



U.S. Department of Energy
Office of Civilian Radioactive Waste Management



Development and Implementation of the Localized Corrosion Model

Presented to:
Nuclear Waste Technical Review Board

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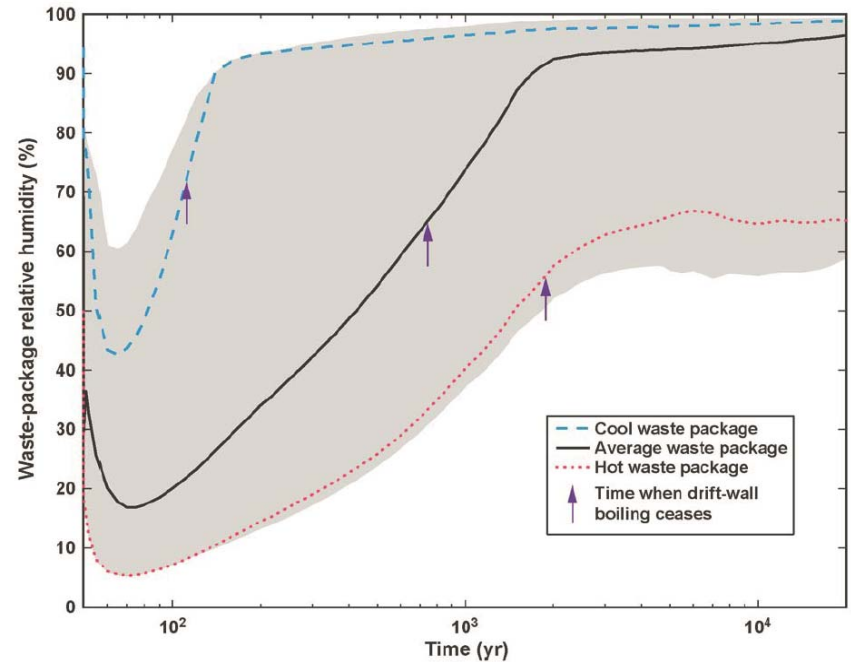
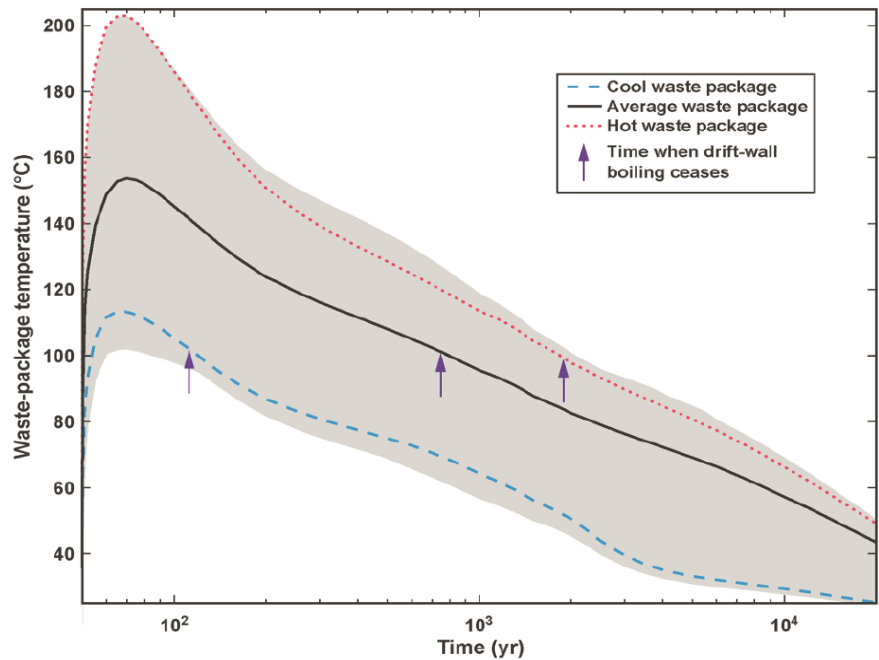
September 26, 2006
Las Vegas, NV

Outline

- **In-drift exposure conditions**
- **Localized corrosion (LC) model for seepage conditions**
 - Initiation model
 - Propagation model
- **LC model for dust deliquescent conditions**
- **Conclusions**



