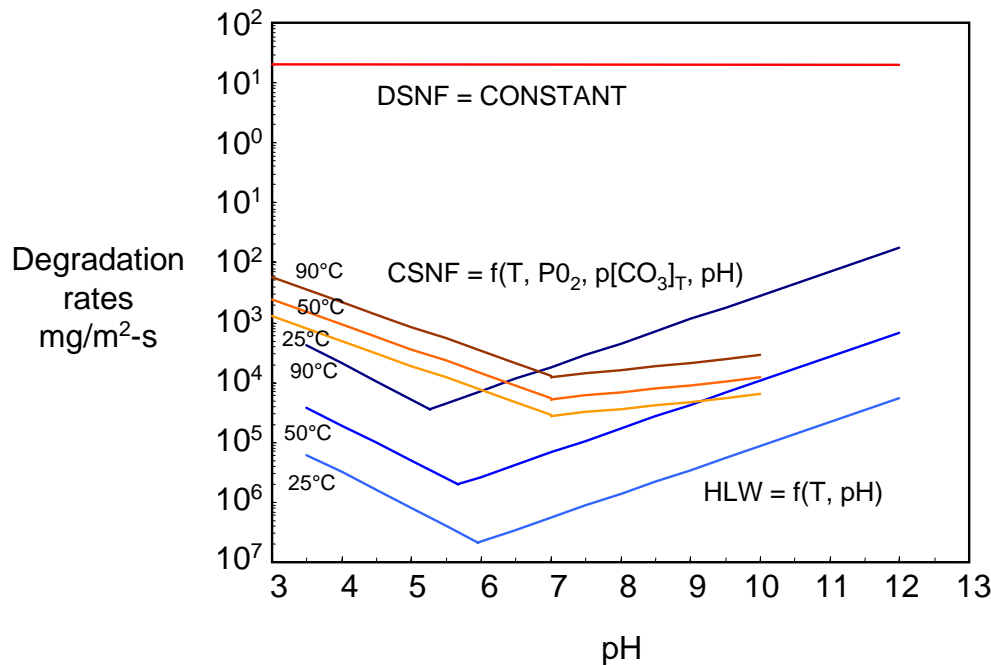
CSNF



Co - Disposal



Conservative Waste Form Degradation Rates Assumed for CSNF*, HLW[†], and DSNF[‡]

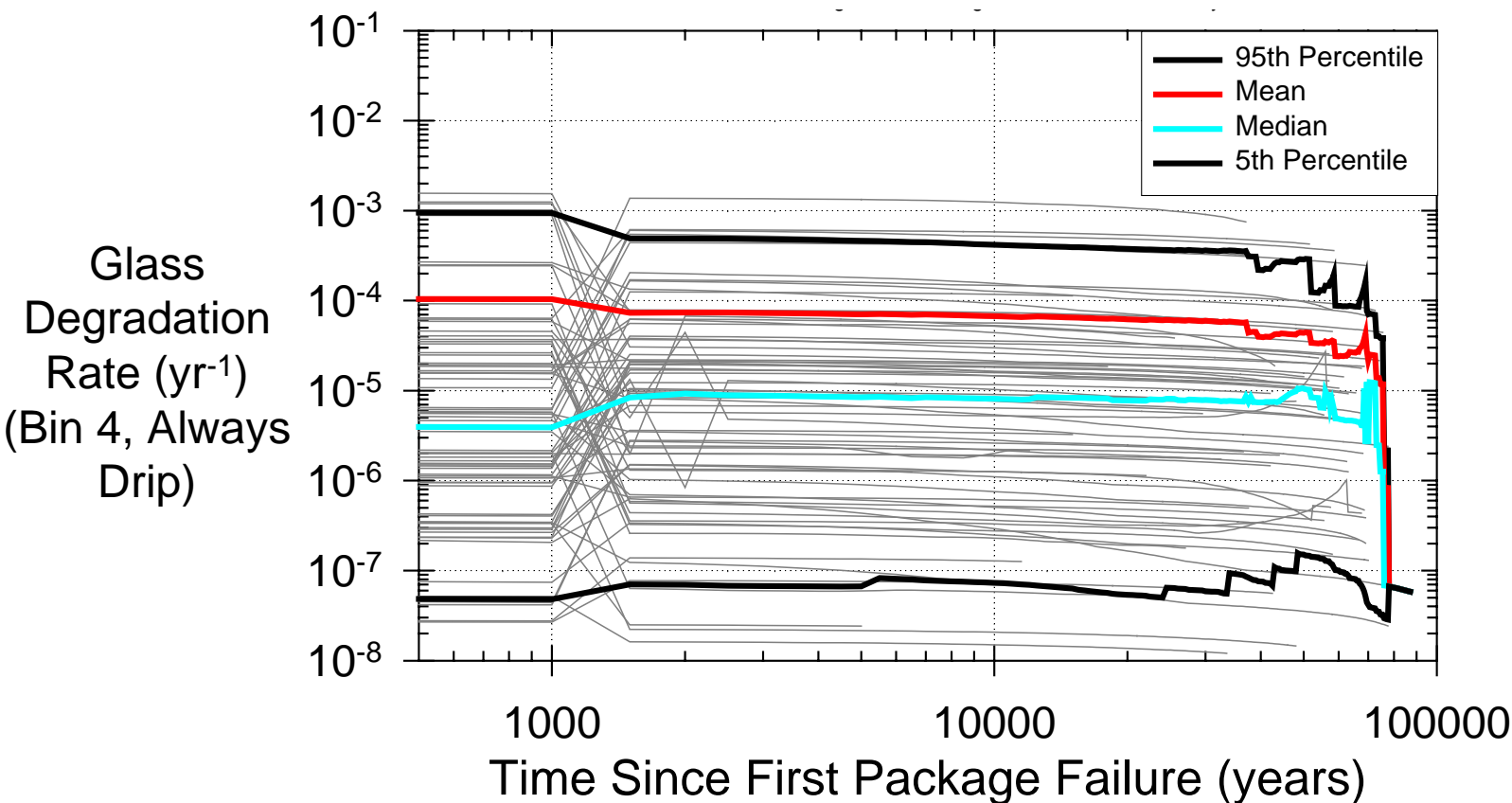


*Discussed in *CSNF Waste Form Degradation: Summary and Abstraction AMR*

†Discussed in *Defense High-Level Waste Glass Degradation AMR*

‡Discussed in *DSNF and Other Waste Form Degradation Abstraction AMR*

Glass Degradation Rate Has Very Large Uncertainty



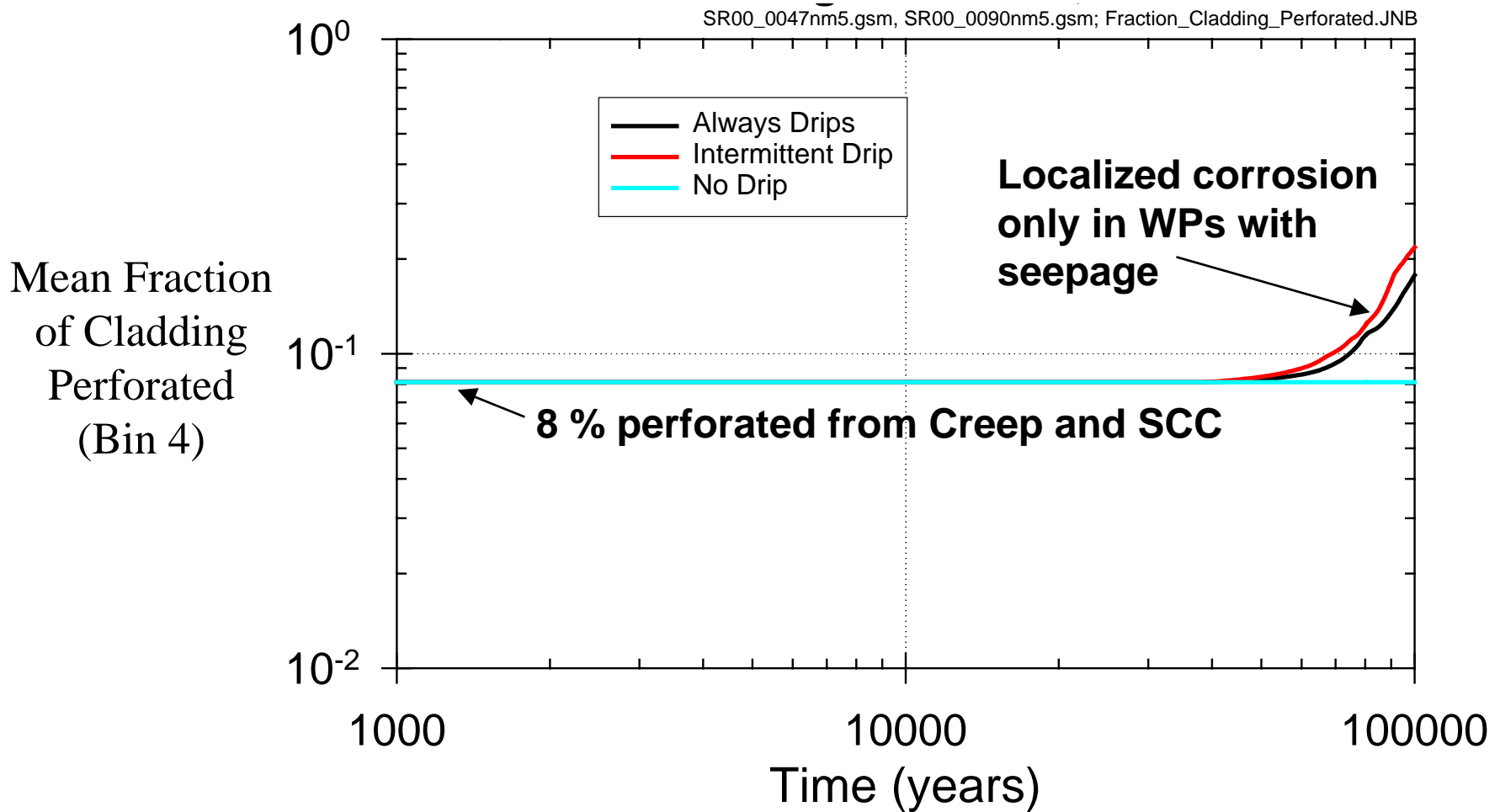
TSPA-VA: $1 \times 10^{-2} \text{ yr}^{-1} < 1000 \text{ yr}$ after exposure; $1 \times 10^{-6} \text{ yr}^{-1}$ at 10,000 yr

Assumptions in Cladding Component*

- **Two steps: perforation, unzipping**
- **Four perforation mechanisms included**
 - initial
 - creep and SCC (average of 8%)
 - localized corrosion (after water in WP ~40,000yr)
 - seismic: (rare - frequency of 10^{-6} /yr)
 - Fast release = gap fraction + fraction of rod dissolved before unzipping starts
- **Unzipping assumed to occur between 1 and 240 times faster than CSNF degradation rate**
 - Inventory releases as cladding unzips (except fast release)