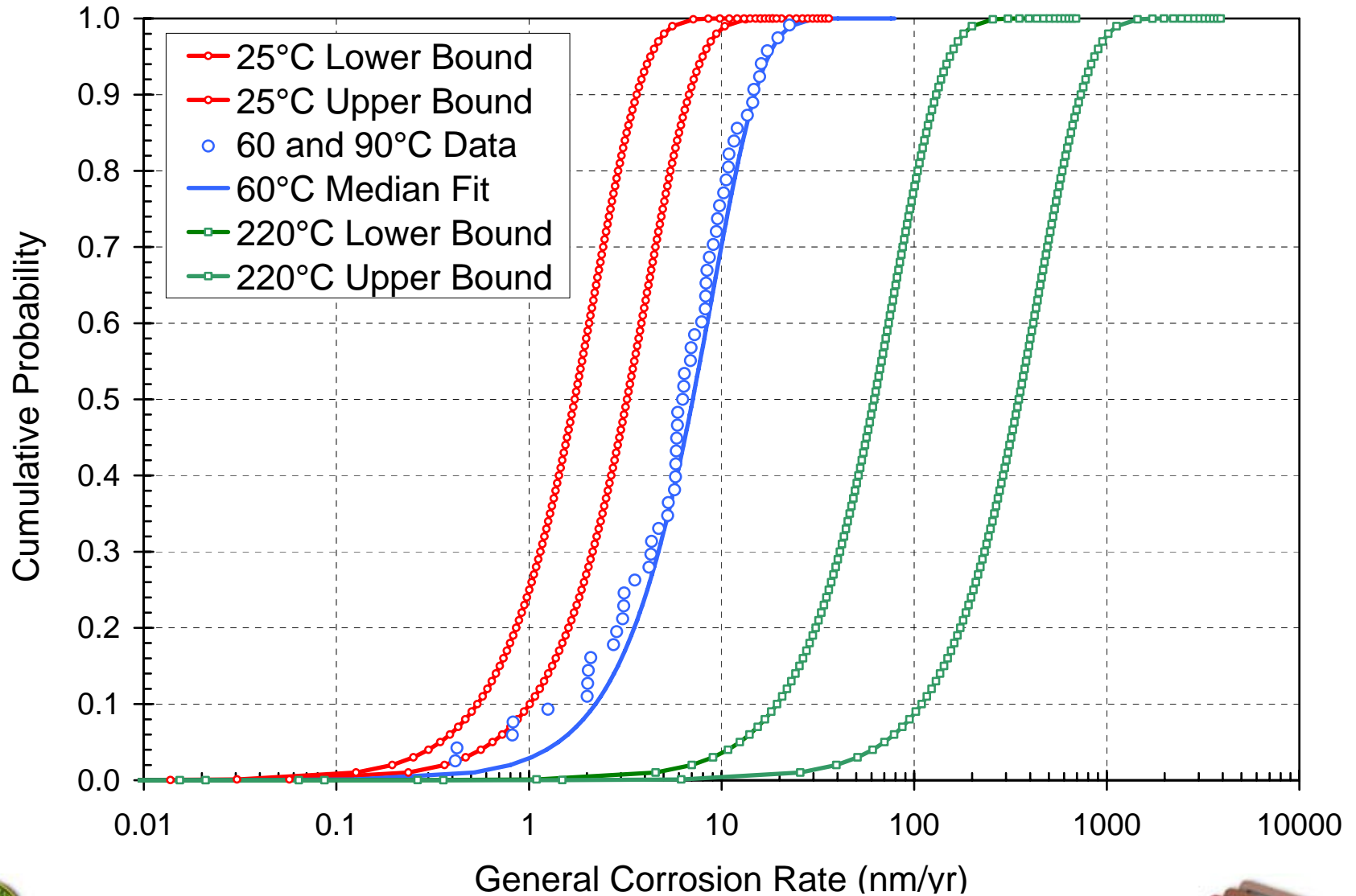
In-Drift Exposure Conditions



Ion	SDW (mg/L)	SCW (mg/L)	SAW (mg/L)	SSW (mg/L)	BSW-12 (mg/L)
K ⁺	34	3400	3400	142,000	67,620
Na ⁺	409	40,900	37,690	48,700	105,840
Mg ²⁺	1	<1	1000	0	0
Ca ²⁺	0.5	<1	1000	0	0
F ⁻	14	1400	0	0	1470
Cl ⁻	67	6700	24,250	128,000	130,830
NO ₃ ⁻	64	6400	23,000	1,313,000	1,395,600
SO ₄ ²⁻	167	16,700	38,600	0	14,700
HCO ₃ ⁻	947	70,000	0	0	0
Si	27 (60°C), 49 (90°C)	27 (60°C), 49 (90°C)	27 (60°C), 49 (90°C)	0	0
pH	9.8 to 10.2	9.8 to 10.2	2.7	5.5 to 7	12



General Corrosion Modeled to Always Occur



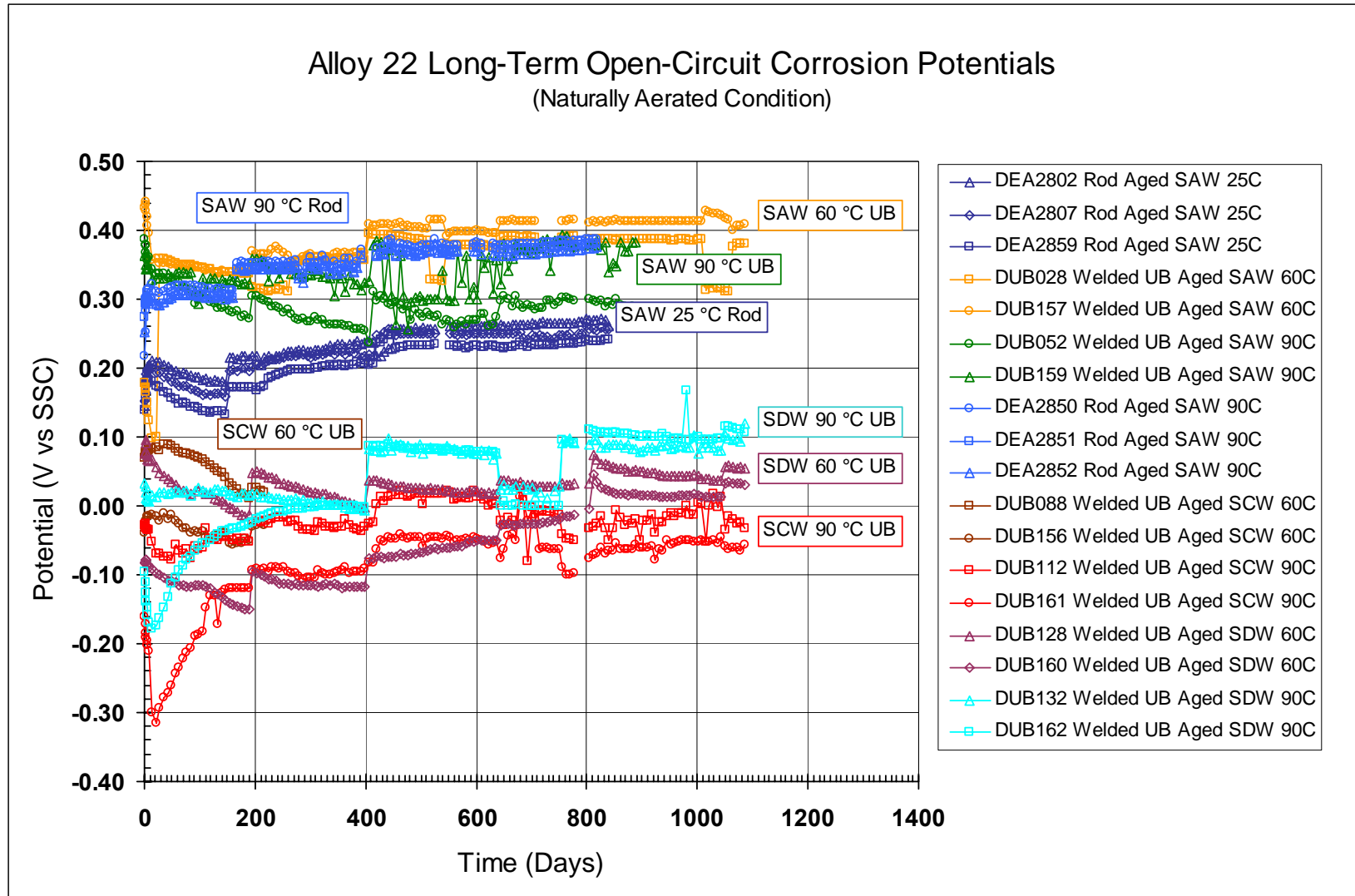
LC Model for Seepage

- **Model based on comparison of long-term corrosion potential with crevice repassivation potential**
 - If $E_{\text{corr}} \geq E_{\text{rcrev}}$ model initiates LC
 - Model applied to $T < 105^{\circ}\text{C}$
 - ◆ Maximum possible seepage temperature
 - If seepage occurs $\text{RH} < 77\%$ model initiates LC to account for potential salt separation
 - Entire waste package surface may be subject to crevice corrosion
 - ◆ Crevice corrosion thresholds less than pitting thresholds
- **Model fit to experimental data and accounts for associated uncertainty**



Long-Term Corrosion Potential

- Corrosion potential tends to increase with time



Corrosion Potential (E_{corr}) Model

- E_{corr} determined by long-term tests (>300 days)
- Over 55 test conditions are available

T 25°C to 155°C

pH 1 to 13

NO₃ 0 to 18 molal

Cl 0 to 36 molal

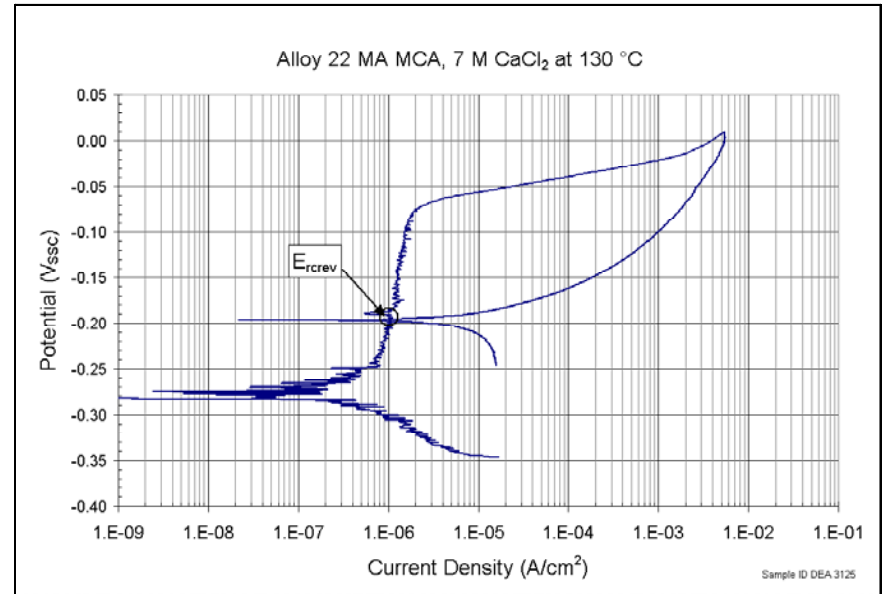
NO₃/Cl 0 to 100

$$E_{\text{corr}} = c_0 + c_1 T + c_2 \text{pH} + c_3 [\text{Cl}^-] + c_4 \log \left(\frac{[\text{NO}_3^-]}{[\text{Cl}^-]} \right)$$



Crevice Repassivation (E_{rcrev}) Model

- E_{rcrev} obtained from cyclic polarization
- Over 90 test conditions are available
 - T 25°C to 160°C
 - pH 1 to 13
 - NO_3 0 to 13 molal
 - Cl 0 to 36 molal
 - NO_3/Cl 0 to >1000



$$E_{rcrev} = E_{rcrev}^o + \Delta E_{rcrev}^{\text{NO}_3^-}$$

$$E_{rcrev}^o = a_0 + a_1 T + a_2 \text{pH} + a_3 \log([\text{Cl}^-]) + a_4 T \times \log([\text{Cl}^-])$$

$$\Delta E_{rcrev}^{\text{NO}_3^-} = b_0 + b_1 [\text{NO}_3^-] + b_2 \frac{[\text{NO}_3^-]}{[\text{Cl}^-]}$$



Cyclic Polarization: Na and K Brines at 110°C

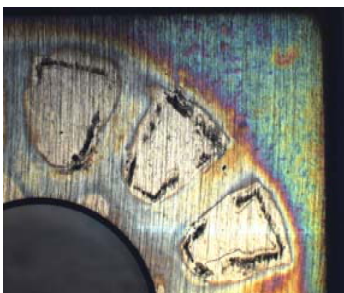
$\text{NO}_3/\text{Cl} = 0$



$\text{NO}_3/\text{Cl} = 0.1$

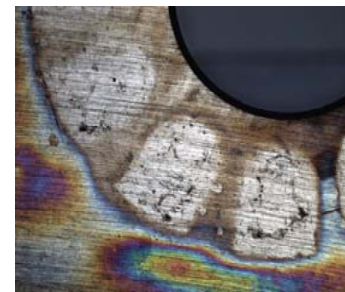


$\text{NO}_3/\text{Cl} = 0.2$



Increase in NO_3/Cl ratio results in shrinking of the hysteresis loop, and drives crevice attack deeper under the crevice former