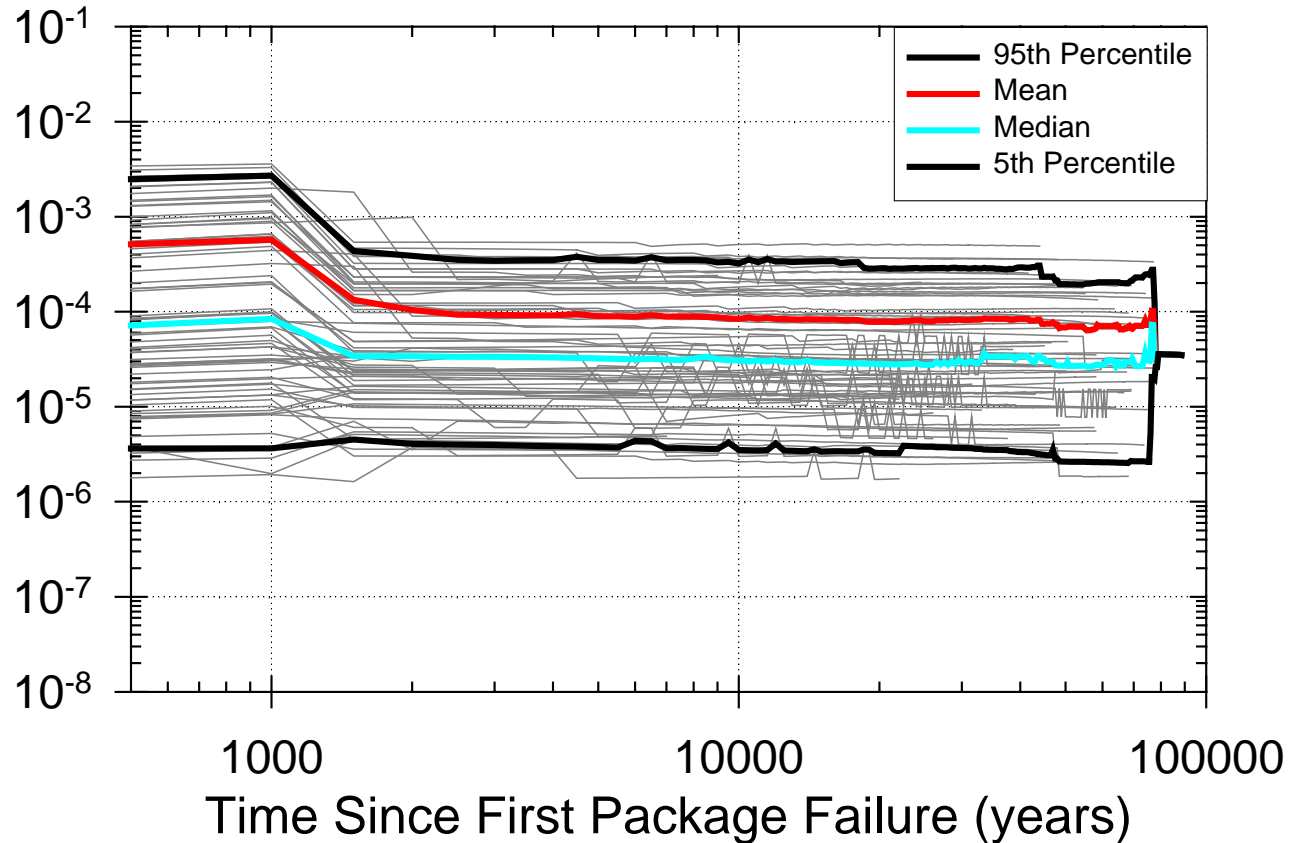
*Discussed in *Clad Degradation- Summary and Abstraction* AMR

Prior to 50,000 yr Cladding Perforation Caused by creep rupture



Unzipping Rate has Large Uncertainty

SR00_047nm5.gsm; Unzipping_Rate_CSNF_Bin4_Always_vs_Failure_Time.JNB



TSPA-VA: CSNF degradation $2 \times 10^{-2} \text{ yr}^{-1}$ to $4 \times 10^{-3} \text{ yr}^{-1}$ over 10,000 yr

Assumptions in Solubility Component*

- **Conservatively selected pure phases to control solubility**
- **Conservatively fixed gas pressures CO₂, O₂ at atmospheric conditions**
- **Conservatively neglect sorption or coprecipitation of radionuclides**

*Discussed in *Summary of Dissolved Concentration Limits AMR*

Solubility of Important Radioisotopes updated for TSPA-SR

Distributions

- Pu - Solid Pu(OH₄)(am)
- Pa
- Pb

Empirical functions

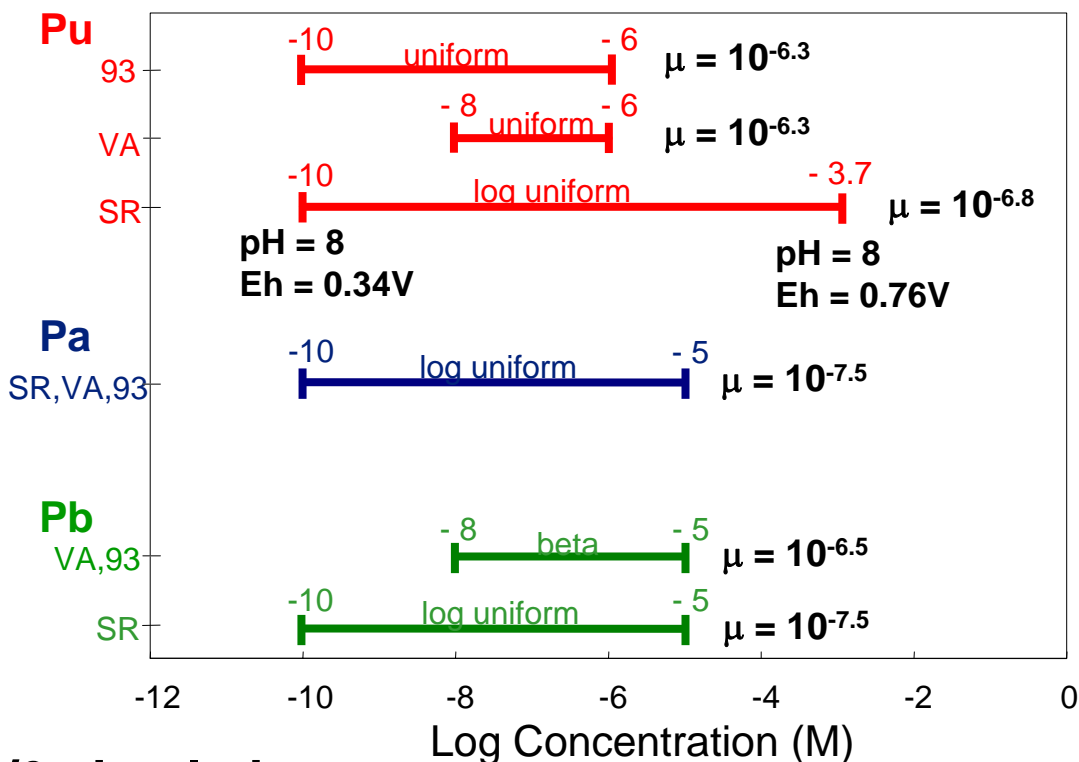
- Np = f (pH)
- Am = f (pH, P_{co2})
- U = f (pH, P_{co2}, T)