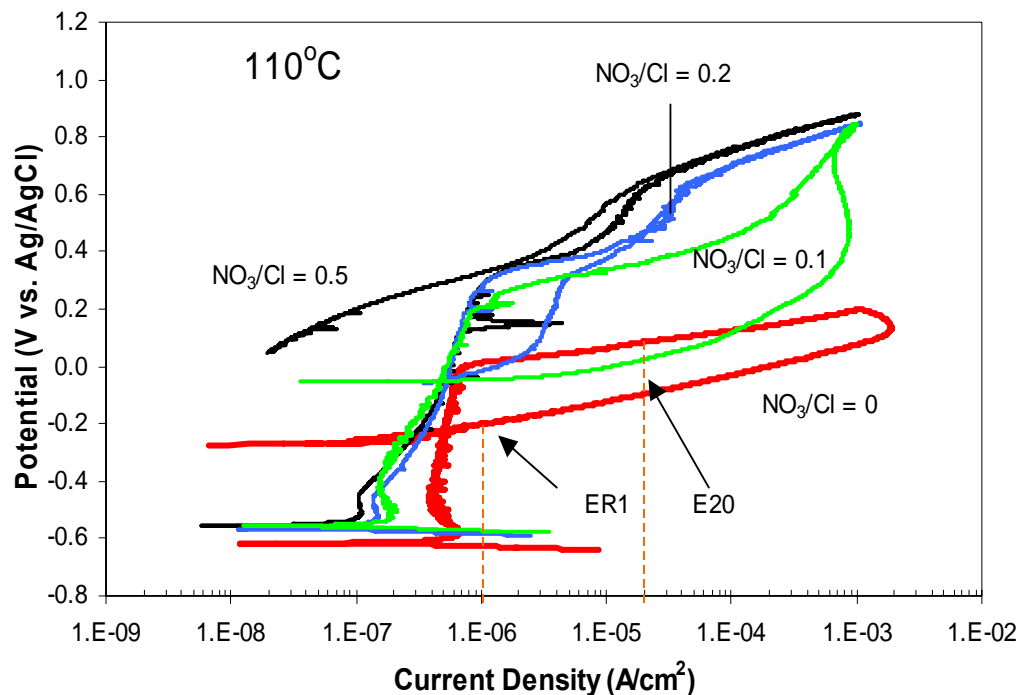
$\text{NO}_3/\text{Cl} = 0.3$



$\text{NO}_3/\text{Cl} = 0.5$

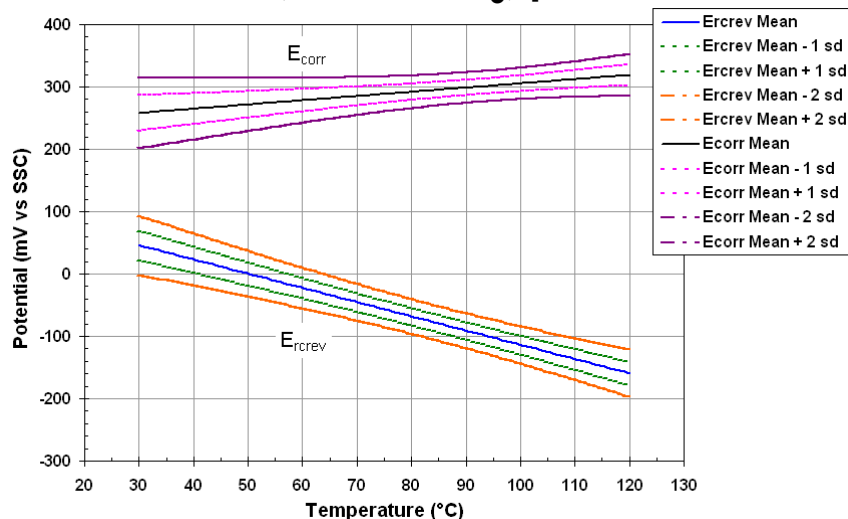


$\text{NO}_3/\text{Cl} = 1$

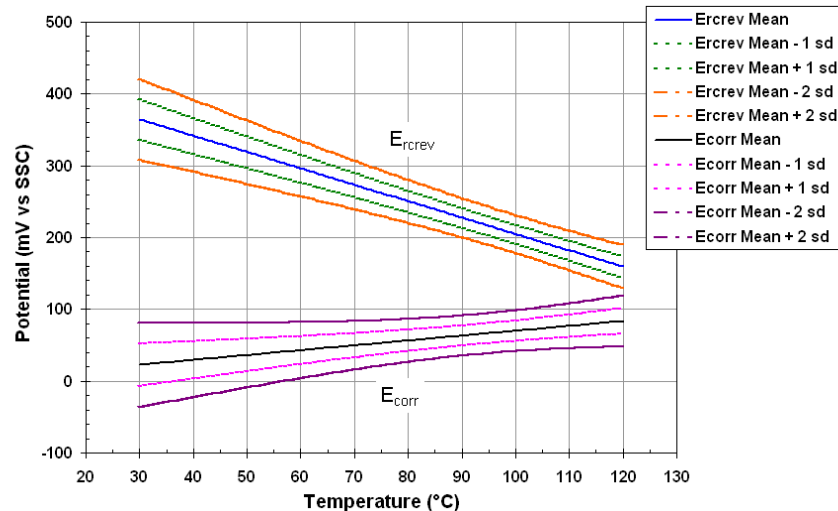


LC Initiation Model

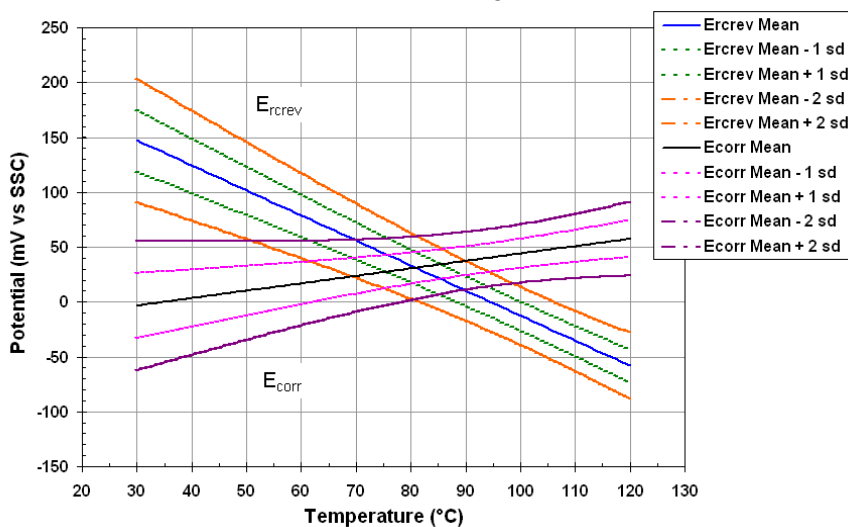
10 m Cl, 0.5 m NO₃, pH 3



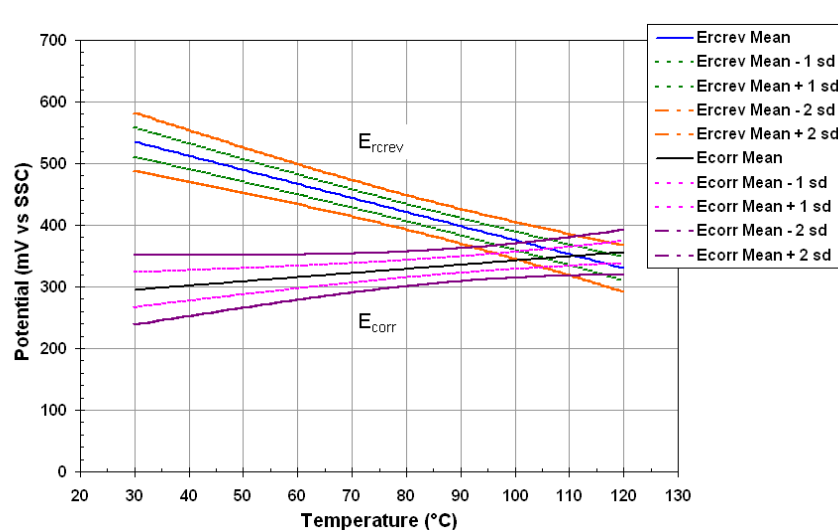
10 m Cl, 2.5 m NO₃, pH 7



10 m Cl, 0.5 m NO₃, pH 7



10 m Cl, 5.0 m NO₃, pH 3



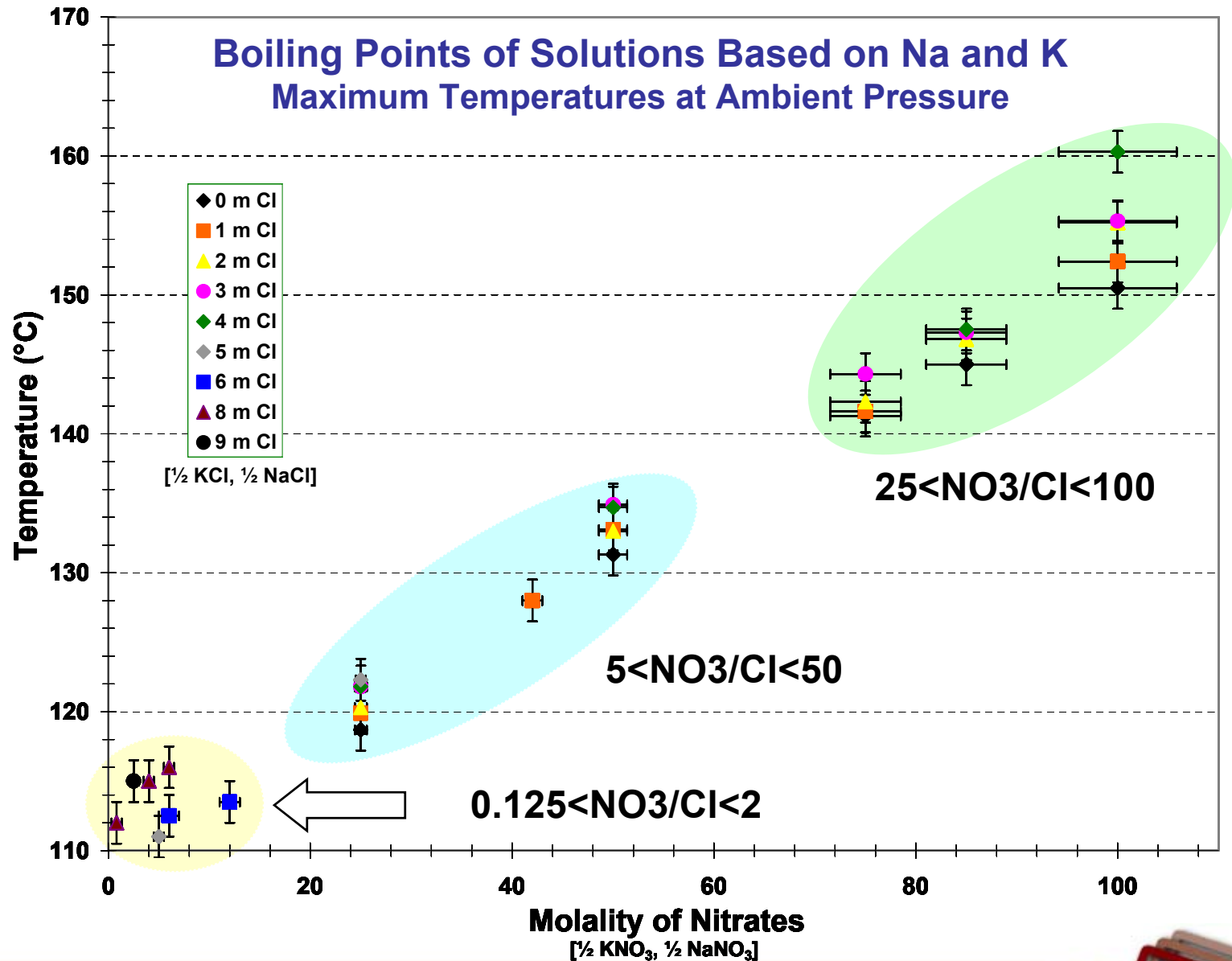
LC Propagation Model Seepage Conditions

- **Once LC initiates linear corrosion rate applied until penetration occurs (no stifling)**
- **Rate 12.7 to 1,270 μm per year**
 - Log uniform
- **Based upon testing in highly aggressive solutions**