Constants

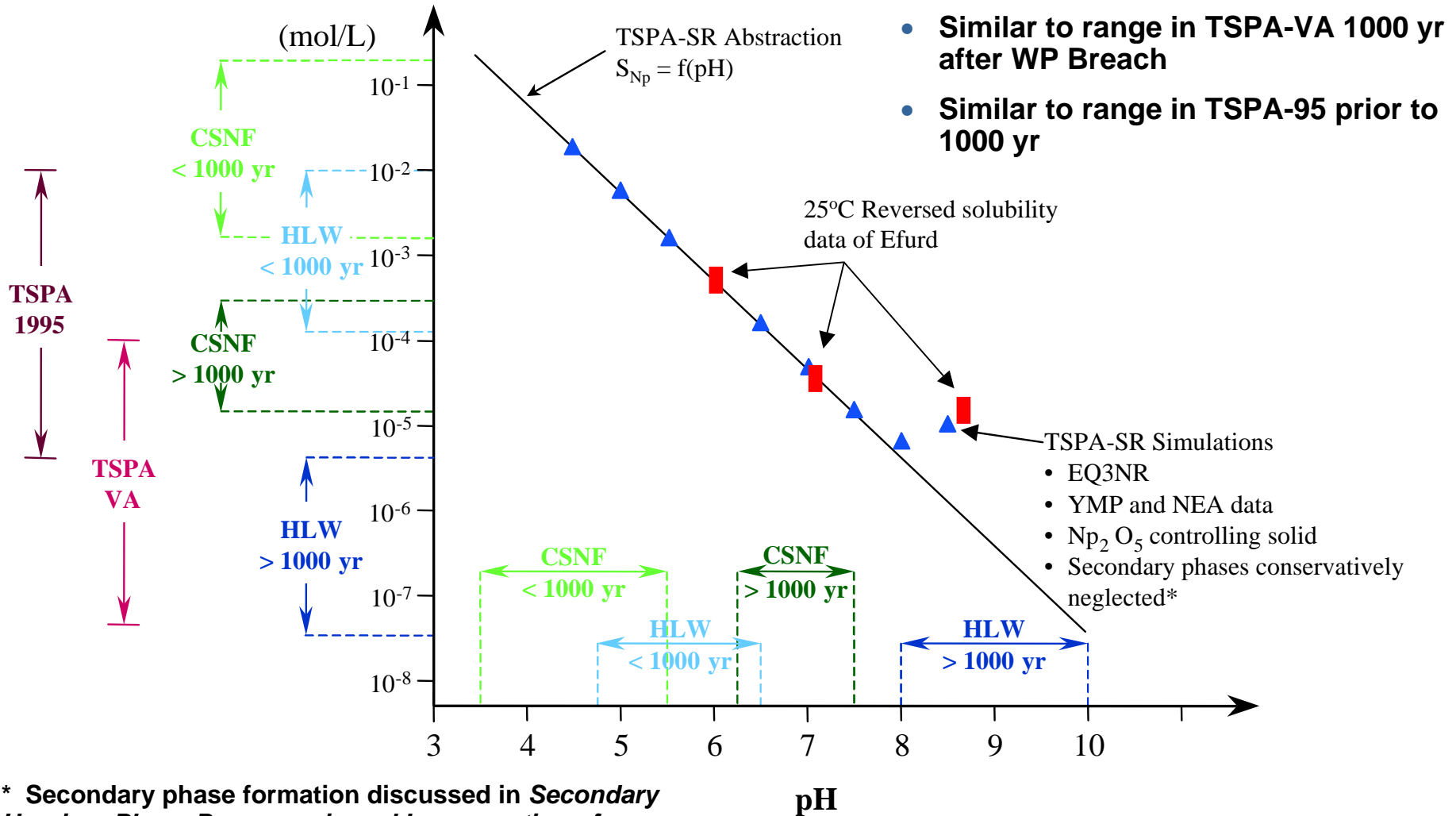
- Tc = I = Sr = Cs = C = 1M

Estimates based on EQ3/6 simulation

- Thermodynamic data used recent NEA and literature



Np Solubility Varies with pH

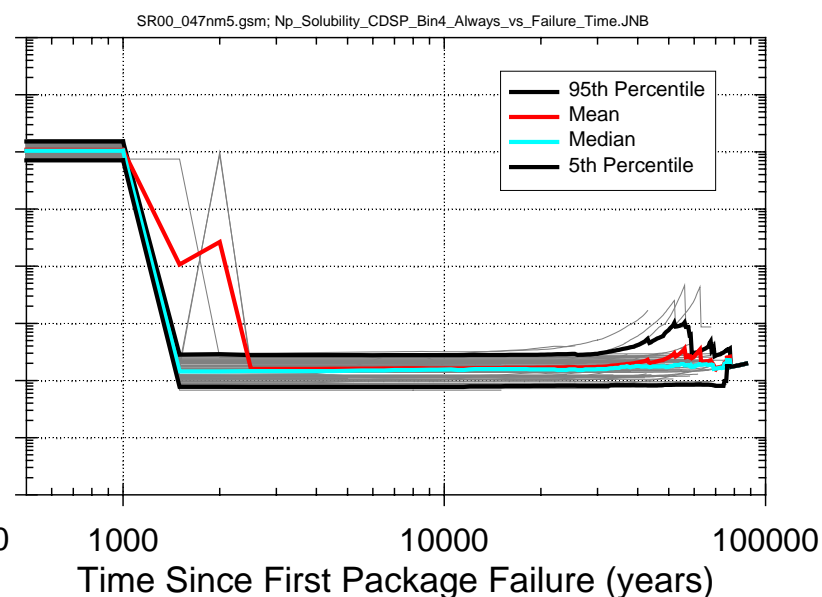
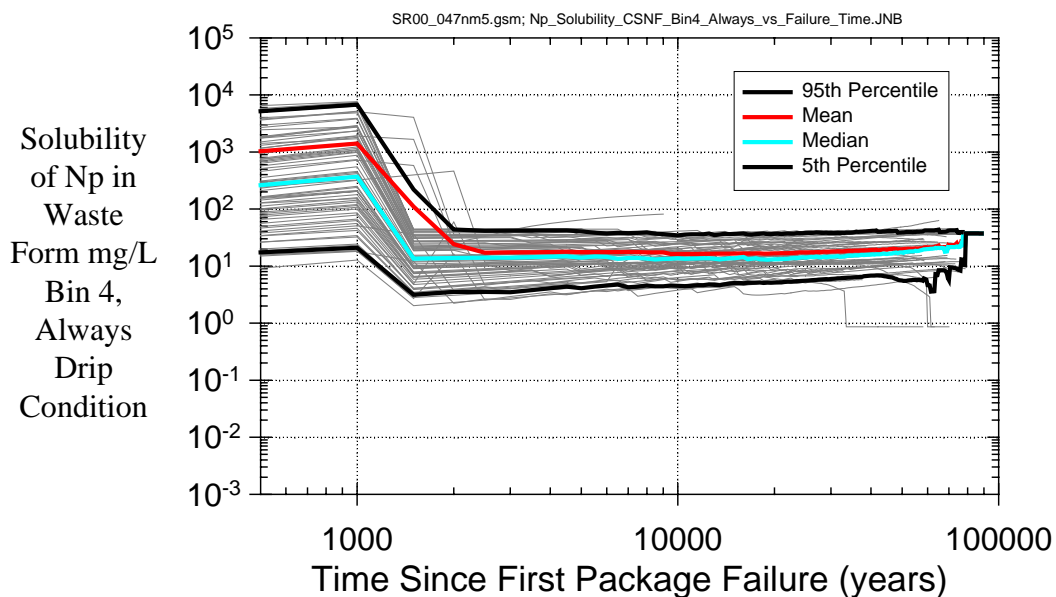


* Secondary phase formation discussed in *Secondary Uranium-Phase Paragenesis and Incorporation of Radionuclides into Secondary Phases AMR*

Uncertainty in Solubility of Np Determined by Uncertainty in pH

CSNF

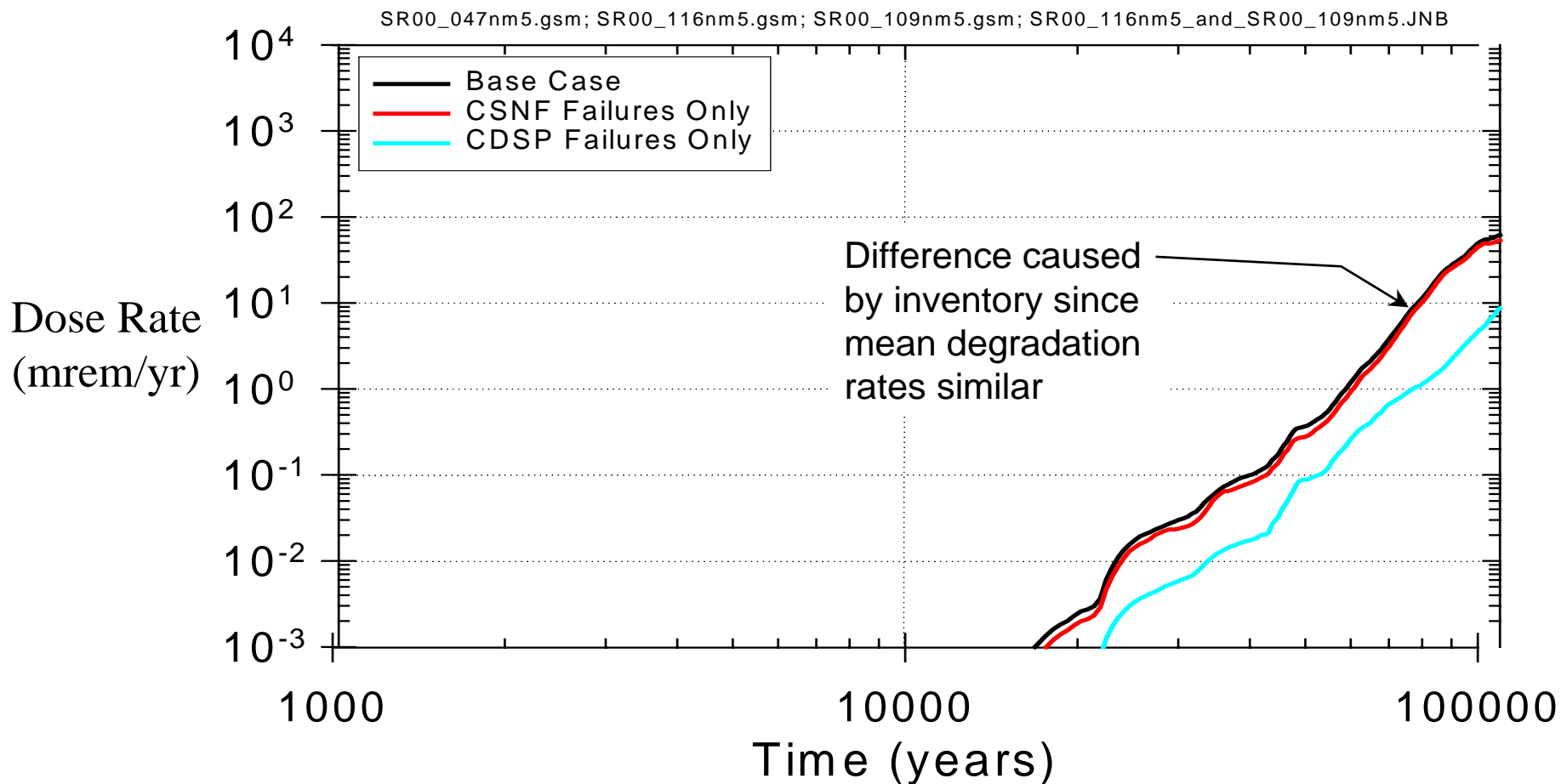
Co - Disposal



Assumptions in Colloid Component

- Calculated ionic strength and pH determines concentration
- *Irreversible* waste colloids from HLW
- Pu and Am transported as *irreversible* colloids
- *Reversible* colloids from groundwater, rust, and waste
- Pu, Am, Th (Ra, Pb), Pa (Ac), Sr, Cs transported as *reversible* colloids
- No filtration or sorption within package
- Diffusion coefficient for colloids very conservative (only 100 times less than aqueous diffusion)

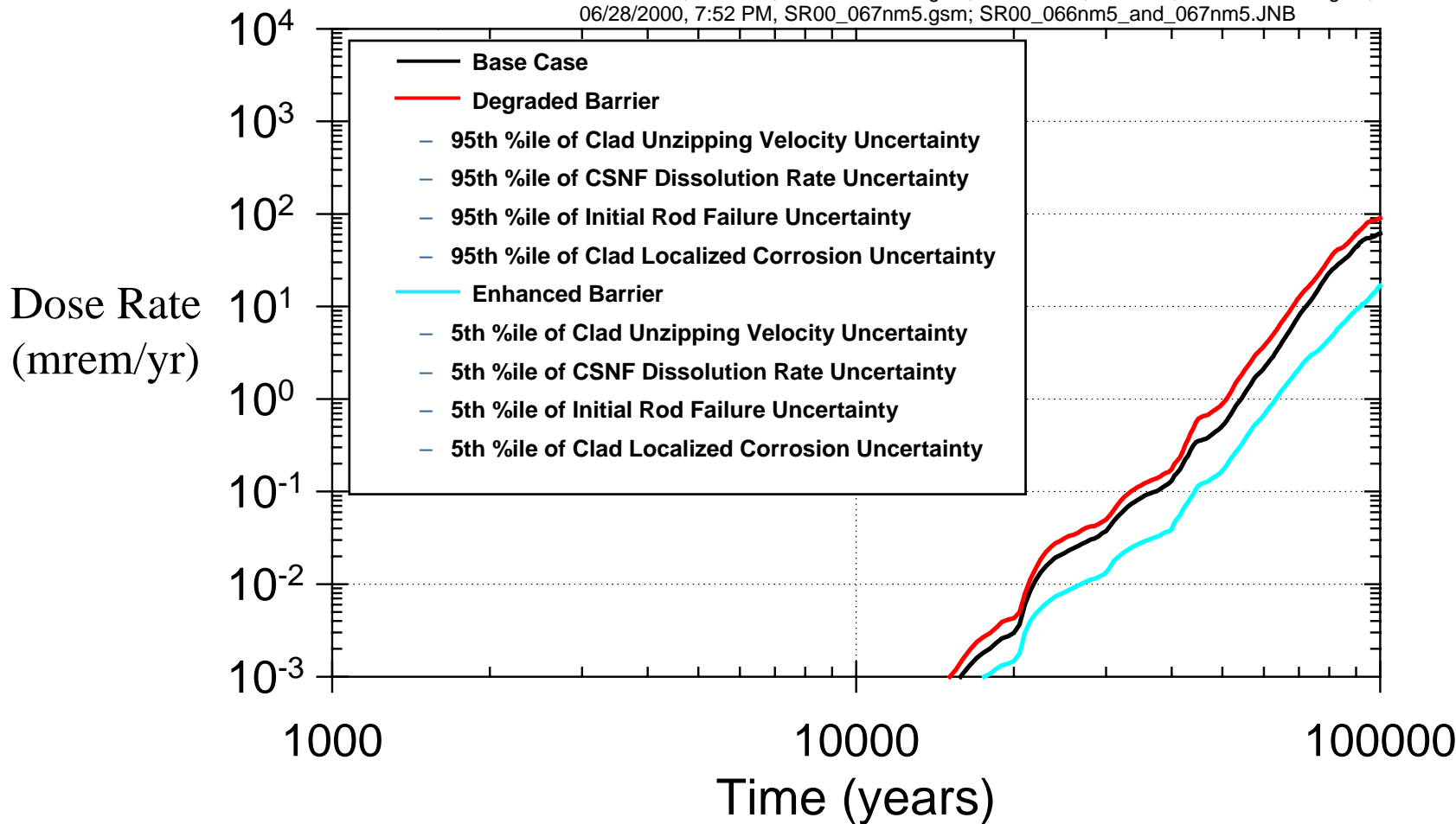
Releases from CSNF Contribute Most to Dose



This information was prepared for the 8/00 NWTRB meeting for illustrative purposes only and is subject to revision; not appropriate for assessing regulatory compliance.