Percentile	Corrosion Rate ($\mu\text{m}/\text{yr}$)	Type of Solution
0 th	12.7	10% FeCl_3 solution $\sim 75^\circ\text{C}$
50 th	127.0	Concentrated HCl $>100^\circ\text{C}$
100 th	1,270.0	Concentrated HCl $>150^\circ\text{C}$



Deliquescent Solution Chemistries



LC Model Dust Deliquescent Conditions

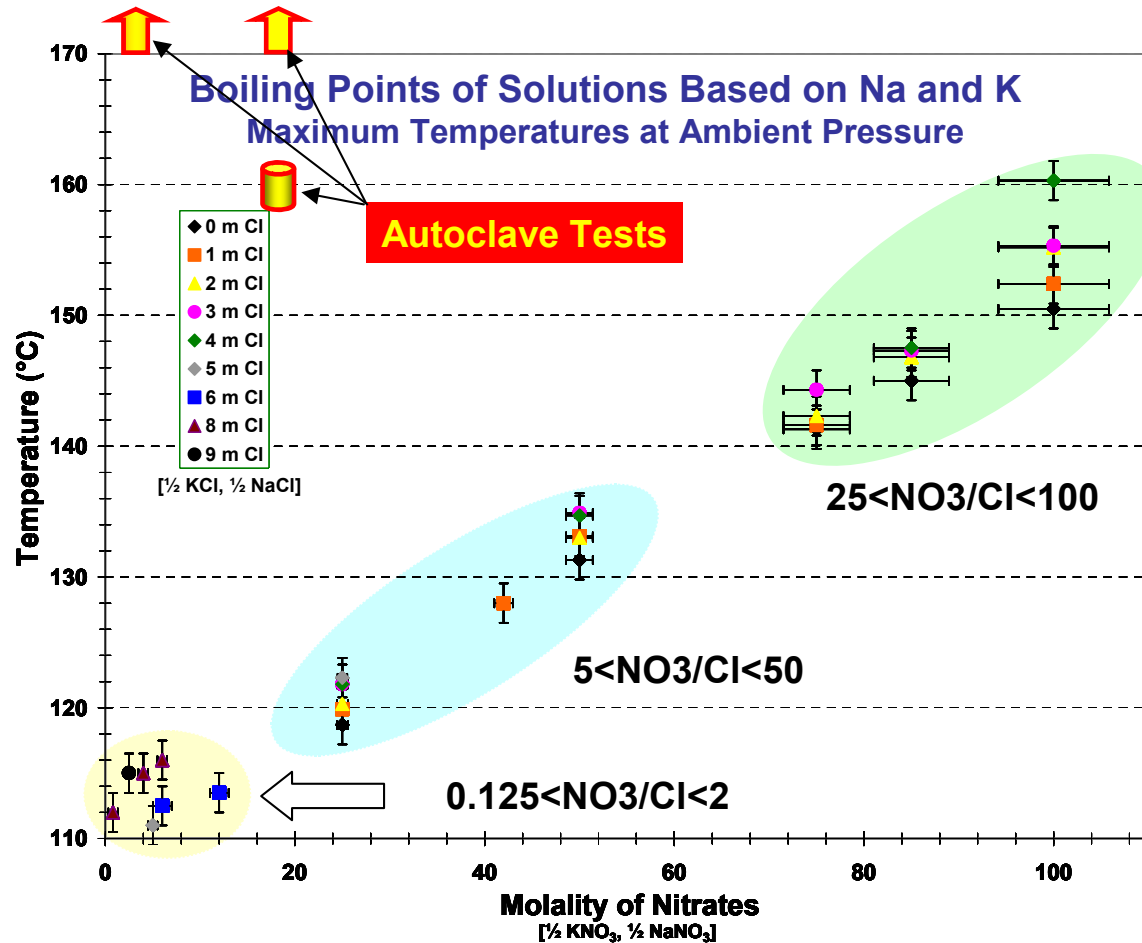
- **T > 105°C liquid can only exist as a result of salt deliquescence**
- **LC due to deliquescence is screened out on basis of low consequence**
 - *Analysis of Dust Deliquescence for FEP Screening (ANL-EBS-MD-000074 REV 01)*
- **5 questions must all be ‘yes’ for LC to occur**
 - (1) Can multiple-salt deliquescent brines form at elevated temperature?*
 - ◆ **Yes**
 - (2) If brines form at elevated temperature, will they persist?*
 - ◆ **Sometimes**



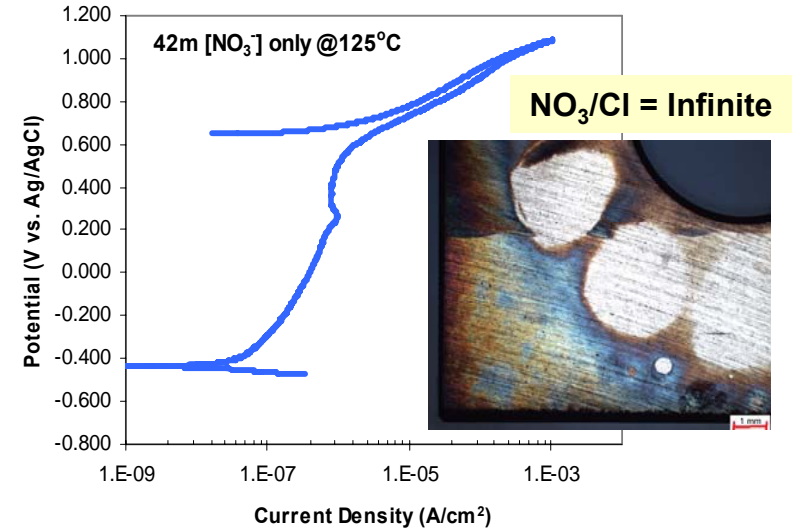
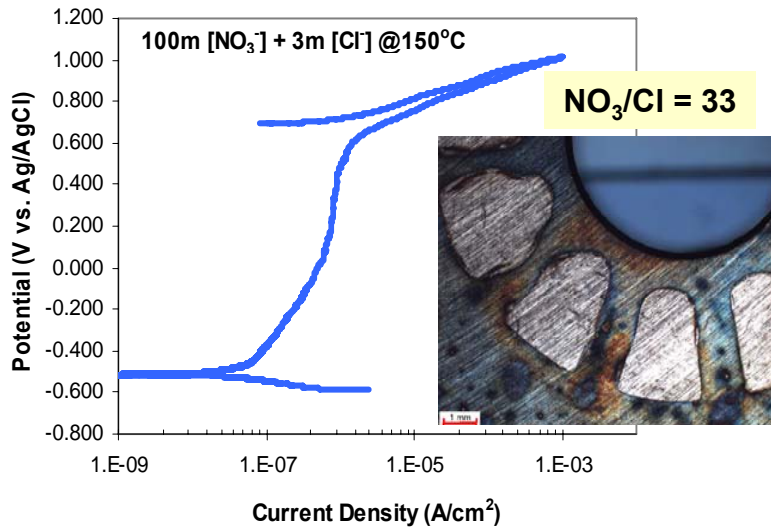
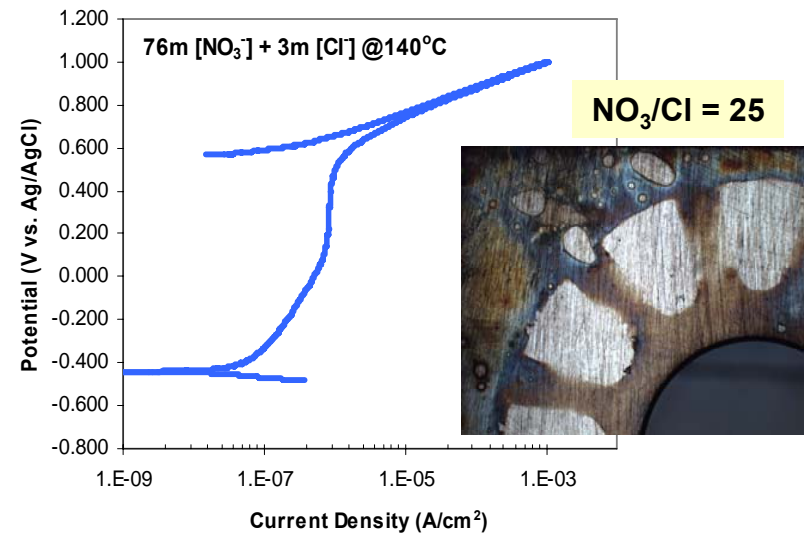
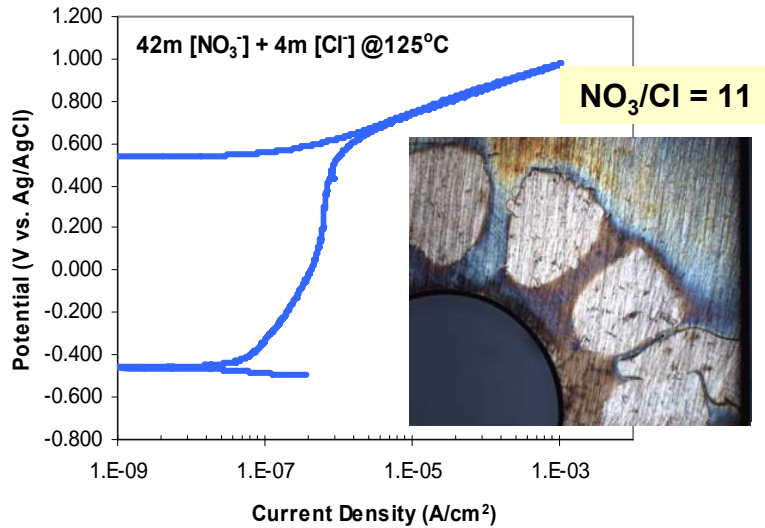
LC Dust Screening Arguments (cont.)

(3) *If deliquescent brines persist, will they be corrosive?*

– No - not under repository-relevant conditions



LC Dust Screening Arguments (cont.)



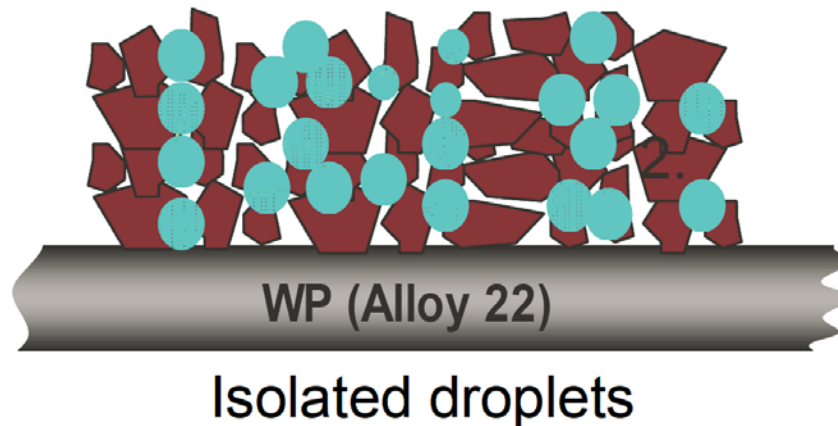
High NO₃ brines inhibit localized corrosion



LC Dust Screening Arguments (cont.)