Degraded Cladding Condition Increases Dose by Factor of 4

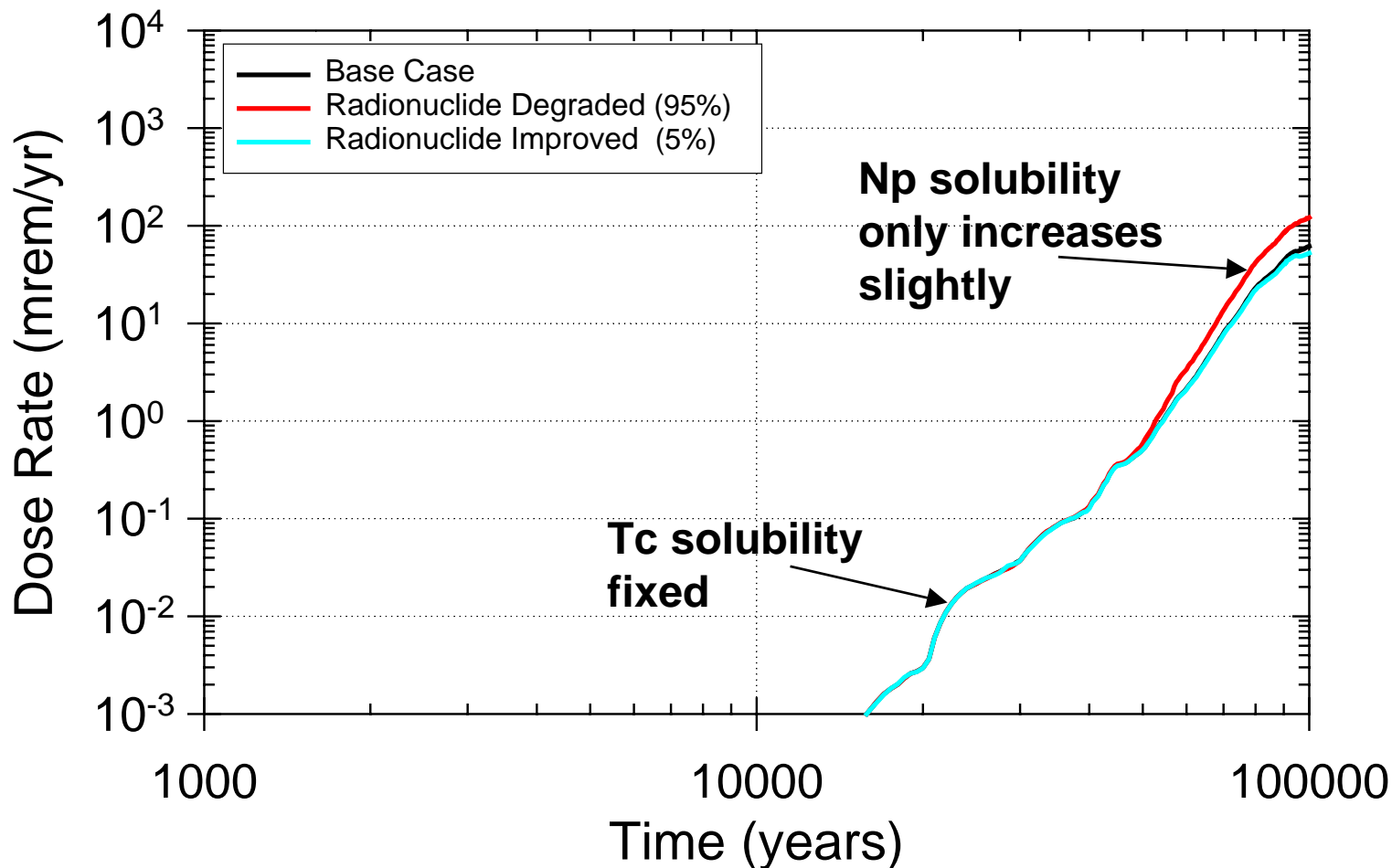
06/25/2000, 1:33 PM, SR00_047nm5.gsm; 06/28/2000, 9:18 PM, SR00_066nm5.gsm;
06/28/2000, 7:52 PM, SR00_067nm5.gsm; SR00_066nm5_and_067nm5.JNB



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Because pH Range Narrow in EBS, Np Release Only Changes Slightly

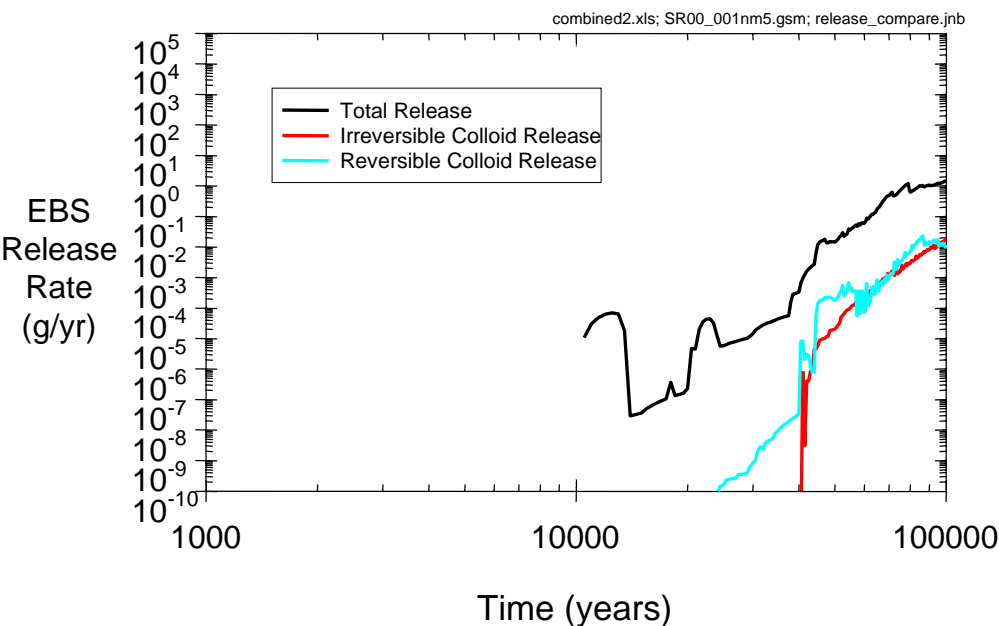
SR00_047nm5; SR00_093nm5; SR00_094nm5; SR00_093nm5_and_SR00_094nm5.JNB



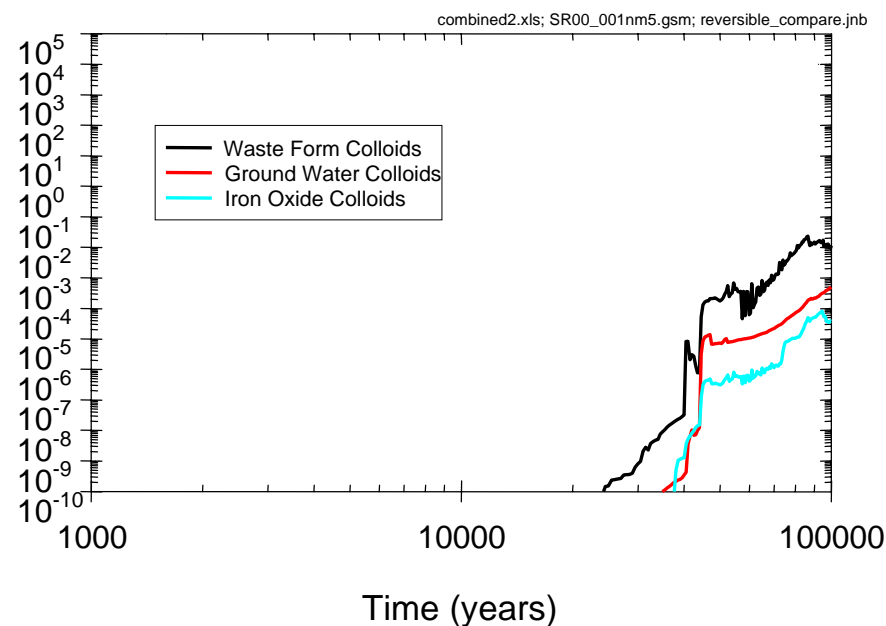
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Colloids Only Contribute a Small Fraction to Release of ^{239}Pu