(4) If deliquescent brines are potentially corrosive, will they initiate LC?

- No - not under repository-relevant conditions
- Max brine volume $\sim 1.8 \mu\text{L}/\text{cm}^2$ at 120°C or $\sim 18 \mu\text{m}$ thick
- Much of the brine will be held in dust by capillarity and not contact the waste package (WP) surface
- Small-scale and rapid mass transport will hinder establishment of chemical gradients
 - ♦ i.e., separation of cathode and anode



LC Dust Screening Arguments (cont.)

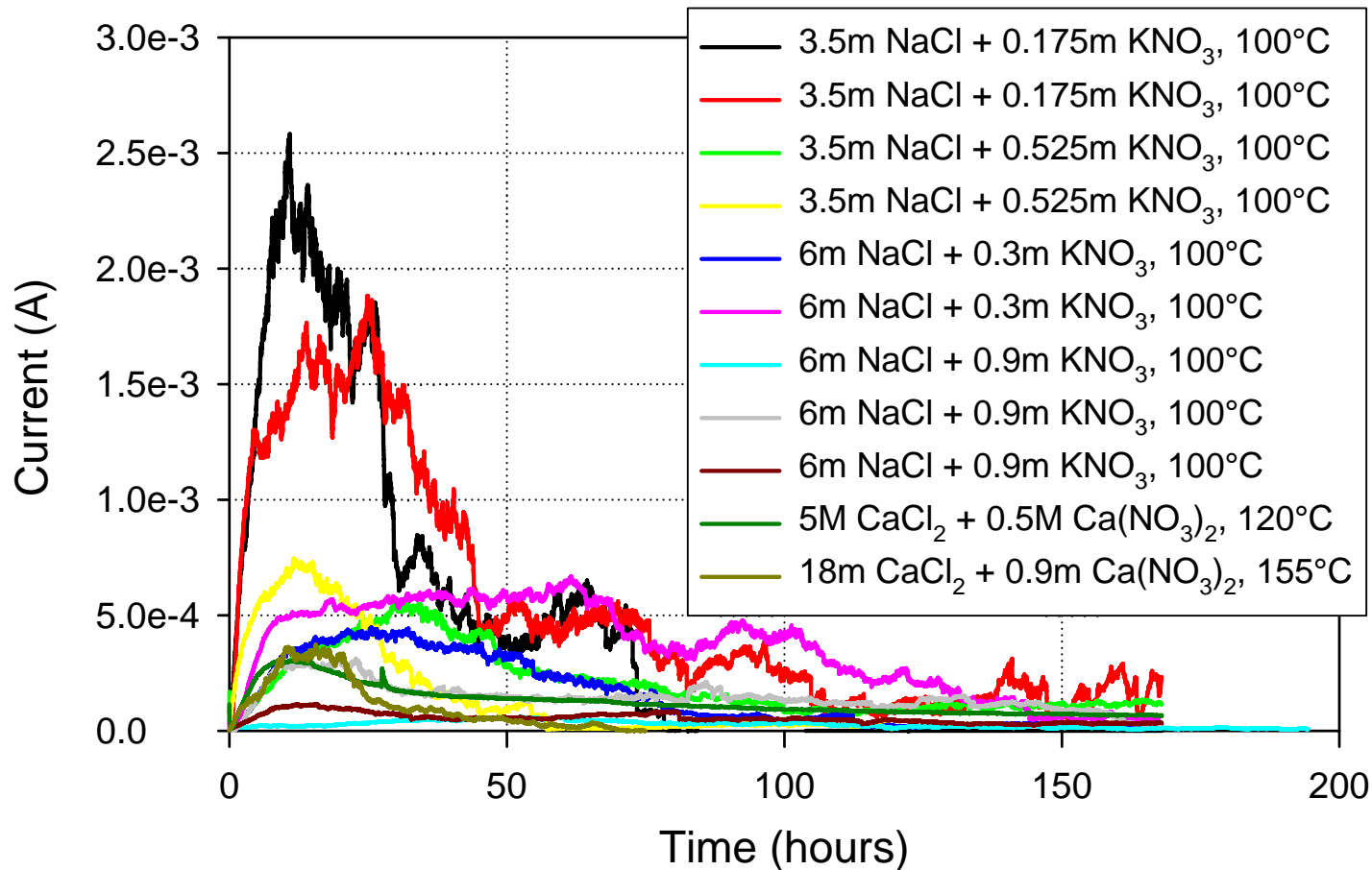
(5) Once initiated, will LC penetrate the WP outer barrier?

- No**
- Crevice penetration rates follow a power law, $D = At^n$**
 - He and Dunn 2006; Hunkeler and Boehni 1983; McGuire et al. 1998; EPRI 2002; Frankel 1998; Newman and Franz 1984**
- Experimental results (He and Dunn 2006; Kehler and Scully 2005) indicate that the depth of attack may be limited**
- Limited brine volumes and sequestration in corrosion products**
 - Limits amount of Cl available for reaction**
- Corrosion products can also limit the extent of crevice corrosion**



LC Dust Screening Arguments (cont.)

**(5) Once initiated, will LC penetrate the WP outer barrier?
(cont.)**



LC Dust Screening Arguments

- (1) *Can multiple-salt deliquescent brines form at elevated temperature? Yes***
- (2) *If brines form at elevated temperature, will they persist? Sometimes***
- (3) *If deliquescent brines persist, will they be corrosive?***
 - No, not under repository-relevant conditions
- (4) *If deliquescent brines are potentially corrosive, will they initiate LC?***
 - No, not under repository-relevant conditions
- (5) *Once initiated, will LC penetrate the WP outer barrier?***
No
 - On this basis, LC due to dust deliquescence is screened out due to low consequence



Conclusions

- **LC model based upon experimental data is implemented for seepage conditions ($T < 105^{\circ}\text{C}$)**
 - **LC is unlikely in nitrate containing neutral brines**
- **LC due to dust deliquescence is screened out on the bases of low consequence**