Total ^{239}Pu Release

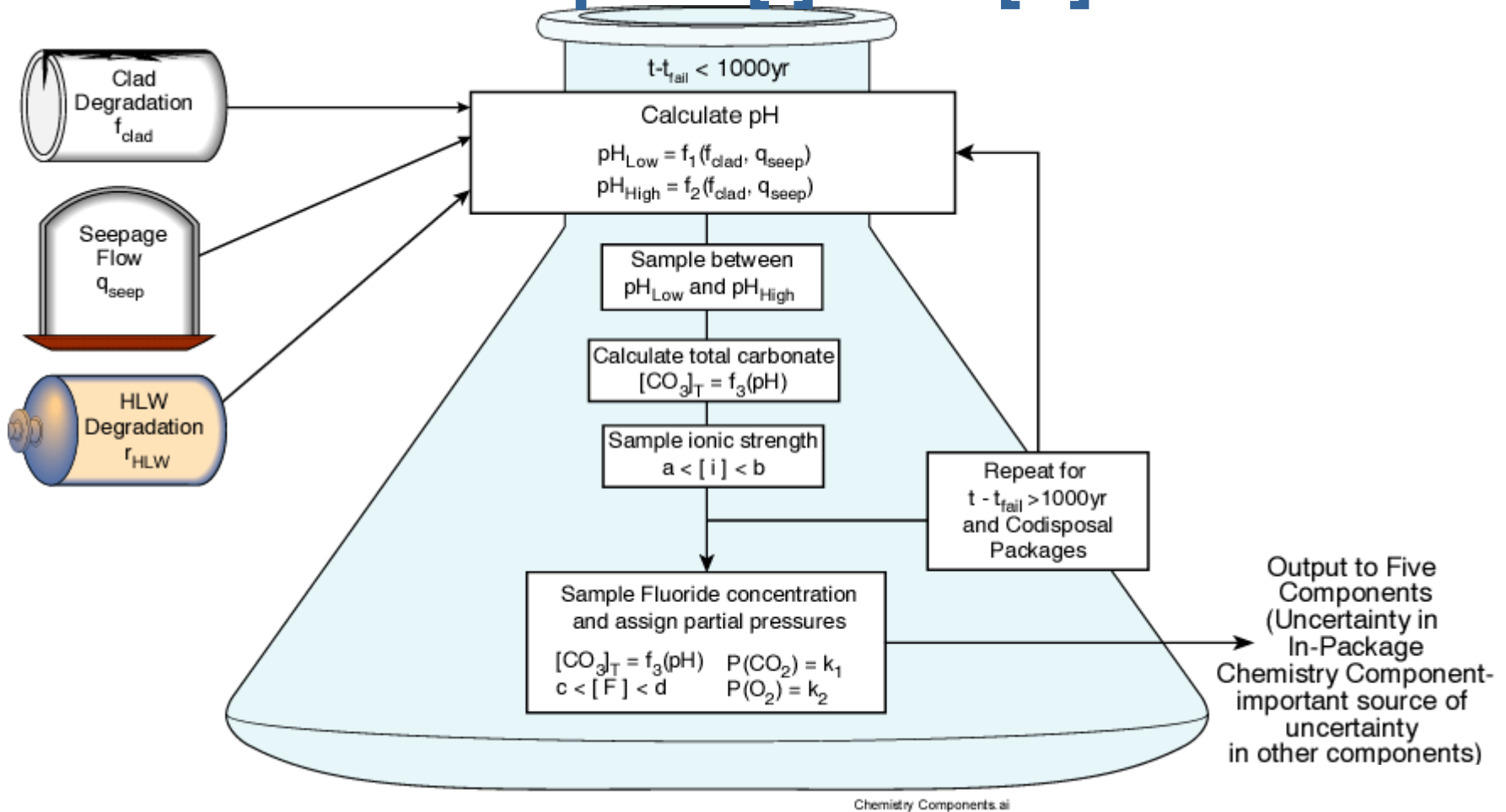


Source of Reversible Colloids

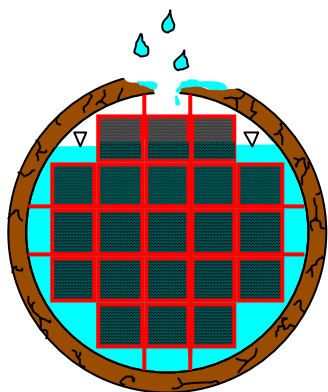


Backup Slides

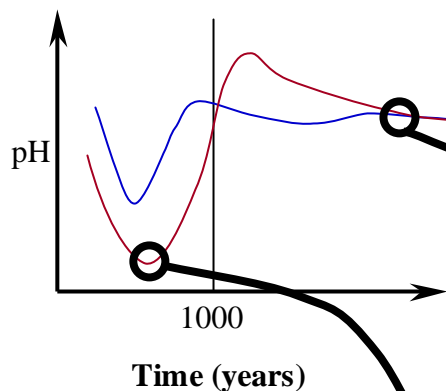
In-Package Chemistry Component Estimates pH, Calculates $[\text{CO}_3]_T$, and Samples $[i]$ and $[F]$



In-Package Chemistry Component Developed from Regression Analysis on FQ3/6 Runs



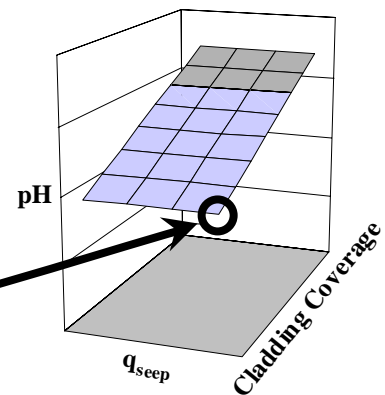
CSNF Conceptual Model



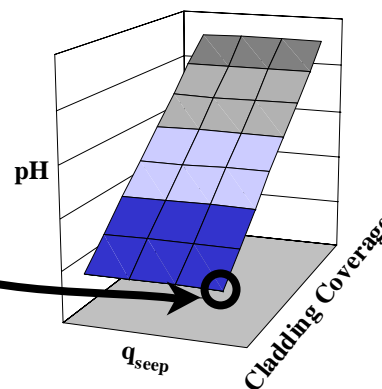
EQ3/6 Runs Varying:

- q_{seep}
- r_{steel}^*
- r_{hlw}
- f_{clad}

* Corrosion of steel releases sulfur which can lower pH.

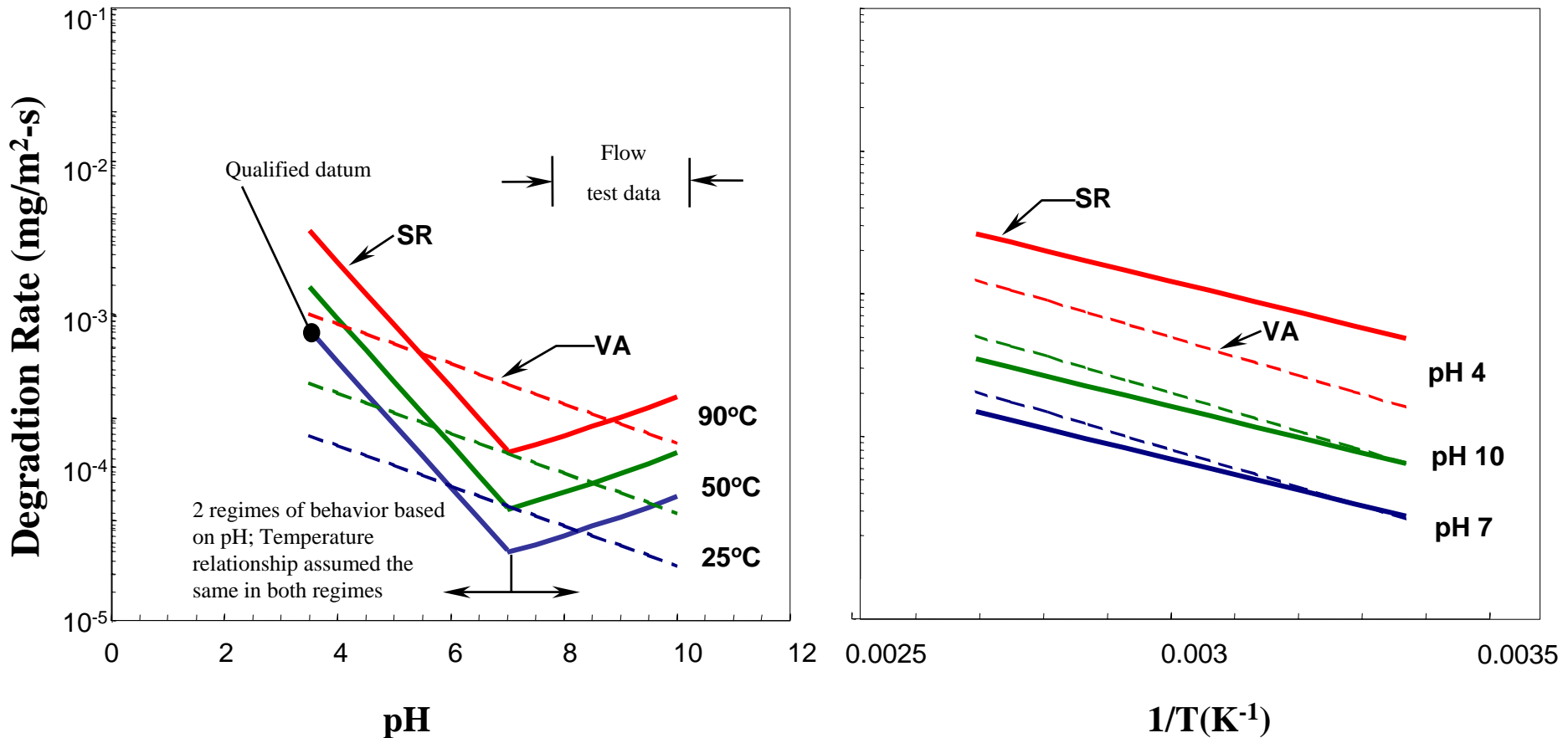


pH Abstraction for > 1,000 Years

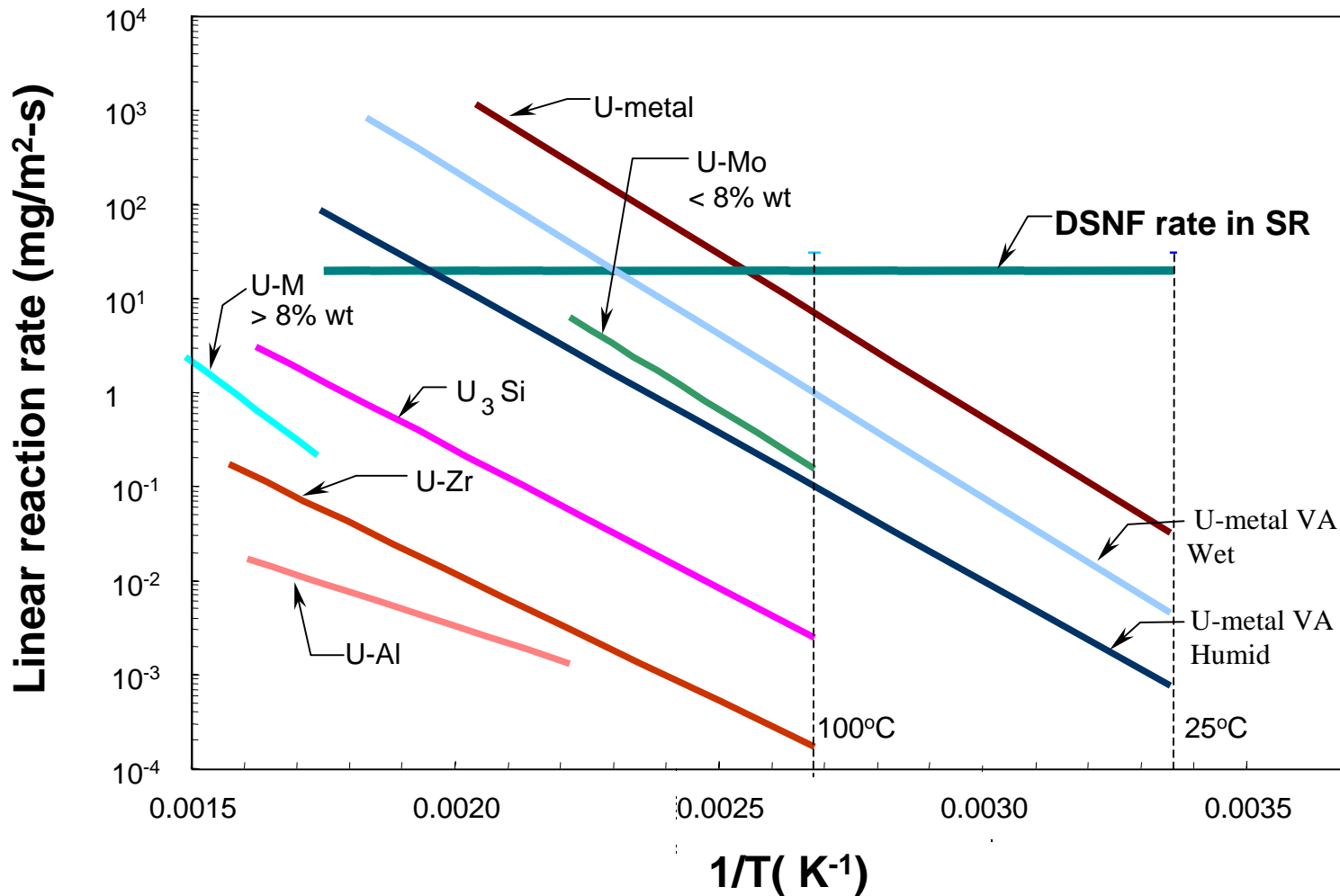


pH Abstraction for < 1000 Years

CSNF Degradation Rates in SR Similar to Rates in VA

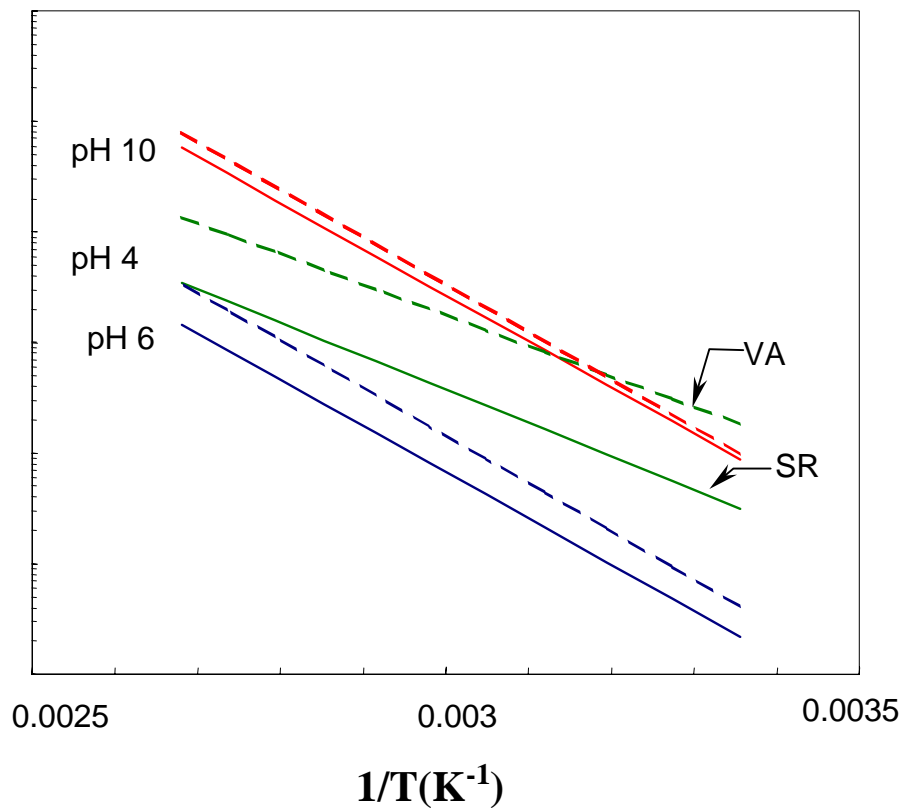
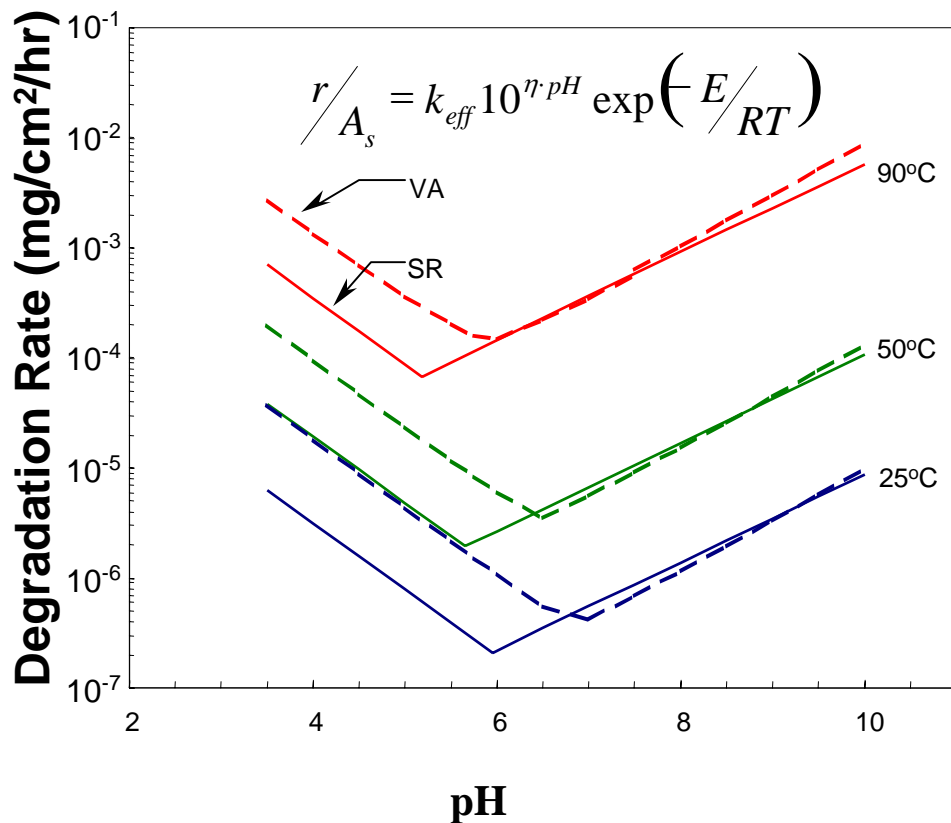


Constant Degradation Rate Used for DSNF Category Bounds all Measured Degradation Rates

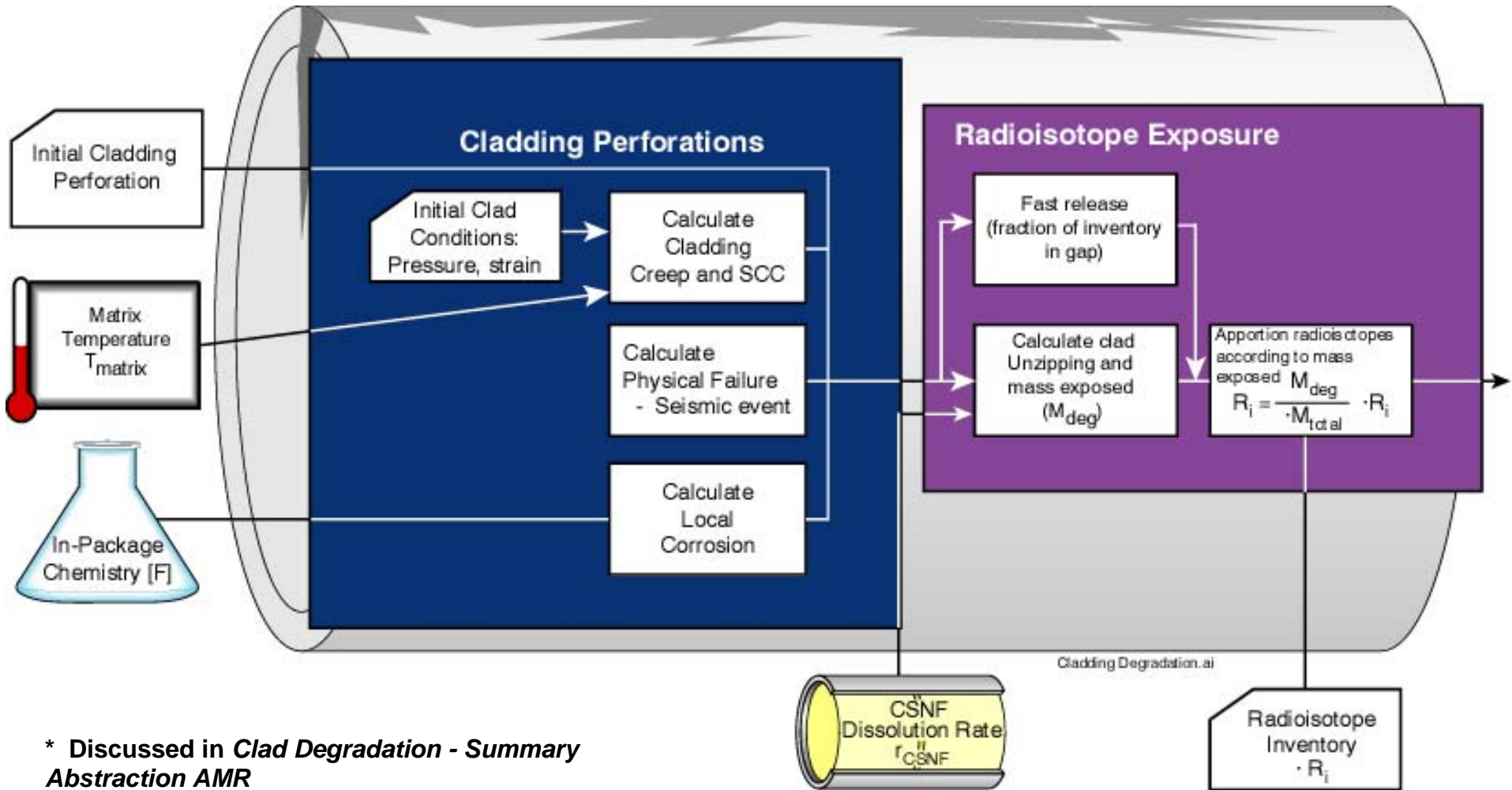


HLW Reaction Rates in SR similar to VA

- HLW rate less than CSNF degradation except at high pH and high temperature
 - HLW rate bounds stage I, II, III degradation rates

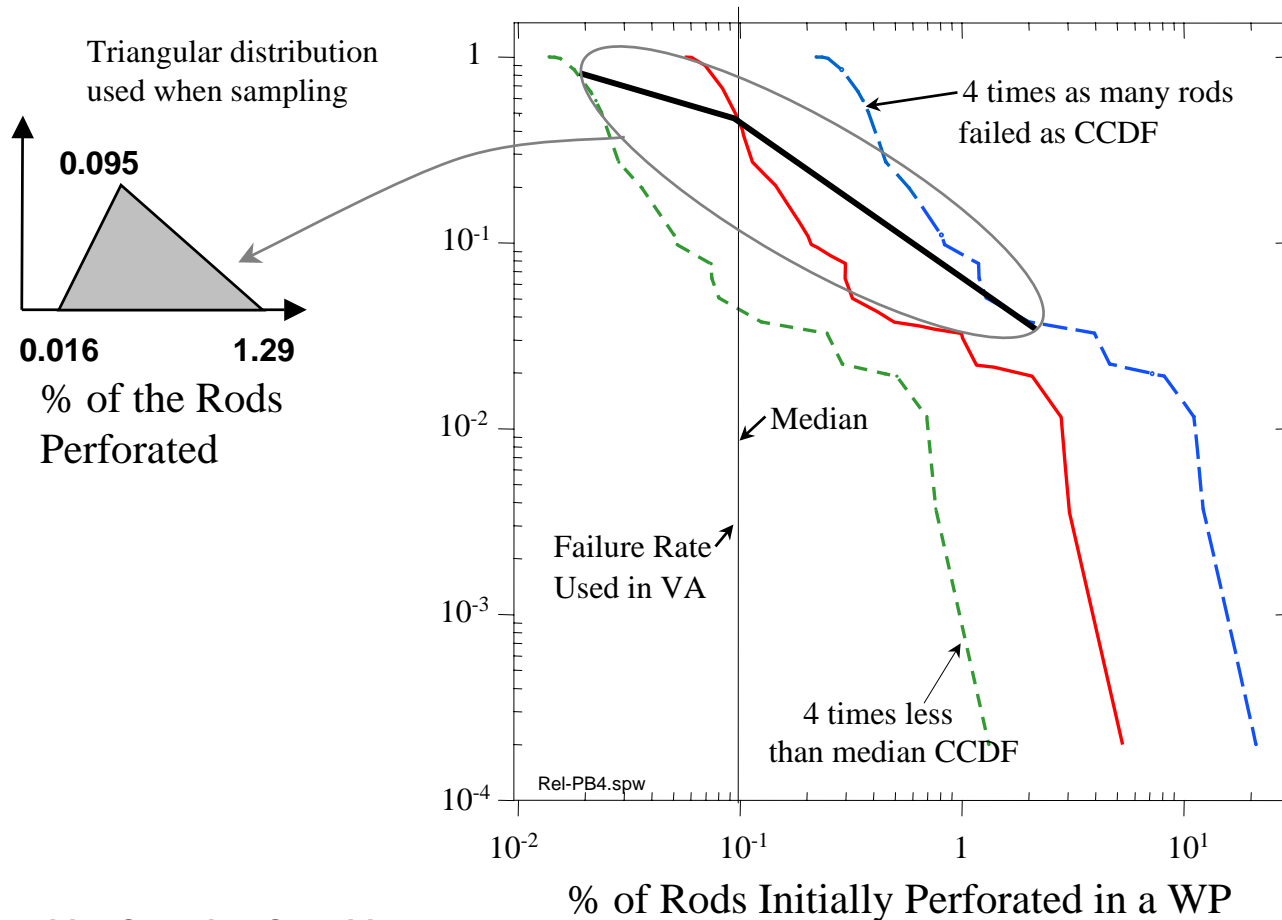


Cladding Degradation* Consists of Two Steps: Perforation and Unzipping



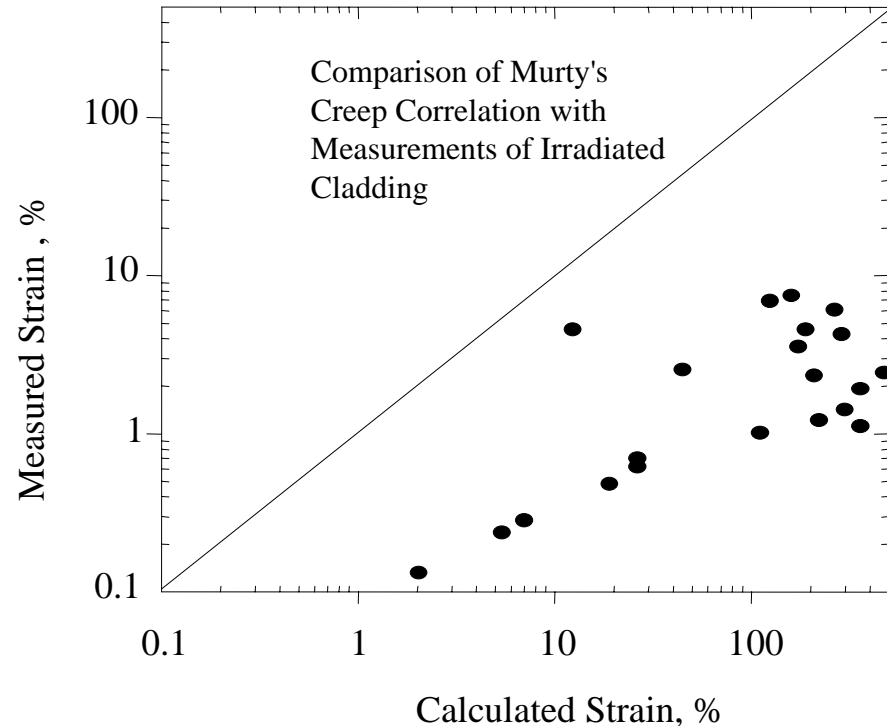
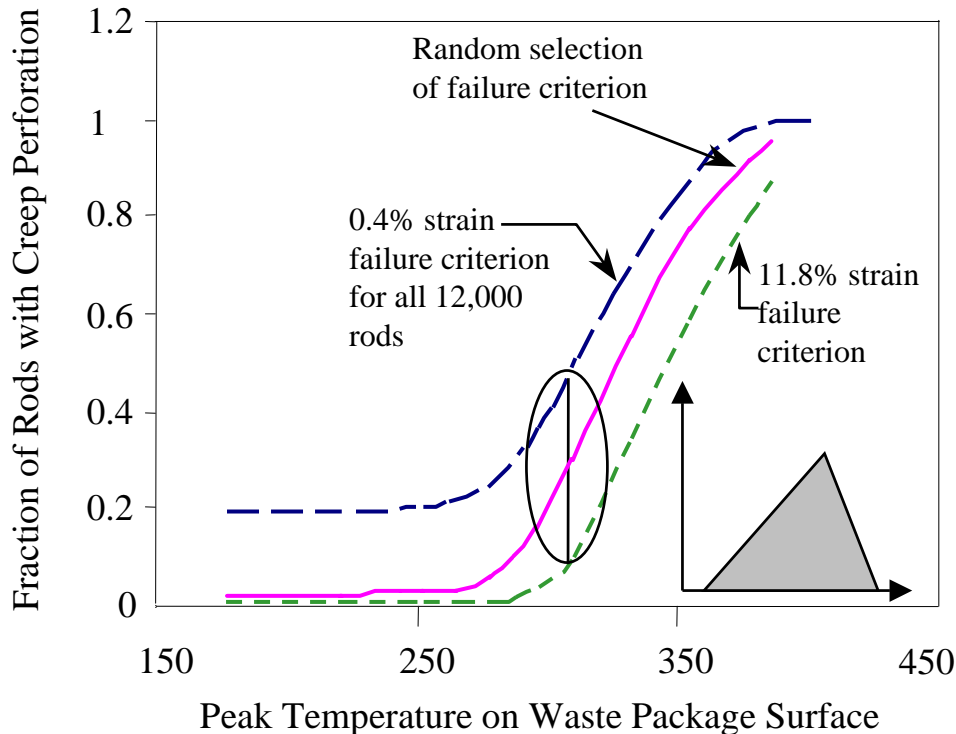
* Discussed in *Clad Degradation - Summary Abstraction AMR*

Cladding Perforations* before Receipt based on NRC Contractor Report (1969-1985) and Literature from 1985-1995



* Discussed in Initial *Cladding Condition AMR*

In TSPA-SR, Perforation from Cladding Creep Sampled Between Analytical Estimates



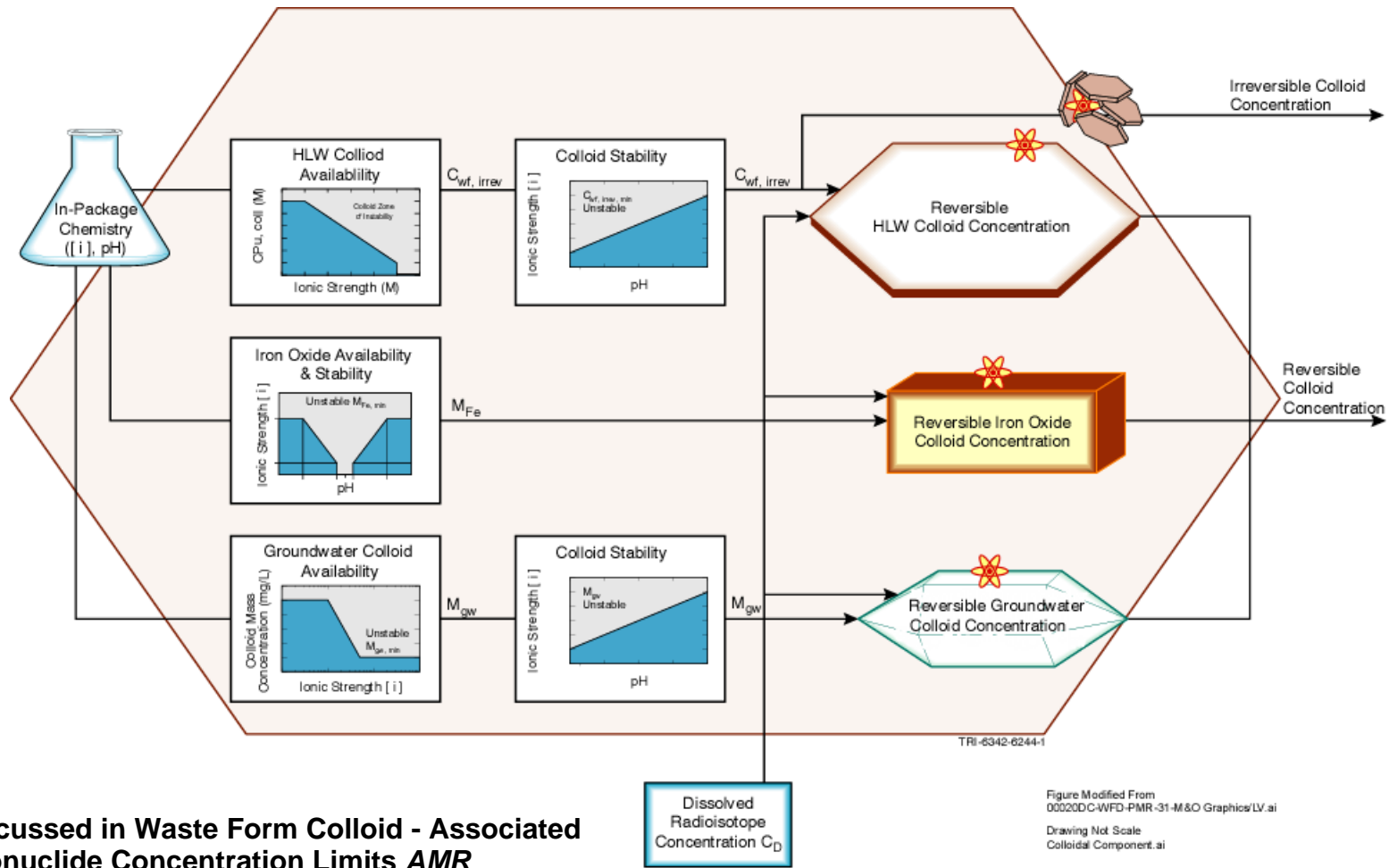
Perforation of Cladding* by Localized Corrosion

- To account for microvariation in chemistry, pitting is included since it is thought to be more likely to occur relative to other localized corrosion mechanisms
- Fraction of perforated rods conservatively assumed to be proportional to seepage of water into WP

$$f_{clad} = \frac{1}{2424m^3} \bullet q_{seep} \Delta t_i$$

* Fluoride pitting discussed in *Clad Degradation - Summary and Abstraction* AMR

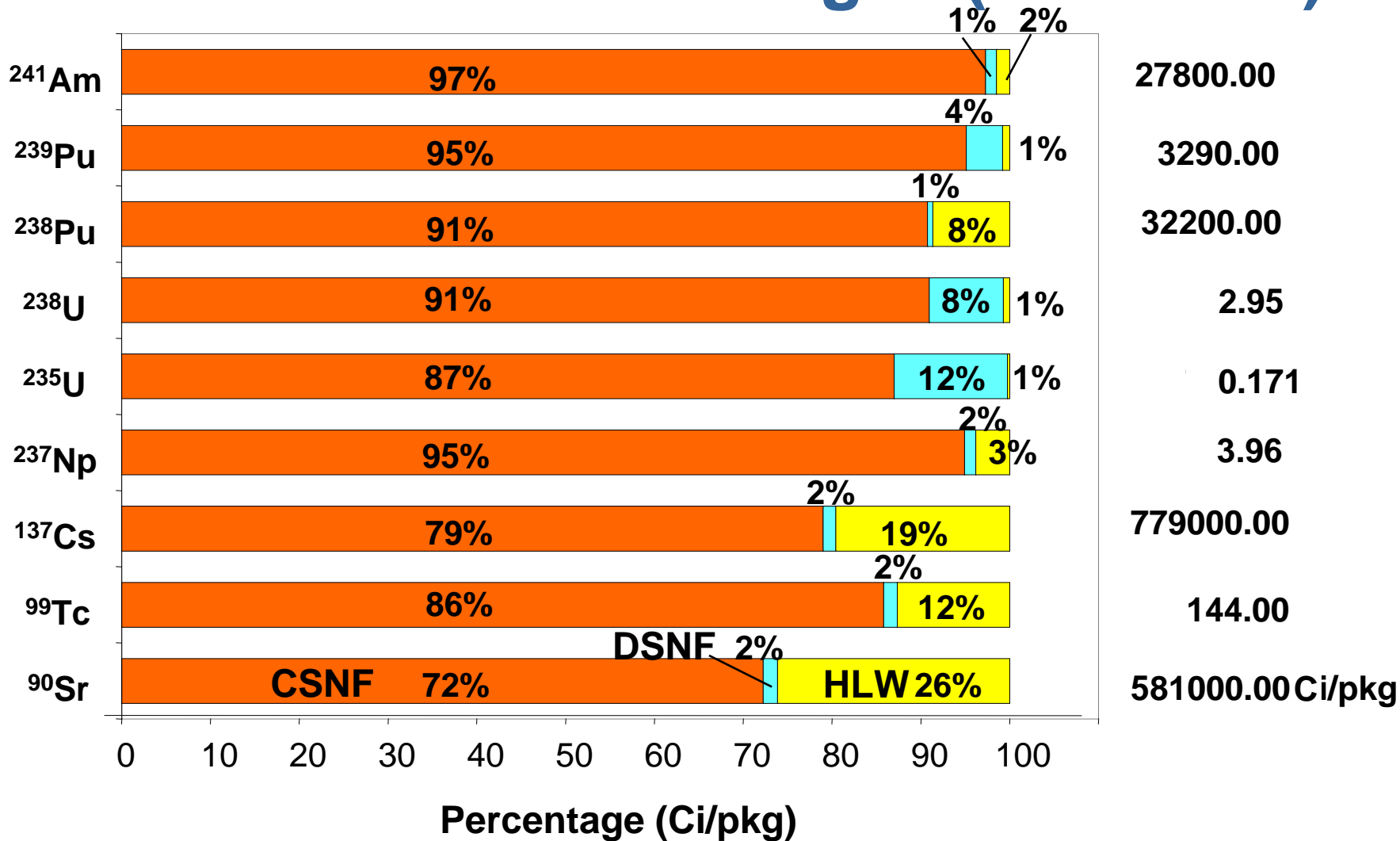
Colloidal Component* Evaluates the Colloid Concentration on Three Types of Colloids: Waste, Rust and Natural



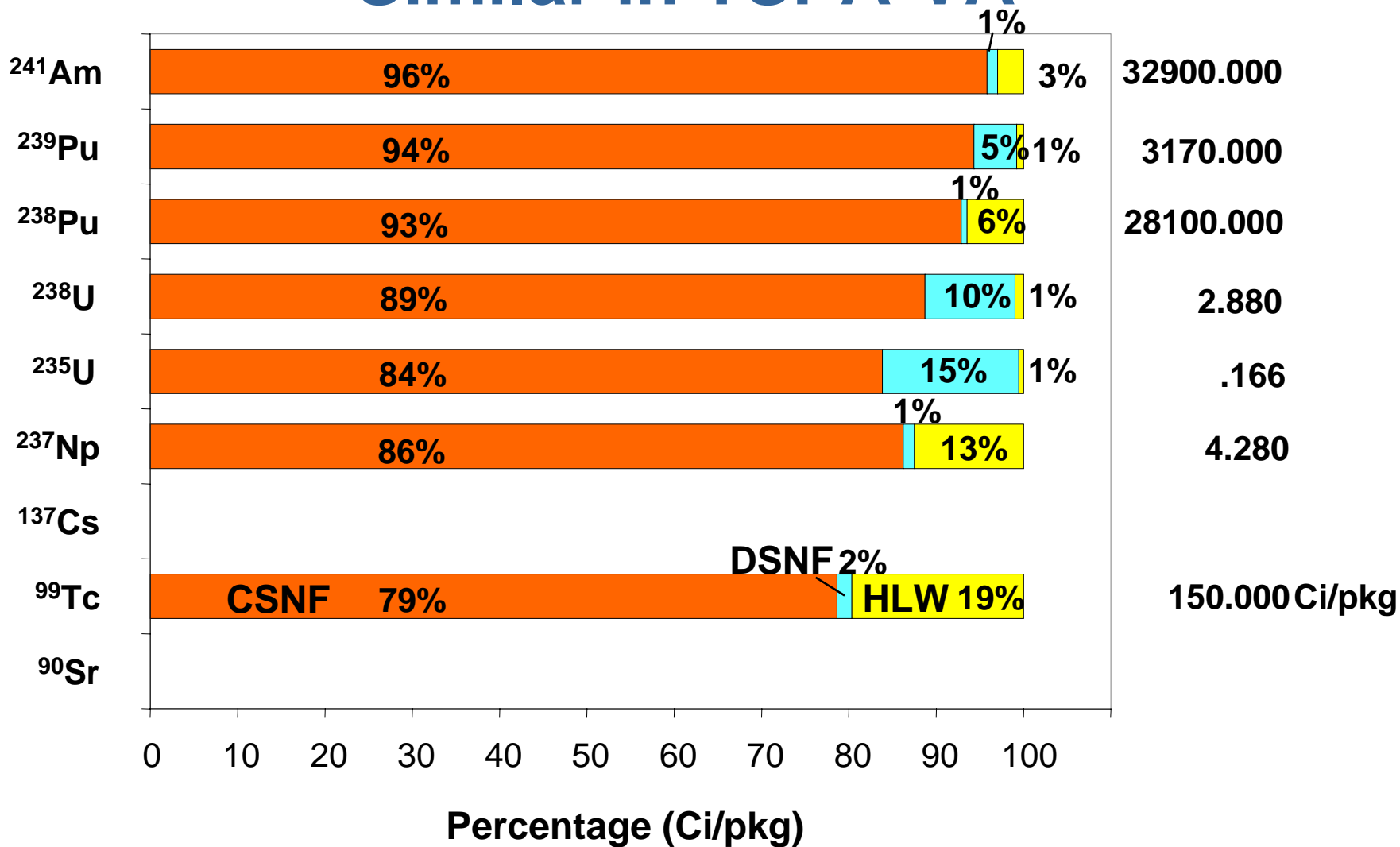
* Discussed in Waste Form Colloid - Associated Radionuclide Concentration Limits_AMR

Figure Modified From
00020DC-WFD-PMR-31-M&O Graphics/LV.ai
Drawing Not Scale
Colloidal Component.ai

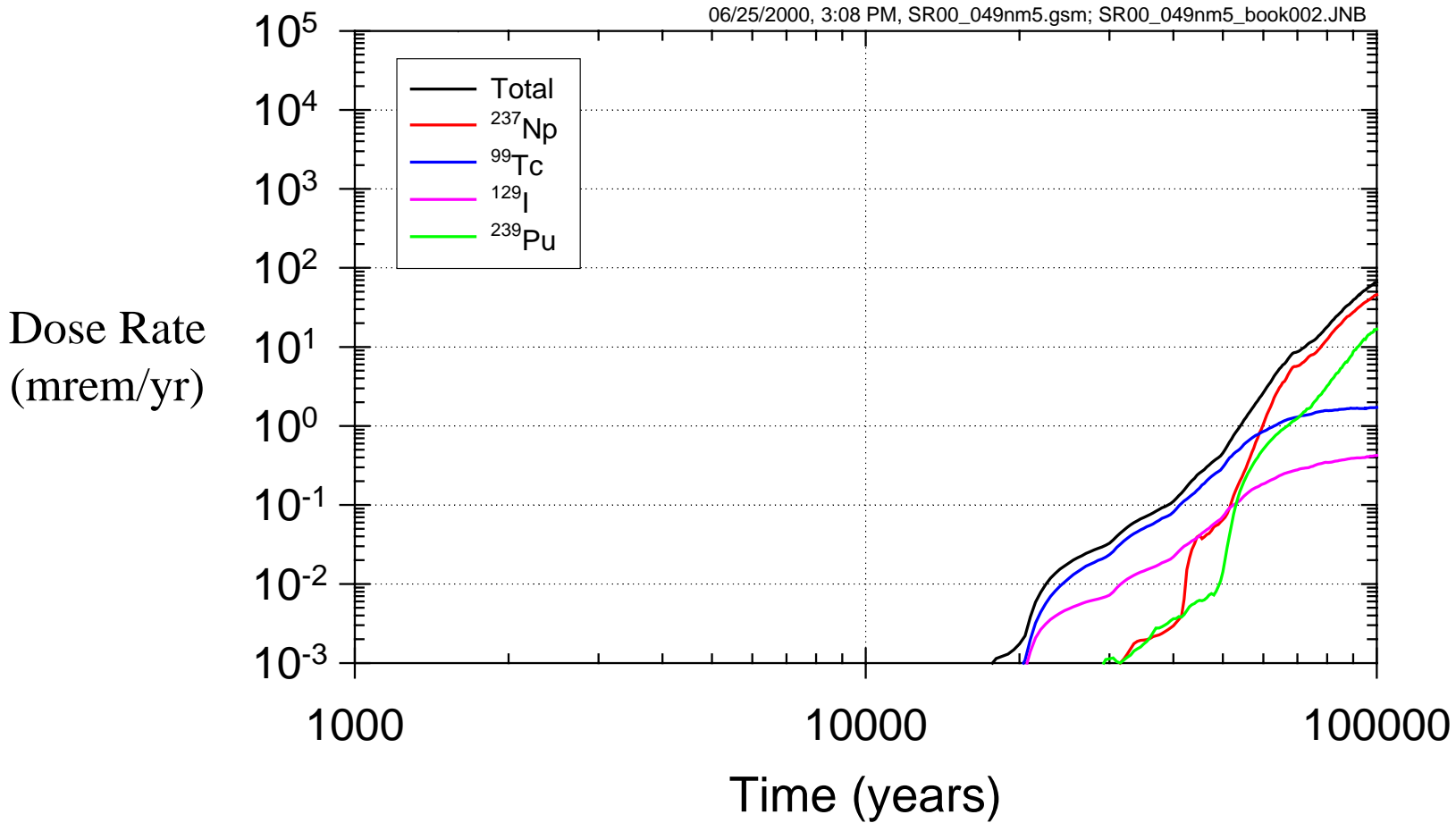
Highest Percentage of Radioisotopes Reside in CSNF Packages (TSPA-SR)



Percentage of Radioisotopes in Packages Similar in TSPA-VA



^{99}Tc and ^{237}Np Contribute Most to the Dose



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Rates of Release from CSNF Slightly Larger than from Co-Disposal Packages

CSNF

Co - Disposal

